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Osmond, T.

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MK II MEDIUM GIMBAL SIDE-PULL EXPERIMENT

SR-2005-18

Tim Osmond

August 2005

ABSTRACT

The new yaw resistant Mk II Medium Gimbal was tested throughout May 2005. An experiment was conducted to quantify the adverse effects of side force on the internal load cell in the gimbal. Side force was applied both through the centerline of the gimbal with respect to the *z*-axis and in moment to the gimbal both forward and rearward. Side forces of between 0 and 55 lbs were applied to the gimbal as the gimbal was experiencing rearward forces (drag forces) ranging between 0 and 300 lbs. This experiment demonstrated that there was on average 0.0139 lbs of absolute error added to the internal load cell with the addition of each pound of side force. Applying side force 6 inches rearward and forward of center, 0.0148 lbs and 0.0155 lbs respectively, of absolute error are added, on average for every pound of side force applied. This amounts to on average 0.76, 0.82 and 0.85 lbs of error added in the center, rearward and forward pull respectively.

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APPENDIX A: SECTION A RESULTS

APPENDIX B: SECTION B RESULTS (SIDE PULL 1, 2 AND 3)

1.0 INTRODUCTION

Within IOT a new yaw restrained tow post and Mk II medium gimbal have been designed and fabricated (for further details regarding this equipment see the Mk II Medium Gimbal Yaw Restrained Tow Post design manual, June 15, 2004). Before this new equipment may be issued for use, it must be tested to ensure that it operates to theoretical expectations and where it does not, tests must determine the extent to which there is deviation. A side pull experiment was conducted with the new Mk II medium gimbal throughout May 2005 as part of an effort to make these determinations. This report is assembled to present findings of this side pull experiment.

2.0 EXPERIMENT OBJECTIVE

The Mk II medium gimbal is outfitted with an internal load cell that may be interchanged from 50 lbs, 100 lbs and 300 lbs. It is intended to measure model drag and reverse drag only and should not be affected by side forces applied through the center axis or in moment about the z-axis with the gimbal.

This experiment was designed to determine the extent to which, if any, side force interferes with readings from the internal load cell in the medium gimbal. To make this determination there were two sections in this experiment referred to as Section A and Section B.

The objective (Objective A1) of section A was to determine the internal load cells deviation from theoretical expectations without side force applied.

There were two objectives in section B. The first object (Objective B1) was to apply a perpendicular load to the gimbal without moment and determine the effects on the gimbal internal load cell. The second objective (Objective B2) was to apply both side force and moment to the gimbal to quantify the effect on the gimbal internal load cell.

All side forces applied were applied perpendicular to the x-axis with respect to the gimbal. Side forces were applied through the neutral point on the x-axis of the gimbal as well as 6 inches in the positive x direction and 6 inches in the negative x direction. (see figure 1)

3.0 EXPERIMENTAL FACILITY

To conduct the necessary pulls to accomplish objectives A1, B1 and B2 the gimbal needed to be free to experience forward and rearward loads as well as side loads without undergoing pitch or roll. To accomplish this the gimbal was suspended attached to the bottom of the tow post. The pitch-lock plate was attached to the gimbal. This prevented the gimbal from both pitch and rolling.

The tow post was bolted to the calibration frame found in the prep shop of the Institute for Ocean Technology. (see figure 2)

A gimbal board was fabricated that contained the necessary features to allow the gimbal to be bolted to the board and allow cables be attached to the front and the rear of the boards as well as several locations on the side of the board. (see figure 3)

Cables, pull frames, weigh pans and pulleys were used to apply loads to the board.

In-line load cells were used to measure the loads applied to the gimbal board through each cable (see figure 4). A 300 lbs load cell was used as the gimbal internal load cell for this experiment.

A Data Acquisition System (DAS) measured the output from each load cell.

4.0 PROCEDURE

All experimental facility components were located (c-clamps, pulleys, pull frames, load cells and shackles) or fabricated (pulley plates, pull frame bars, cables, the gimbal board and the calibration frame bridal).

All load cells were manually calibrated. Known weights were hung from the load cells and the voltages were recorded using the DAS. This data was implemented into an excel chart and a trend line was used to generate the slope equation (the equation is of the form mX + b). This equation was entered into the DAS and the zero intercept (b value) was the determined based on the load cell reading while undergoing 0 load. A load cell undergoing 0 load is considered to be a load cell lying in a horizontal position with nothing attached.

The experimental facility was fully assembled as described above. A 300 lbs load cell was used for the rear load cell (positive drag) and for the internal gimbal load cell. A 100 lbs load cell was used for forward load (negative drag) and for the side load cell (<u>see load cell</u> <u>locations, figure 4</u>).

This experiment was composed of two sections. Section A was intended to determined the error in the gimbal before any side load was applied. Section B was intended to determine the error in the gimbal after the side load was applied.

<u>Section A</u> (<u>see figure 5</u>)

Load cell readings were manually recorded with the application of each load. A preload tension was applied to the forward and rearward load cell. A net forward load of approximately 20 lbs was applied to the gimbal. From this point the rearward load was incrementally increased until a net rearward load of approximately 270 lbs was reached. This was repeated three times. The differences between the forward and rearward load cells are used to produce a theoretical load values for the internal gimbal load cell.

Section B (see figure 6)

The front, rear and side cables were preloaded. The side pull cable was attached to the center connection point of the gimbal board. Load cell readings were taken at every load addition. A random load was applied in the rearward direction to the gimbal. At this rearward load, side

loads were randomly increased in six increments to approximately 55 lbs. This was then repeated using different incremental loads. The rearward load was then increased and the process of loading the side pull was repeated. The process of increasing the rearward load was repeated until there was a net rearward load on the gimbal of approximately 280 lbs. To reach this load five random increments of rearward load were used.

Section B was repeated, only with the side load attached both 6 inches forward of the centerline of the gimbal and 6 inches rearward of the centerline of the gimbal (see figure 3).

