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Publisher's version / Version de l'éditeur:

https://doi.org/10.4224/20358623

Technical Report (National Research Council of Canada. Division of Building Research), 1951-02-01

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NATIONAL RESEARCH COUNCIL



OVERALL HEAT
TRANSMISSION COEFFICIENTS

OF
BUILDING SECTIONS

ANALYZED

BY

A. D. KENT AND H. L. HALL

FEBRUARY 1951

National Research Council

Division of Building Research

TECHNICAL REPORT NO. 7

OF THE

DIVISION OF BUILDING RESEARCH
OTTAWA

DBR NO. 16

PRICE 25 CENTS

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OVERALL HEAT TRANSMISSION COEFFICIENTS OF BUILDING SECTIONS

The tables which follow have been prepared to indicate the "overall heat transmission coefficients" of a wide range of wall, floor and ceiling constructions, for home-owners and builders. Following the tables formulae and technical data are provided for the use of architects, engineers and contractors.

The "overall heat transmission coefficient" (U value), indicates the amount of heat passing through I square foot of the building section, in I hour, when there is a I degree temperature difference between one side of the section and the other. The lower the 'U' value, the better is the heat insulating property.

cular building section will conduct heat. Thus they provide a means of comparing its heat insulating property with those of other building sections. The values given in the tables have been calculated on the basis of materials applied in an ideal manner. Thus, if the same values are to be obtained in practice, great care must be taken in the application of the insulation.

A knowledge of the heat insulating properties of building sections enables one to provide for ease and economy of heating, and comfort, by the selection of proper materials. 'U' values will permit the heating contractor to provide for the supply and proper distribution of heat to all parts of a building.

It is not always possible to state definitely what 'U' values should be provided. Climate, and construction and fuel costs vary across the country and these all have a bearing on the selection of an economical 'U' value. However, it is generally recommended that building sections should have 'U' values of 0.15 or less (CMHC Building Standards). In all cases this will require the use of insulating material, in some form, in addition to the materials normally used to provide strength, and inside and outside finish.

The tables provided cover most of the combinations of building materials normally encountered. They do not provide all the data that are required for the calculation of the heat loss from buildings. Heat losses through windows and doors, and by the exchange of inside and outside air through cracks around windows and doors, must also be considered in the calculation of total heat losses from buildings. This is a task which requires experience and special technical knowledge.

HOW TO USE THE TABLES

1. For Walls

Two series of tables are provided for both wood-frame and masonry wall sections.

The first series in each case gives 'U' values for wall sections which have no insulation between the stude or furring strips. Thus these may be used directly where insulation is not placed in air spaces in the walls.

The second series in each case gives 'U' values for walls with varying amounts of insulation between studs or furring strips. To use this series of tables it is first necessary to find the 'U' value provided by the basic materials of the wall, i.e., those materials which provide strength, and interior and exterior finish, from the first series. The value thus found is used as a key to the tables in the second series.

It is important in the use of the tables to follow the procedure outlined in the following example.

Example 1 Problem:

To find the 'U' value of a wall consisting of wood lap-siding, sheathing paper, 3/4" rigid insulation-board sheathing, 2 x 4 studs, and 3/8" gypsum lath and plaster. Solution:

Refer to tables for frame-walls with no insulation between studs; either table WFl(a) or WFl(b). The type of siding used determines which table applies (in this case wood lap-siding). Thus refer to table WFl(b) as it has, under the heading "exterior finish" a subdivision for wood lap-siding. (See portion of table below).

Beginning in the left-hand column follow across the appropriate horizontal line as indicated by the type of sheathing material in the column headed "sheathing" (in this case 3/4" rigid insulation board). Continue into the column headed "interior finish", and select the type of finish which applies (in this case 3/8" gypsum lath and plaster). The number, 0.19, in the square under the specified interior finish is the 'U' value desired.