Section B is summarized for clarity. The gimbal was tested at 3 different side pull positions; the center of the gimbal axis, 6 inches rearward of center and 6 inches forward of center. At each location a small preload was applied in the forward direction. Loads were then applied in the rearward direction to simulate drag. Rearward loads ranged between 0 and 280 lbs in 5 random increments. At each increment of rearward load, 12 (2 x 6) random loads ranging from 0 and 55 lbs were applied as side pulls. Readings were taken for all four load cells at each increment.

5.0 RESULTS

All results recorded from this side pull experiment are found under <u>\Knarr\CAD_User\Projects\421016\Medium_Gimbal_MkII\Tosmond\WeightApplications.xls</u> Data taken from section A is found on sheet "Section A" and is contained in <u>APPENDIX A</u>. Data taken from section B is found on sheets "Side Pull (1), (2), and (3)" and is contained in <u>APPENDIX B</u>.

A summary of the averages and ratios calculated from the recorded data is shown on table 1.

Section	Result	Value
Section A	average absolute error for gimbal values greater than 20 Lbs	0.41
Section A	average absolute error for gimbal values greater than 50 Lbs	0.43
Section A	average % error for gimbal values greater than 20 Lbs	0.44
Section A	average % error for gimbal values greater than 50 Lbs	0.38
Section B	average absolute error - center pull	1.00
Section B	average absolute error - 6 inch rearward pull	1.10
Section B	average absolute error - 6 inch forward pull	1.05
Section B	average % error - center pull	1.07
Section B	average % error - 6 inch rearward pull	1.33
Section B	average % error - 6 inch forward pull	1.23
Section B	ratio of change in absolute error to change in side load - center pull	0.0139
Section B	ratio of change in absolute error to change in side load - 6 inch rearward pull	0.0148
Section B	ratio of change in absolute error to change in side load - 6 inch forward pull	0.0155

Table 1 – Mk II Medium Gimbal Experimental Results

From the data contained in APPENDIX B, charts 1, 2 and 3 have been generated.

Chart 1

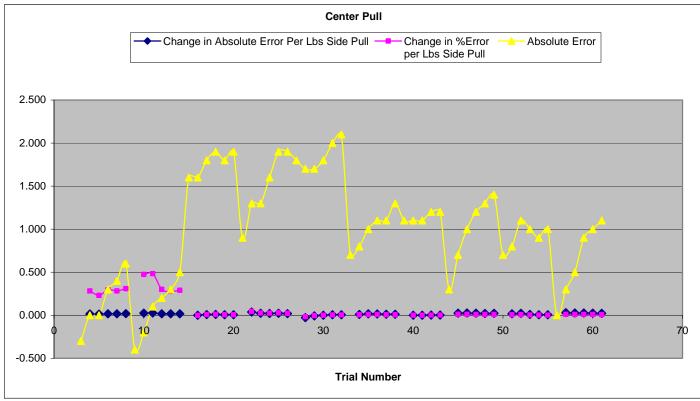


Chart 2

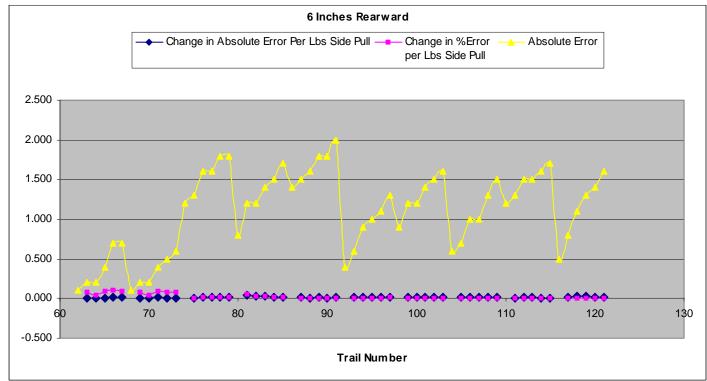
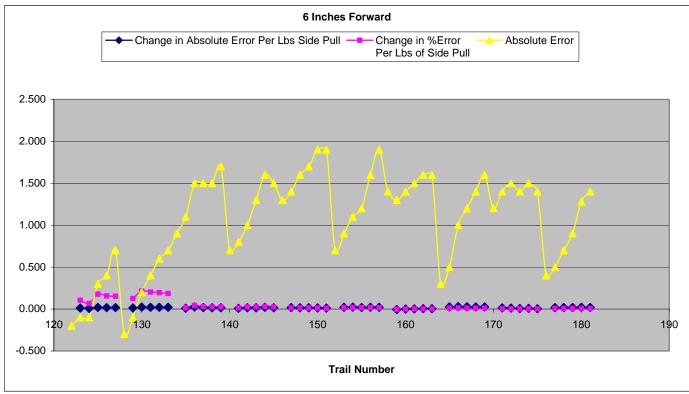


Chart 3



6.0 DISCUSSION

Data taken from Section A indicated that there was some error inherent in the gimbal without the inclusion of side load. Absolute error in the gimbal recorded to be on average 0.41 lbs for gimbal readings greater than 20 lbs and 0.43 lbs for gimbal readings greater than 50 lbs with the internal gimbal continually under reading theoretical values. In terms of % error this equated to an error of approximately 0.44% for gimbal readings greater than 20 lbs and 0.38 % for gimbal readings greater than 50 lbs. For readings less than 20 lbs, the experiment did not yield meaningful results.

The data taken from Section B shows that side force on the gimbal does have some effect on the error in the internal load cell of the medium gimbal. Throughout the experiment the absolute error would increase to the order of several tenths of a pound between the range of 0 – 55 lbs of added side force. Using the data recorded it was calculated that on average the error increased 0.0139 lbs per pound of side force added to the gimbal when the side force was applied to the center of the gimbal. This value increased only slightly to 0.0155 lbs and 0.0148 lbs per pound of side force added for side forces applied 6 inches forward and rearward respectively of the center point for the gimbal. This equates to an increased error of, on average 0.76 lbs, 0.85 lbs and 0.82 lbs of added error with an addition of 55 lbs side force to the center, 6 inches forward and 6 inches rearward respectively. Average moments for the rearward and forward applied forces were 165 in-lbs with a maximum moment of 330 in-lbs

In charts 1, 2 and 3 we can see the absolute error increase as the side load is incrementally increased to 55 lbs. As the load is returned to 0 we see the absolute error drop off. However we also see that the ratio of the change in absolute error to the change in side load added remains nearly constant throughout the entire section for all three pull locations. The ratio of the change in % error to the change in side load is included in these charts and shows consistency through each set of side pulls.

An unusual occurrence in the load cells was noted. After load was applied and then removed the load cells only returned to the same starting point within a couple of pounds. This was particularly true for the load cell in the gimbal. Before commencing a pull the load cell was noted to be in a certain amount of pretension. After the pull test the load cell would be reading a different value by any difference up to as large as 2 lbs. I would have expected the load cell to return to its original value to within several tenths of a pound. This indicates that the primary source of error may have been discrepancies within the load cell.

7.0 CONCLUSIONS

The medium gimbal internal load cell was found to be reading an error of on average between 0.38% - 0.44% when a 300 lbs internal load cell was used to measure drag loads of 20 lbs or greater. This error was found to exist before the application of side force.

With the application of side force without moment there was an increased in the error of the internal load cell. This was calculated to be on average 0.0139 lbs of error in the internal load cell for every pound of side force applied. This equaled on average an increase of 0.76 lbs of error with the addition of 55 lbs.

With the application of side force and moment applied to the gimbal there was an increase in error of the internal load cell. This was calculated to be on average 0.0148 lbs for a rearward force containing an average moment of 165 in-lbs. The average error gain was 0.82 lbs error at 55 lbs side force, 330 in-lbs moment. For the forward force the error was calculated to be on average 0.0155 lbs with an average moment of 165 in-lbs. The average error gain was 0.85 lbs error at 55 lbs side force, 330 in-lbs moment.

8.0 FIGURES

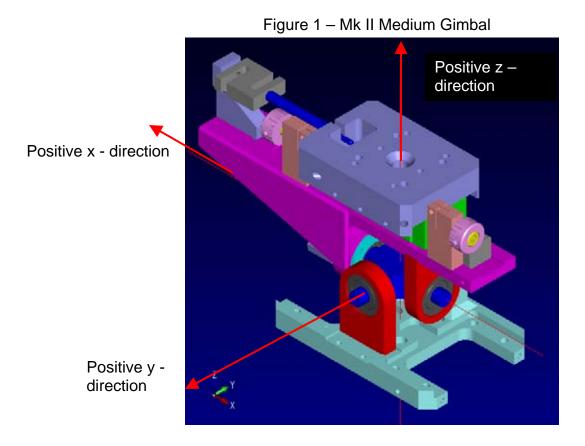
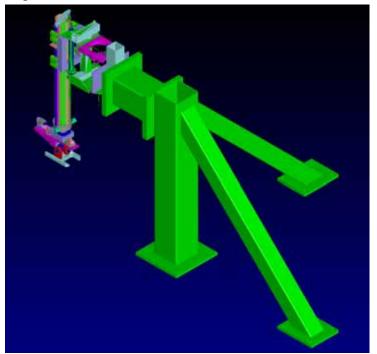


Figure 2 – Tow Post attached to Calibration Frame



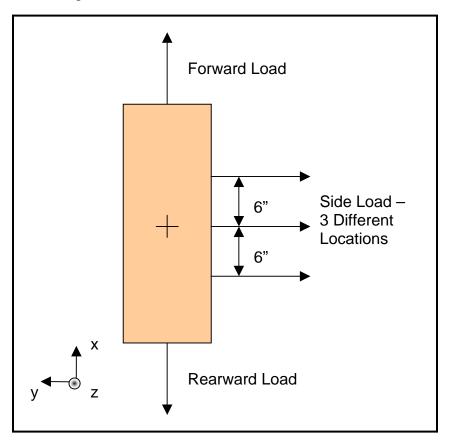
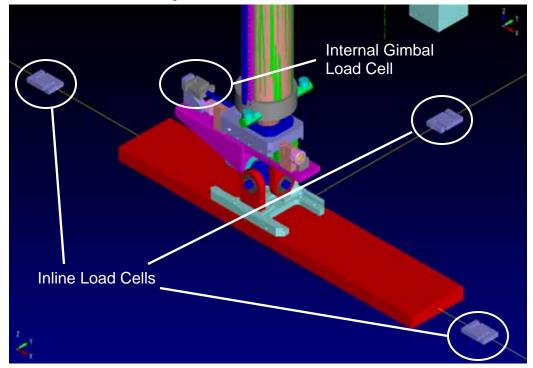


Figure 3 – The Gimbal Board with Load Locations

Figure 4 – Load Cell Locations



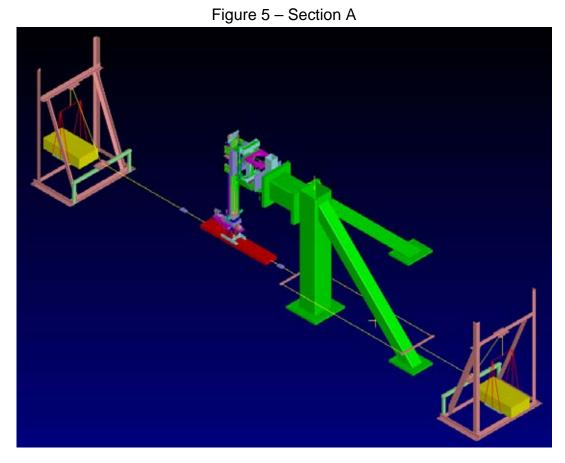
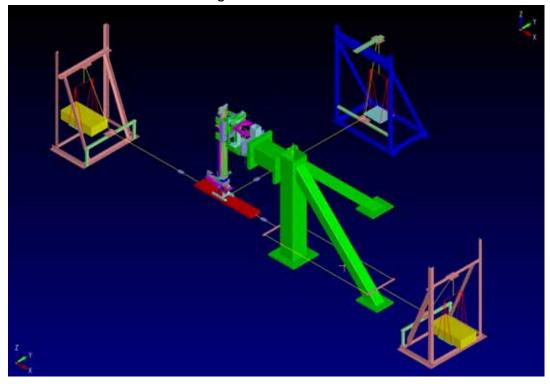