FRAME W	ALLS NO INSULATION BET					*U	*							۴.			
XTERIOR FINISH	SHEATHING					IN'	ER	101	2	F	INI	SH					
PLY WOOD SIDING	* WITH ALL SHEATHINGS EXCEPT 17:30" WOOT SHEATHING, HOETICOHTAL FORZING EXTERIOR FINISH, THE AIR SPACE THUS FORMET HAS BEEN INCLUTED IN THE EXCEPT. "NOOP SHINGLES" ENTEROR FINISH. O POR SRICK VENEERS THE AIR SPACE BETWEEN VENEERS AND SHEATHING MAS NOT BEEN INCLUTED IN THE CALCULATION """ "VALUES."	36 GYPSUM BOARD	12 GYPSUM BOARD	12" RIGID INSULATION BOARD	34" RIGID INSULATION BOARD	1 GIGID INSULATION BOARD	14 PLYWOOD	3% PLYWOOD	36 GYPSUM LATH, 1/2 PLASTER	METAL LATH, 34 PLASTER	WOOD LATH, 34" PLASTER	1/2 INSULATION BOARD LATH, 1/2 PLASTER	34 INSULATION BOARD LATH, 1/2 PLASTER	I' INSULATION BOARD LATH, 1/2 PLASTER	FOIL BOARD, REFLECTIVE INTERIOR SIDE	FOIL BOARD, REFLECTIVE BOTH SIDES	INCH ATTIMO from paccess) 3/4 GVD LATE 1/6 DI ACT
- Frue					INS		7101	VU	£	TABL		VF. 2 VF. 3		2b) or	6	CON	
	3/8" PLY VOOD SIDING	.41	.40	27	-23	19	.40	38	.39	.42	.39	.26	,22	.19	32	.25	
	19 PLY WOOD SIDING	-39	-37	26	-22	-19	.38	36	36	39	-37	.25	.21	.18	.51	.24	
WOOD LAP	BUILDING PAPER ONLY	34	-33	24	-20	.18	.34	.32	.33	.35	.33	.23	.20	.17	-28	.22	Ţ.
SIRING	12 GYPSUM BOARD & BUILDING PAPER	.31	.30	.22	-19	.17	-30	.29	129	.31	.29	.21	ا8،	.16	.26	.20	ŀ
WYER OR	5/16 PLYVOOD &	30	-29	.22	-19	-16	.30	.26	.29	- 31	.29	.21	-18	-16	-25	-20	1
_ I Feet	25/2" WOOD SHEATHING &	26	-25	19	-17	.15	-25	.24	.25	.76	.25	.19	.17	-15	-22	-18	I
· Selima	12" RIGID INSULATION BOARD & BLOG PAPER	.23	-22	-18	-16	.14	182	-7		23	.22	-17	.15	.14	.20	.16	
H Tarks	34 RIGID INSULATION BOARD &	19	.19	.16	.14	-13	19	×(.	19	1)0	-19	-15	-14	-12	-17	:14	
SHEATHINE	I RIGID INSULATION BOARD &	.17	-17	.14	-13	11	167	. 6		.17	-16	.14	.12	.11	.15	-13	1

HOW TO USE THE TABLES

Example 2 Problem:

To find the 'U' value of a wall which has the same basic materials as the wall described in Example 1 but, in addition, the wall has 2 inches of insulation having a 'k' value" of 0.27. Solution:

The first step is to find the 'U' value of the wall without any insulation. This has been done in Example 1 and the 'U' value

was found to be 0.19.

The second step is to select one of the tables (WF2(a), (b) or (c)) which apply to wood-frame walls having mass insulation between the studs. In this case the insulation used has a 'k' value of

0.27. Therefore Table WF2(b) applies.

Beginning at the top of the table, select the type of installation which is proposed, as indicated by the sketches. Under the sketch pick out the vertical line of figures which applies to the thickness of insulation to be used. Continue down this column until it intersects the horizontal line which has the 'U' value of the wall without insulation in the extreme left-hand column. In this case the insulation is to be installed as indicated in the first sketch. Then proceed down the column headed 2", to the horizontal line which has 19 in the extreme left-hand column. The figure .08 which occurs at the intersection of these two lines is the 'U' value of the insulated wall. (See portion of table below).