Figure 6 – Section B



APPENDIX A: SECTION A RESULTS

Trail # A A1 A2 A3	Forwa Pan 5.2	ghts (lbs rd 4	Rearv	ded / Tota vard	Side					Theoretical					6 10 10 10 10 10 10 10 10	*****	19 19 20 20 20 20 20 20	
A1		Δ			Side	Forward	Rearward	Side	Reading	Reading	Difference	Difference	Error		F12 F	6 Cnt	<u>r A6 A</u>	12
		4																
A2 A3	5.2		Pan	6		3.9	5.9		-2.2	-2.0								All Load
A3		9.2	0 0	6		8.1	5.9		1,5	2.2	3.7	4.2	-0.5 -2.3	11.9			1.1.1	
	21.4	30.6	0	6		26.2	6.0		17.7	20.2	19.9							Side Loa
A4	5	35.6	0	6		30.8	6.0		21.6	24.8		26.8	-3.0	**************		31. Z	Sec. Control	
A5	0	35.6	15.6	21.6		31.7	21.4		9.5	10.3	A 12 & S & B & B & B & S & S & S & S	12.3	-0.6	4.9			1	Forward
A6	0	35.6	44	65.6		33.8	56.3		-20.5	-22.5	************	-20.5	2.2 0.9	10.7		*****		Rarewar
A7	0	35.6	36.8	102.4		35.7	87.2	********	-50.8 -79.5	-51.5 -79.9	*****	-49.5 -77.9	0.9	1.8				Gimbal I
A8		35.6	37	139.4	* 	37.9 40.1	117.8 152.1		-79.5 -111.7	-79.9 -112.0	the second second second second second second second	-77.9	0.6 0.5 0.3	0.8				
A9	U V	35.6	38.4 35.4	177.8 213.2	*****	40.1	*************		-111.7 -143.1	-112.0			0.0 0 3	0.5		******		average
A10	0	35.6 35.6	54.6	267.8		42.0	*************		-143.1	-143.2		-141.2	0.3	0.2				∽ to or gre
A11 A12	0	35.6	53.2	321		42.8	270.0	*****	-227.2	-227.2	-225.0		0.0		*****			• • • • • • • • • • • • • • • • • • • •
B					*	-12.0	270.0						0.2	0.1				
B1	Pan	4	Pan	6		5.1	5.4		-1.2	-0.3								average
B2	5.2	9.2	0	6	and the second	8.6	5.4		2.1	3.2	N N N S N N S N N N N N N S	3.5	-0.2	5.7				to or gre
B3	5.2	14.4	0	6		12.4	5.4		5.8			7.3	-0.3					
B4	4.8	19.2	0	6		16.2	5.5		9.3	10.7	10.5	7.3 11.0	-0.5					
B5	0	19.2	15.6	21.6		16.6	18.6		-2.4	-2.0	-1.2		-0.5 0.5	29.4				Test Cor
B6	0	19.2	35.4	57		17.6	48.5		-31.6	-30.9			0.2	0.7				
B7	0	19.2	53.2	110.2	 	19.0	94.7		-76.4	-75.7	5 36 36 36 36 36 36 36 36 36 36 36 36 36		0.2					
B8	0	19.2	38.4	148.6	*	20.2	128.7	****	-109.3	-108.5	3 30 30 30 30 30 30 30 30 30 30 30 30	-108.2	0.1					
B9	0	19.2	44	192.6		21.3	164.6		-144.1	-143.3		* * * * * * * * * * * * * * *	0.1			*******		
B10	0	19.2	36.8	229.4		22.4	195.4		-173.9			-172.7	0.0					
B11	0	19.2	37	266.4	* * * * ~ < ~ < ~ < * < * * * * * * * *	22.2	227.4	*****	-206.0				0.1	***************	*******	** ****		
B12		19.2	54.6	321	* *	23.2	270.7		-247.4	-247.5	-246.2	-247.2	1.0	0.4		_		
С					1				0.0	1.0		1						
C1	Pan 4.8	4	Pan	6	Sec. Sec.	4.4	6.0 6.0		-3.0	-1.6 2.4	St	10	0.2	5.0				
C2		8.8	0	0	Construction of the second	0.4	6.0 6.0		0.8 3.7	5.7	3.8 6.7	4.0	-0.2 -0.6			. P.,		***********
C3 C4	5	13.8	U	0	al and the second second	16.4	6.1			• * * * * * * * * * * * * * * * * * * *		St. St. M. W. W. Marthaller, in North Mr. W. W.	-0.0			******	· · · · · · · · · · · · · · · · · · ·	
5 5 5 5 5 5 5 S S	5.2 0	19 10	15.6	21.6		16.8			8.5 -2.3	-1.5		0 c c c c c c c c c c c c c c c c c c c	0.6	-600.0			0.211	
C5 C6	0	19 19	36.8	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		10.0	28 2 2 2 2 2 X X X X X X X X X X		-33.9			*****	0.4	1.3				*******
C7	0	19 19	30.0	accountered	****	18.9	82.1	***********	-64.3	-63.2				********		******	• • • • • • • • • • • • • • • • • • • •	* * * * * * * * * * * * * * *
C8		19 19	35.4	******		19.9	****************		-92.4	-91.5	***********	*****		. 	*******	******	********	***
C9		19	38.4	*************		21.0	z~ ~ ~ ~ <i>~ ~ ~ ~ ~ ~ ~ ~ ~ ~</i>		-124.7	-123.8				**********	งผมมหญ้ามา			****
C10		19	53.2	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		22.5	3 <i></i>	******	-169.0	-167.9		*********		~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	******	~~ \$ ~ ~ ~	* 1 ~ ~ ~ ~ ~ ~ ~ ~	
C11		19	44	***************************************	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	23.0	2		-205.2			****					• • • • • • • • • • •	**********
C12		19	54.6	***************************************	2 20 /0 /0 /0 /0 /0 /0 /0 /0 /0 /0 /0 /0 /0	23.0	****		-248.8	50 50 50 50 50 50 50 50 50 50 50 50 50 5		*****	an a		* * * * * * *	*****	* 16 * * * * * * *	****

Overall Average > 20 lbs > 50 lbs 0.41 0.43

0.44 0.38

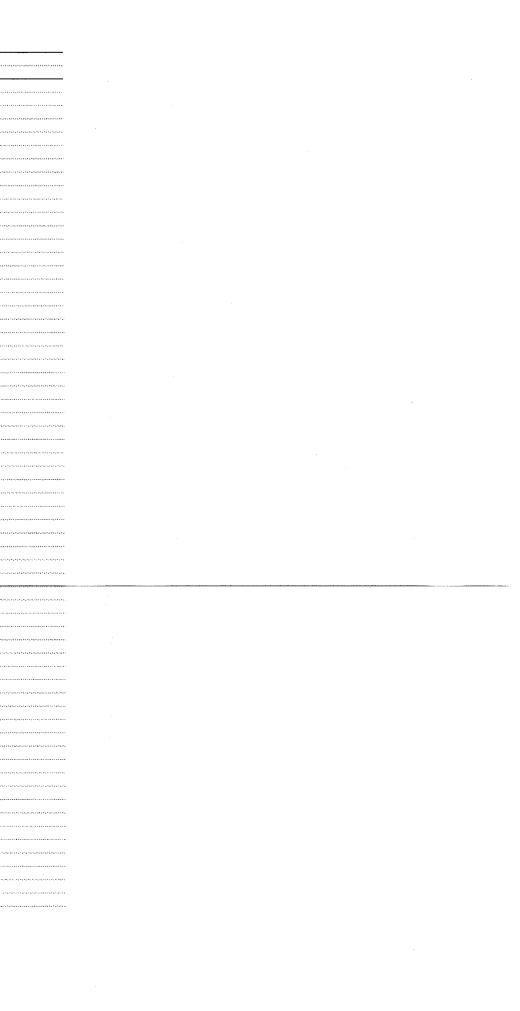
Notes
oad Cells Calibrated for these tests
e Load Cell not attached
ward Load Cell 100 Lbs eward Load Cell 300 Lbs ibal Load Cell 300 Lbs
rage % error for gimbal values, equal r greater than 20 Lbs
0.38
rage % error for gimbal values, equal r greater than 50 Lbs
0.44
t Conducted with pitch/roll lock plate attached

APPENDIX B: SECTION B RESULTS (SIDE PULL 1, 2 AND 3)

	May 19 Weights		/ Total		Load Ce	ell Reading	ıs (lbs)	Gimbal	Theoretical	Absolute	% Error	Change in Absolute	Change in %Error	S	ide Pull	Notes
******	Forward	Rearward	Side	e	Forward		Side	Reading	Reading	Error		Error Per Lbs Side Pull	per Lbs Side Pull	F12 F6	Cntr A6	5 A12
		0 No Load	0 No Load	0	0.8	1.8			1.0						X	
Pan		5 Pan 5 15.6	6 Pan 21.6 0	4	4.5	4.9 19.3	2.7 2.7	2.8 8.1	0.4		-5.5				X	
			21.6 0 21.6 19.6	23.6		19.5		8.4	6.1			a an and a second a second	0,283		X	
	0 1		21.6 8.6	32.2	13.4	19.5		a contraction of the contraction of the second			A CONTRACTOR OF				X	
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			21.6 5	50.6	13.2	19.7	43.9	8.4	6.5	0.4	6.2		0.282		Х	
			21.6 9.6	60.2	13.2	19.8	49.7		6.6				0.309		Х	
			21.6 Pan	4	13.7	19.1	3.4								X	
		5 0	21.6 9.8	13.8	13.6	19.2	11.5	8.1	5.6				0.474		X	
	a	and the second	21.6 13.4	27.2	13.4	19.4	22.2		6.0 6.4	0.1	1.7				X	
			21.6 19.6	46.8	13.2 13.2	19.6	38.3 46.8				3.1 4.6		0.302		XX	
			21.6 8.6 21.6 9.8	55.4 65.2	13.2	19.7 19.8	Chevron and the second s						0.290		x	
			13.2 Pan	4	16.2	97.1				S 3.86.			0.200		X	38.4+53.2
			13.2 19.6	23.6	15.8	97.5			81.7		PROPARATE STRATES CONTRACTOR		-0.001		X	
			13.2 13.4	37		97.8	\$xex10ex10ex10ex10ex10ex10ex	82.6	82.1	1.8			0.008		X	
			13.2 5	42		97.9	34.4	82.7	82.3						X	
			13.2 9.8	51.8		98.2			82.6						X	
			13.2 13.4	65.2		98.2			82.6				0.006		X	
		***************************************	13.2 Pan	4	16.3	95.4							0.045		X X	
			13.2 13.4 13.2 8.6	17.4 26		95.9 96.2									X	
			13.2 0.0 13.2 19.6	45.6		97.0		82.0	A CANADA CANADA CANADA CANADA CA		************************		0.023		X	
*****			13.2 9.8	55.4	15.6	97.4	3aeraaeeaaeraeeaeeae			**************************************			0.027		X	***************************************
			13.2 9.8	65.2	15.6	97.8					2.3	0.019	0.022		X	****
		15 91.4 2	04.6 Pan	4	te a ser	176.9			159.2	1.8					X	54.6 + 36.8
			04.6 5	9	17.6	176.6						a a second a second a second a second se	-0.017	E CONTRACTOR OF THE	X	