FRAME						SION (VF 2	
				T	HERMA	L CON	PUCT	IVITY	of INSULATION	k:	27	
COEFFICIENT WITH NO INSULATION BETWEEN STUPS.	AGA! WITH LEA!	NST E	AIR S	SIDE	AT	BATT SEPA AIR S	PACLS EAST	TERED, TWO LACH	BLANKETS BATTS OR FILL; NO AIR SPACE. INSULATION	CENTE	BACH RIOR F KETS O LREP, ST AIR SP AT LE	R BATTS PARATIN AGES
THICKNESS -	1	1/2	2"	24	3"	1	1/2	2"	338	1"	11/4"	2"
- 11	.08	-07	.06	.06	.05	.07	.07	.06	.05	.07	-07	.06
.12	.08	.07	.07	.06	.06	.08	.07	.06	.05	.08	.07	.06
. 13	.09	-08	.07	.06	.06	.08	.07	.07	.06	.08	.07	.07
.14	.09	-08	.07	.07	.06	. 09	,08	.07	.06	.09	.08	.07
-15	.10	.08	.08	.07	.06	.09	.08	.07	.06	.09	.08	.07
.16	.10	.09	.08	_07	.06	.09	.08	.07	.06	.09	.08	.07
.17	-10	.09	08	.07	.07	.10	.09	-08	.06	.10	.09	.08
.18	.11	109		-07	.07	.10	.09	.08	.06	-10	.09	.08
.19	.11	.10	(.08)	.08	.07	.10	.09	.08	.07	.10	.09	.08
.20	.17	10	Y	.08	.07	.H.	.09	.08	.07	.11	.09	.08

Note: Tables are provided for mass insulation having 'k' values of 0.24, 0.27 and 0.30. The 'k' value is the amount of heat (B.t.u.) which will pass through I square foot of a 1-inch thick sample of the insulation in I hour, when there is a I degree temperature difference between one side of the sample and the other. 'k' values are determined by laboratory test and may be obtained from technical publications, universities and testing laboratories. Tables are also provided for reflective insulations, giving 'U' values based on an emissivity of .05, an inside design temperature of 70°F. and an outside design temperature of -10°F. The 'U' values given in the tables may be applied to outside design temperatures in the range -30°F. to 10°F. without appreciable error.

How to Use the Tables

2. For Floors

Two tables are provided giving 'U' values for various combinations of materials which are commonly used in floor construction. Table Fl covers the case where there is no finish applied below the floor joists and table F2 applies to the case where either ½" plywood or ½" insulation board is used as a finish on the underside of the floor joists. Unlike the tables provided for walls, each of these tables is complete in itself, and 'U' values may be found directly by comparing a particular combination of materials with those given in the tables.

3. For Ceilings

As with floors, two tables are provided. Table Cl covers the case where there is no finish above the ceiling joists, and Table C2 applies to the case where 25/32" wood flooring is applied on the top side of the ceiling joists. "U" values may be found directly from each table.

Symbols for Reflective Insulation

Indicates a curtain having one reflective surface.

Indicates a curtain having both sides reflective.