			04.6 13.4	22.4		176.7	18.2		159.1	1.7			-0.004	States and services of	*	
			04.6 8.6	31		176.9	Sale Contraction and the	······································						1	X X	
			04.6 19.6 04.6 14.6	50.6 65.2		177.5 177.7	41.6 55.9		Los and the second second		an an the second se		· · · · · · · · · · · · · · · · · · ·	1	Ŷ	***************************************
			04.6 Pan	4		178.6							0.000		X	
			04.6 13.4	17.4	All and the second second and the	179.2	Bayme to see the second second		163.7				0.006		X X	and an
	Real Contraction of the second s		04.6 8.6	26		179.7	20.8	165.6	164.3				0.010		Х	
			04.6 9.8	35.8		180.2			164.9						X	TO SCIENT SCIENT SCIENT SCIENT SCIENT SCIENT
			04.6 9.8	45.6		180.8							0.006		X	
			04.6 19.6	65.2		181.9				A COMPANY OF COMPANY			0.006		X	44.0 + 37.0
			85.6 Pan 85.6 13.4	4 17.4	16.9 16.9	254.9 254.5							0.000		X X	44.0 + 37.0
			85.6 13.4 85.6 13.6	31		254.5 254.1	25.4					***************************************			x	****
		curately accurately	85.6 19.6	50.6		253.5		*** *** ******				***************************************			X	***
*****	******		85.6 14.6	65.2		253.2									X	****
	0		85.6 Pan	4		250.0						A CONTRACT NAMES AND A CONTRACT A CONTRACTACTACTACTACTACTACTACTACTACTACTACTACTA			X	
			85.6 19.6	23.6		250.8					**********************		***************************************	e	X	
			285.6 13.4	37		251.4									X	
			285.6 13.6 285.6 9.8	50.6	A & C & C	252.0 252.4			********************************				0.010		X X	
-			285.6 9.8 285.6 4.8	60.4 65.2		252.4			235.2			***************************************			x x	***
			39.8 Pan	4		294.3							0.000		X	
		15 0 3	39.8 8.6	12.6	a second s	294.4							0.006		X	
			39.8 13.4	26	16.0	294.8	21.8	3 280.0	278.8	3 1,1	0.4	0.022	300.0		X	
	0	15 0 3	39.8 19.6	45.6	15.9	295.4	37.5								Х	
			39.8 9.8	55.4		295.4		280.9						an a	X	
_			39.8 9.8	65.2		295.3							0.002		X	
	10 7 3 14 2 3 1 3 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	a series and a series of the s	39.8 Pan	4	All and the second	292.4							0.010		X X	
			339.813.4339.89.8	17.4 27.2	· · · · · · · · · · · · · · · · · · ·	292.9 293.5						A CONTRACTOR AND A CONTRACT OF A			X	
	en e		39.8 9.6 339.8 19.6	46.8		293.3								· · · · · · · · · · · · · · · · · · ·	x	
			339.8 8.6	40.0 55,4		294.8						ter an			x	
			39.8 9.8	65.2		295.1					Selector and the second				X	
and the first of the second									Averages	1.00	1.07	0.0139	0.00809	1		