FRAME W	ALLS NO INSULATION BET					*U 'S								F.			
EXTERIOR FINISH	SHEATHING					INT	TER	HOR	2	F	111	SH					
SIDING SIDING INTERIOR PINISH STUD SHEATHING INTERIOR PINISH STUD METAL LATH INTERIOR FINISH STUD STUD METAL LATH	** WITH ALL SHEATHINGS EXCEPT 25/32 WOOD SHEATHING, HORIZONTAL FURRING STRIPS ARE USED FOR SHINGLE. EXTERIOR FINISH. THE AIR SPACE THUS FORMED HAS BEEN INCLUDED IN THE CALCULATION 9 "II" VALUES GROUPED BESIPE "ASBETTOS SHINGLES" EXTERIOR FINISH. • FOR BRICK AND STONE VENEERS, THE AIR SPACE AND MORTAR BETWEEN VENEER AND SHEATHING HAVE NOT BEEN INCLUDED IN THE CALCULATION 9" "I" VALUES, SINCE THE ADPITIONAL RESISTANCE IS CONSIDERED UNIMPORTANT.	% GYPSUM BOARD	1/2" GYPSUM BOARD	1/2" RIGID INSULATION BOARD	34" RIGID INSULATION BOARD	" RIGID INSULATION BOARD	14. PLYVOOD	% PLYWOOD	36 GYPSUM LATH, 1/2 PLASTER	METAL LATH., 34" PLASTER	VOOD LATH, 3/4" PLASTER	12" INSULATION BOARD LATH, 12" PLASTER	34" INSULATION BOADD LATH, 1/2" PLASTER	I" INSULATION BOARD LATH, 1/2" PLASTER	FOIL BOARD, REFLECTIVE INTERIOR SIDE	FOIL BOARD, REFLECTIVE BOTH SIDES	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
BLDG. SHEATHING					INSU	ULAT.		USE	- TA	BLL		F. 2 ((a), (k	o), or	(c)	. 4A	
I/C =a.casas	BUILDING PAPER ONLY	.46			.24	.20	.45	40	42	47			04	00	20		-
TEMPERED PRESSED WOOD	1/2"GYPSUM BOARD & BUILDING PAPER			_			1	.42	.43	.47	.44	.28	.23	.20	.36	.26	3
SIDING	E / #	.40	.39	.27	.22	.19	.39	.37	.38	.40	.38	.26	.21	.18	.32	.24	.2
LINTERIOR	25/32" WOOD SHEATHING &	.39	.38	.26	.19	.17	.39	.37	.37	.40	.38	.25	.21	.18	.31	.24	
APER,	2" RIGID INSULATION BOARD & BLDG PAPER	.32	.27	.23	.18	.16	.31	.26	.30	.32	.31	.22	.19	-17	-	.21	1
HEATHING	34" RIGID INSULATION BOARD & " "		-										.17	.15	.23	.18	1
	" RIGID INSULATION BOARD & " "	.19	.22	.16	.16	.14	.19	.22	.19	.23	.22	.17	.15	.14	.20	.16	
SBESTOS SHINGLES	BUILDING PAPER ONLY	.31	.30	.22	.19	.17	.31	.29	.30	.31	.30	.22	.19	.16	.26	.20	
*	1/2" GYPSUM BOARD & BUILDING PAPER	.28	.27	.21	.18	.16	.28	.26	.27	.28	.27	.20	.17	.15	.24	.19	
401 11	5/16 PLYWOOD & " "	.28	.27	.21	.18	.16	.27	.26	.27	.28	.27	.20	.17	.15	.23	.18	
IN ERIOR	25/32 WOOD SHEATHING & " "	.30	.30	.22	.19	.17	.30	.29	.29	.31	.29	.21	.18	:16	.25	.20	
APER - STUD	1/2" RIGID INSULATION BOARD & B'LD'G. PAPER	.21	.21	.17	.15	.13	.21	.20	.20	.21	.21	.16	-15	.13	.19	.15	
III II	34" RIGID INSULATION BOARD & # #	.18	.18	.15	.13	.12	.18	.18	.18	.18	.18	.15	.13	.12	.16	.14	
SHEATHING'	1" RIGID INSULATION BOARD &	.16	.16	.13	.12	-11	.16	.16	.16	.16	.16	.13	.12	.11	.14	.12	
4 FACE 0	BUILDING PAPER ONLY	.39	.38	.26	.22	.19	.38	.36	.37	40	.37	.25	.21	.18	.31	.24	5
BRICK VENEER	1/2" GYPSUM BOARD & BUILDING PAPER	.34	.33	.24	.20	.18	.34	.32	.32	.35	- 1	-	.20	.17	.28	.22	-
SHEATHING	5/6 PLYWOOD &	.34	.33	.24	.20	.17	.33	-32	.32	.34	.32	.23	.20	.17	.28	.21	
STUD	25/32 WOOD SHEATHING &	.28	.27	.21	.18	.16	.28	.27	.27	.28	.27	.20	81.	.15	.24	.19	
INTERIOR	1/2" RIGID INSULATION BOARD & B'LD'G. PAPER	.24	.24	.19	.16	.15	.24	.23	.24	.25	.24	.18	.16	.14	.21	.17	
BLDG. PAPER	3/4" RIGID INSULATION BOARD & # *	.21	.20	.16	.15	.13	.20	.20	.20	.21	.20	. 16	.14	.13	.18	.15	
	1" RIGID INSULATION BOARD &	.18	.18	.15	.13	.12	.18	.17	.17	.18	.17	.14	.13	.12	.16	.13	
						_											
6" STONE 0	BUILDING PAPER ONLY	_	- 1				_		.36	-	-		1	.18	-	.23	
BLPG. PAPER	1/2 GYPSUM BOARD & BUILDING PAPER		.33	.24		.17	_	-	-		-	-	-	-	.28		
STUD	5/6 PLYWOOD &		-	.23		.17	-	-	.32		.32	-	-		.27		
INTERIOR	25/32" WOOD SHEATHING & " "		-	.21		-		-		.28	-		-	-	.24	.19	
N FINISH	1/2" RIGID INSULATION BOARD & BLDG, PAPER 3/4" RIGID INSULATION BOARD & # #		.24			.14	-	-	.23		-	-			-		. !
	3/4 RIGID INSULATION BOARD & # #		20		-	.13		-	-	.21	.20	-	-		-	-	.1
	RIGID INSULATION DOAKD &	.18	-17	.15	.13	.12	.18	.17	.17	.18	.17	· 14	.13	-12	.16	.13	

EXTERIOR FINISH	SHEATHING					_					_	_	_		_	_	_
					2.	INT	ER	101	2	F	INI	SH			A		
PLY WOOD SIDING	* WITH ALL SHEATHINGS EXCEPT 25/32" WOOD SHEATHING, HORIZONTAL FURRING STRIPS ARE USED FOR SHINGLE EXTERIOR FINISH. THE AIR SPACE THUS FORMED HAS BEEN INCLUDED IN THE CALCULATION -/ "I" VALUES GROUPED BESIDE "WOOD SHINGLES" EXTERIOR FINISH. • FOR BRICK VENEERS THE AIR SPACE BETWEEN VENEER AND SHEATHING HAS NOT BEEN INCLUDED IN THE CALCULATION -/ "I" VALUES, SINCE THE ADDITIONAL RESISTANCE IS CONSIDERED UNIMPORTANT.	36 GYPSUM BOARD	1/2 GYPSUM BOARD	1/2" RIGID INSULATION BOARD	34" RIGID INSULATION BOARD	I" RIGID INSULATION BOARD	14" PLYWOOD	36" PLYWOOD	36" GYPSUM LATH, 1/2" PLASTER	METAL LATH, 34" PLASTER	WOOD LATH, 34" PLASTER	1/2 INSULATION BOARD LATH, 1/2 PLASTER	34"INSULATION BOARD LATH, 1/2" PLASTER	I" INSULATION BOARD LATH, 12 PLASTER	FOIL BOARD, REFLECTIVE INTERIOR SIDE	FOIL BOARD, REFLECTIVE BOTH SIDES	EALL BACKED 3/" GYP LATE 1/" PLASTED
FINISH		FOR	MA 2 RE	SS	INS	ULA	7101	V U	SE	TABL		VF.2 VF.3		b),01	(c)	3 C	
BUILDING	3/8" PLY WOOD SIDING & B'LD'G. PAPER	.38		.26			.38	.35	.36	20	.36		.21	.18	.31	.23	-
• 4 6-7-19	3/8 PLYWOOD SIDING & B'LD'G PAPER 1/2" PLYWOOD SIDING & B'LD'G PAPER	.36	- 1	.25		.18	.36		.34		.34	-	.21	.18	.30	.23	-
2000-200-	72		100				1	.55		-1	- 1						
W005 115	BUILDING PAPER ONLY	.34	.33	.24	.20	.18	.34	.32	.33	.35	.33	.23	.20	.17	.28	.22	1.
WOOD LAP	1/2" GYPSUM BOARD & BUILDING PAPER	.31	.30	.22	.19	.17	.30	.29	.29	.31	.29	.21	.18	.16	.26	.20	
INTERIOR	5/6 PLYVOOD &	.30	.29	.22	.19	.16	.30	.28	.29	.31	.29	.21	.18	.16	.25	.20	
FINISH	25/32" WOOD SHEATHING &	.26	.25	.19	.17	.15	.25	.24	.25	.26	.25	.19	.17	-15	.22	.18	
Builping	1/2" RIGID INSULATION BOARD & BLOG PAPER	.23	.22	.18	. 16	.14	.22	.22	.22	.23	.22	.17	.15	.14	.20	.16	
PAPER	3/4" RIGID INSULATION BOARD & " "	.19	.19	.16	.14	.13	.19	.19	.19	.19	.19	.15	.14	.12	.17	.14	
SHEATHING	I" RIGID INSULATION BOARD &	.17	.17	.14	.13	.11	.17	.16	.16	.17	.16	.14	.12	.11	.15	.13	.1
		0.5	0.5	00	1.2	l e	04	ar	0.5	04	05	10		1.5	00	10	T
WOOD SHINGLES	BUILDING PAPER ONLY	.26	.26	.20	.17	.15	.26	.25	.25	.26	.25	.19	.17	.15		.18	٠
INTERIOR	1/2" GYPSUM BOARD & BUILDING PAPER 5/16" PLYVOOD & " "	.24	.23	.18	.16	.14	.24	.23	.23	.24	.23	.18	.16	.14	.21		-
PINISH		.24	.23	.18	.16	.14	.23	.23	.23	.24	.23	.18	.16	.14	.21	-	1
SHEATHING	25/32" WOOD SHEATHING & " " 1/2" RIGID INSULATION BOARD & BLDG. PAPER	.26	.25	.19	.17	.15	.25	.24	.25	.26	.25	.19	.17	.15		.18	1
BUILDING	34" RIGID INSULATION BOARD & " "		.16	-			-	-		-				-	-		٠
PAPER	I RIGID INSULATION BOARD &	.15	-	.12				.14								.11	1
1.0									7					Y.			_
4° COMMON O	BUILDING PAPER ONLY	.34	.33	.24	.20	.18	.34	.32	.32	.34	.33	.23	.20	.17	.18	.22	Γ.
4 COMMON BRICK VENEER	1/2" GYPSUM BOARD & BUILDING PAPER	.30						.29			.29	-		.16	.25	-	٠
INTERIOR	5/6 PLYWOOD & .	.30		_	.19	-		.28			-		.18	.16	.25	.20	1
AN PENISH	25/32" WOOD SHEATHING & " "	.26	-	-			.25		.25	-	.25			.15	-	.18	+
STUD	1/2" RIGID INSULATION BOARD & BLDG. PAPER	.22		_	.15		.22		.22	-	.22		.15	.14		.16	+
SHEATHING	3/4" RIGID INSULATION BOARD & .	.19	.19		-		.19	-	.19			.15	.14	.12	.17	.14	
BLOG. PAPER	I" RIGID INSULATION BOARD &	.17	.17	.14	.13			.16	.16	.17	.16	.14	.12	II.	.15	.13	
A STATE OF THE STA							31								79		
NSULATED SIDING	BUILDING PAPER ONLY	.29	.29	.21	.18	.16	.29	-28	.28	.30	.28	.21	.18	.16	.25	.19	
MITATION BRICK)	1/2" GYPSUM BOARD & BUILDING PAPER	.26	.26	.20	.17	.15	.26	.25	.26	.27	.26	.19	.17	.15	.23	.18	
INTERIOR INTERIOR	5/16" PLYWOOD & " "	.26	.26	.20	-17	.15	.26	.25	.25	.26	.25	.19	.17	.15	.22	.18	
STUP	25/32" WOOD SHEATHING & " "	.23		-		.14	-	-	-			,	.15	.14	.20	.16	
SHEATHING	7.4	.20	.20	.16	.14	.13	.20	.19	.20	.20	.20	.16	.14	.13	.18	.15	
	34" RIGID INSULATION BOARD & " "	18	.17	14	.13	12	-17	17	.17	.18	1.00	.14	.13	.12	.16	.13	