..... ****** ***** . ****** **>** ***** ***** ****** **** ***** ****** ****** ****** ***** ersore . ****

Page 2		May 19th							<u></u>							N La La Ja
Trail #			ded / Tol	tal Side		Load Ce Forward	ell Readings	(lbs) Side	Gimbal Reading	Theoretical Reading	Absolute Error	% Error	Change in Absolute Error Per Lbs Side Pull	Change in %Error per Lbs Side Pull	Side Pull F12 F6 Cntr A6 A12	Notes
	Forw No Load	0 No Load		No Load		0.8	1.8	0.3	3.3	V	2.3					
	Pan	5 Pan		Pan	4		4.9	2.7	2.8		-0.1				X	
62	Pan+5.2	10.2 Pan+15.€	21.6		4	8.6	19.3	3.7	12.9		0.1	0.9			Х	
63	0	10.2 0,	21.6	13.4	17.4	8.5	19.5	14.4	13.1	11.0	0.2	1.8	0.009	0.083	X	
64	0	10.2 0	21.6	13.4	30.8	8.5	19.7	25.4	13.3		0.2	1.8	0.005	0.039	X	
65	0	10.2 0	21.6	9.8	40.6	8.4	19.9 20.3	33.0 50.8	13.4 13.6	*******************************	0.4	3.5 5.8	0.010 0.013	0.087 0.104	X	
66 67	0; 0	10.2 0 10.2 0	21.6 21.6	19.6 5	60.2 65.2	8.3 8.2	20.3	56.6	13.0		0.7			0.104	X	
68	0	10.2 0	21.6		4	8.5	19.5	2.9	13.2		0.1	0.0		0.002	X	
69	0:	10.2 0	21.6	13.4	17.4	8.5	19.7	14.3	13.3		0.2			0.077	X	
70	0	10.2 0	21.6	10	27.4	8.4	19.8	22.2	13.5		0.2	1.8		0.044	X	
71	0	10.2 0	21.6	8.6	36	8.4	19.9	31.1	13.4		0.4			0.091	X	
72	0	10.2 0	21.6	19.6	55.6	8.3	20.2	45.2	13.7		0.5			0.078	X	
73	0	10.2 0	21.6		65.2		20.4	55.9	13.9		0.6			0.076	X	
74	0	10.2 75.2	96.8	N 1997 2012 2017 10 10 10 10 10 10 10 10 10 10 10 10 10	4	9.6	84.4	3.9	75.9 76.5					0.007	X	38.4 + 36.8
75	U	10.2 0	96.8	19.6 13.4	23.6 37		85.0 85.5	20.4 31.3	76.5		1.3 1.6		0.005	0.007	X	
76 77	0	10.2 0 10.2 0	96.8 96.8	8.6	45.6	A 1. M.	85.7	38.6	77.0		1.6	2.1	0.012	0.014	X	
78	0	10.2 0	96.8		55.4	9.4	86.1	46.4	77.2		1.8			0.017	Х	***************************************
79	0	A CONTRACTOR OF A CONTRACTOR O	96.8		65.2		86.4	53.5						0.015	Is the second s second second se second second s	***************************************
80	0			Pan	4		83.5	3.6	75.3	73.8	0.8	1.1			X	
81	0	10.2 0	96.8	13.4	17.4		84.1	13.7	75.6					0.052	X	
82	0	10.2 0	96.8		26		84.5	20.8	76.0					0.030	X	
83	0	10.2 0	96.8		35.8		84.9	28.9	76.3					0.031	X	
84	0	10.2 0			55.4		85.7 86.1	45.7 53.7	77.1	E	1.5 1.7	2.0		0.021	A S	
85	0		96.8 204.6		65.2	9.3	179.7	3.5	169.3		1.4			0.023	X	53.2 + 54.6
86 87	0		204.6		12.6		179.8	10.0	169.4	A	1.5			0.009	X	00.2 007.0
88	0	10.2 0	204.6		26		180.4	24.0	170.0		1.6			0.006	X	
89	Ō	น่างการการการการการการการการการการการการการก	204.6		45.6		181.0	37.6	170.5		1.8			0.007	X	
90	0	10.2 0	204.6		55.4		181.4	47.8	170.9		1.8			0.005	X	
91	0		204.6		65.2		181.8	54.4	171.2		2.0			0.007	X	
92	0		204.6		4	11.7	178.5	3.7			0.4	· · · · · · · · · · · · · · · · · · ·		0.000	X	
93	0	ใบการการการการการการที่ยายายายายายายายายายายายายายายายายายายา	even exercise a construction of the second	Accession and a second s	12.6		179.3	19.2	169.4		0.6			0.008		
94	0		204.6		26		180.4	36.4 42.2						0.009 0.009		
95	0		204.6 204.6		35.8 55.4		180.7 180.8	42.2 46.0						0.009		
96 97	0		204.6		65.2		181.2	-+0.0 53.6							X	
98	0	1		Pan	4		249.6	4.0						0.071		44.0 + 35.4
99	0	the state of the second st	284		23.6		250.1	19.6					0.019	0.008	a series of the	
100	0		284		32.2	11.6	250.4	26.4	239.9	238.8	1.2	0.5	0.013			
101	0	10.2 0	284		45.6		250.9	37.3	240.3		1.4	0.6	0.015			
102	0	10.2 0	284		55.4		251.2	45.0								
103	0		284		65.2		251.5	52.1						0.006		
104	0			Pan	126	· [248.5	3.5 9.9			- F			0.007	X	
105	0	and the second	10008 (P10) - An		12.6 26		248.8 249.6	22.7		And a concerning the first of the second				0.009	Construction and the construction of the co	
106	0				35.8		250.1	31.5						5 57. s		
108	0	and the second	284		55.4		250.8	45.2				0.5				
109	Ō	Contraction of the second s			65.2		251.1	52.9				5 0.6		0.008		
110	0	,		Pan	- 4		274.9	3.9	263.8	3 262.7					X	
111	0	10.2 0			17.4	***************************************	275.1	14.1	264.0							
112	0				26		275.4	20.9							X	energenergenergenergenergenergenergener
113	0	~~~~~			35.8		275.8	28.9		*******************	AND MAN CHEMICAL CHEMICAL CHEMICAL AND CAUSED	ACCOUNTS ACCOUNTS AND ACCOUNTS		7 232323023232323232323232323232323232323		********
114	0		**********************		55.4		276.6	44.7 52.5	265.4 265.6	23 NOVA28282828282828282828282828282828282828			***************************************	• VENTATION CONTRACTOR VENTATION CONTRACTOR VENTATION CONTRACTOR CONT CONTRACTOR CONTRACTOR CONT	17 กรรษรรรษรษฐ์พระกรรษรรู้ระบวจระระษฐ์เกราะระระสุจักรระระการ	
115	0				65.2		276.9	<u> </u>						0.004	X	
116	0			I Pan	23.6		273.9	3.c 20.1	*****************************	127 AVA 444 AVA 444 AVA 474 AVA 474 AVA 474 AVA		***************************************		0.007	· X	
117		ก่างการการการการสูบการการการการการการการการการการการการการก	5		23.0 33.4		274.0	20.1 27.5				*** ******************************		The second se		***************************************
119			*******************				275.6	34.2								
120			S ** ** ** ** ** *** ** ** ** **		55.4		276.2	45.7						0.008		
121	Ő				65.2		276.6	53.2		***						
		· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·							Averages	1.10	1.33	0.0148	0.02417		



Page 3		ay 19th ghts (lbs) Addeo	d / Total	Load C	ell Readings	(lbs) I	Gimbal	Theoretical	Absolute	% Error	Change in Absolute Error	Change in %Error	Side Pull	Notes
#	Forwa	rd Rearwar	d Side	Forward	Rearward	Side	Reading	Reading	Error (lbs)		Per Lbs Side Pull	Per Lbs of Side Pull	F12 F6 Cntr A6 A12	
	No Load	0 No Load	0 No Load	0 0.8	1.8	0.3	<u>3.3</u> 2.8		2.3					
2	Pan Pan +5.2	5 Pan 10.2 Pan + 15	6 Pan 21.6 Pan	4 4.5 4 8.5	4.9	2.7			-0.1			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	X	
123	0	10.2 0	21.6 9.8 1	3.8 8.4	18.9	11.9				-1.0	0.011	0.105	X	
124	0	10.2 0		2.4 8.4	18.9	17.2	12.9				0.007	0.067	X	
125 126	0. 0	10.2 0 10.2 0		5.8 8.3 5.6 8.2	19,1 19,2	29.1 38.2	12.8 12.9		0.3	2.8 3.6	0.019 0.017	0.177 0.156	X X	******************
120	0	10.2 0		5.2 8.1	19.4	55.6	12.9			6.2	0.017	0.153	a a the second of the second se	***************************************
128	0	10.2 0	21.6 Pan	4 8.4	18.8	4.2							X	***************************************
129	0	10.2 0	21.6 19.6 2	3.6 8.3 2.2 8.2	18.9 19.0	19.7 26.1	13.0 12.9		//////////////////////////////////////	been a second	0.013	0.125	X	
130 131	0	10.2 0 10.2 0		2.2 8.2 42 8.2	19.0	36.5	12.9		0.2			0.202	a second a second second a second	
132	0	10.2 0		5.4 8.1	19.3	46,4	12.9	11,2	0.6	5.4	0.021	0.195	X	
133	0	10.2 0		5.2 8.1	19.4	53.4	12.9			······		0.185		*****
134	0	10.2 54.2 10.2 0	75.8 Pan 75.8 19.6 2	4 9.6 3.6 9.5	68.2 68.8	3.8 23.6	60.0 60.5		0.9 1.1			0.016	X	
136	0	10.2 0	75.8 9.8 3	3.4 9.4	69.0	27.6	60.4	59.6	1.5	2.5	0.025	0.041	X	*********
137	0	10.2 0		3.2 9.4	69.3	37.2	60.7			2.5	0.018	0.029	X	
138	0	10.2 0; 10.2 0;		1.8 9.4 5.2 9.3	69.5 69.9	43.4 55.0			1.5 1.7			0.024 0.025	X	C220C122C128E<220C182EC182C182EC182EC182EC182EC182EC182EC
139		10.2 0	75.8 Pan	4 9.6	67.7	3.6	59.7	58.1	0.7	1.2		0.020	X	
141	0	10.2 0	75.8 13.4 1	7.4 9.5	68.1	16.0	60.1		0.8	1.4	0.008	0.013		
142 143	0	10.2 0 10.2 0	75.8 8.6 75.8 19.6 4	26 9.5 5.6 9.3	68.4 69.2	22.9 41.5						0.026 0.025		•>><<>>><<>>><<>>><<>>><<>>><<>>><<>>>
143	0	10.2 0		5.4 9.3	69.5	47.3					0.021	0.023		*****
145	0;	10.2 0	75.8 9.8 6	5.2 9.3	69.7	55.8	61.2	60.4	1.5	2.5		0.024	X	
146	0	10.2 72.2		4 11.2 2.6 11.1	128.3 128.5	3.9 9.7			1.3 1.4			0.014	X	36.8 + 35.4
147 148	0	10.2 0 10.2 0		2.6 11.1 26 11.0	120.0	22.5							I water the second state of the second state of the second	****
149	0	10.2 0 10.2 0	148 9.8 3	5.8 10.9	129.2	29.9	118.9	118.3	1.7	1.4	0.015	0.013	X	
150	0	10.2 0		5.4 10.8	130.0	47.5 57.0						0.011	A Construction Construction of the second difference in the second difference of the second diff	
151 152	0	10.2 0 10.2 0	148 9.6 148 Pan	65 10.7 4 11.2	130.3 127.5	3.7						0.003	X	4 1 4 7 4 7 4 7 4 7 7 7 7 7 7 7 7 7 7 7
153	0	10.2 0	148 13.4 1	7.4 11.1	128.0	13.6	118.3	116.9	0.9	0.8	0.020		Х	***************************************
154	0	10.2 0	148 8.6	26 11.0	128.3	20.8			and the second se					
155 156	0	10.2 0 10.2 0		5.8 11.0 5.4 10.8	128.7 129.5	29.4 46.2						0.018		***************************************
157	Ő	10.2 0	148 9.8 6	5.2 10.8	130:2	59.6	119.8	119,4	1.9	1.6	0.021	0.018	X	
158	0		255.8 Pan	4 12.0	221.5	4.1	210.4					0.002	X	53.2 + 54.6
159	0	*********************	255.8 19.6 2 255.8 13.4	3.6 11.9 37 11.8	222.0 222.5	20.0 30.6	***************************************	210.1 210.7	1.3 1.4		-0.006 0.000	-0.003 0.000	***************************************	
161	0			5.6 11.7	222.9	40.6	212.0	211.2					X	
162	0	· < = > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × < > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 < × > 0 <		5.4 11.7	223.3	48.0	212.3					• • • • • • • • • • • • • • • • • • •		
163	0		255.8 9.8 6 255.8 Pan	5.2 <u>11.6</u> 4 12.1	223.5 220.5	<u>55.2</u> 3.6	212.6 210.4					0.002		
165	0	10.2 0	255.8 9.8 1	3.8 12.0	220.9	11.9	210.7	208.9	0.5	0.2	0.024	0.011	X	
166	0	10.2 0		3.4 11.8	221.8	28.3	211.3							
167				6.8 11.7 5.4 11.6	222.3 222.9	38.3 49.3	211.7 212.2	210.6 211.3						
169	0	10.2 0	255.8 9.8 6	5.2 11.6	223.3	56.2	212.4	211.7	1.6	0.8	0.025		X	****
170	0	10.2 82.4		4 12.4		4.4						0.000	X	44.0 + 38.4
171 172	0		338.2 19.6 2 338.2 13.4	3.6 12.2 37 12.1	288.6 289.0	19.4 30.6								
172	a la construction de la construc		338.2 8.6 4	5.6 12.1		40.1		277.2	1.4	0.5	0.006			
174	0	10,2 0	338.2 9.8 5	5.4 12.1	289.5	46.8	278.2	277.4	1.5	0.5	0.007	0.002		
175	0	10.2 0	338.2 9.8 6 338.2 Pan	5.2 12.1 4 12.5	289.5 286.5	53.3 4.1						0.001	X	
176 177	0	10.2 0 10.2 0		4 12.5 2.6 12.4		10.0						0.006		
178	0	10.2 0	338.2 13.4	26 12.3	287.5	21.9	276.8	275.2	0.7	0.3	0.017	0.006	X	
179	0			5.8 12.2		29.7 45.0								
180 181	0	10.2 0 10.2 0		5.4 12.1 5.2 12.1		45.0 55.1								**************************************
L								Averages						