FRAME		ALL:					ON C	, .		,	"U"			BLE / F. 2	
					HERM		_	DUCT		_	INSULAT	ON	k = .		- 2017
COEFFICIENT WITH NO	AGAI	ikets nst e one	ITHER	SIDE	,		BATTS SEPARAIR SI	KETS CENTRATING PACES,	TWO EACH		BLANKETS BATTS OR FILL; NO AIR SPACE. INSULATION		BLAN CENTE	BACK RIOR F KETS O RED, SE AIR SP. AT LE	PARATI
INSULATION BETWEEN STUPS.		SPACE		INTER			INSUL		SPACES		EXT. INT.		INSUL- ATION.		SPACE
HICKNESS 4	1"	11/2"	2"	2 1/2"	3"		1"	1/2"	2"		3 1/8"		1"	1/2"	2"
-11	.08	.07	.06	.06	.05	1	.07	.06	.06		.05		.07	.06	.06
.12	.08	.07	.06	.06	.05	1	.08	.07	.06		.05		.08	.07	.06
.13	.09	.08	.07	.06	.06		.08	.07	.06		.05		.08	.07	.06
.14	.09	.08	.07	.06	.06		.08	.07	.07		.05		.08	.07	.07
.15	.09	. 08	.07	.06	.06		.09	.08	.07		.06		.09	.08	.07
.16	.10	.08	.07	.07	.06		.09	.08	.07		.06		.09	.08	.07
.17	.10	.09	.08	.07	.06		.09	.08	.07		.06		.09	.08	.07
.18	.10	.09	.08	.07	.06		.10	.08	.07		.06		.10	.08	.07
.19	.11	.09	.08	.07	.07		.10	.09	.08		.06		.10	.09	.08
.20	.11	.09	.08	.07	.07		.10	.09	.08		.06		.10	.09	.08
. 21	.11	.10	.08	.07	.07		.11	.09	.08		.06		.10	.09	.08
. 22	.12	.10	.08	.08	.07		-11	.09	.08		.06		- 11	.09	.08
. 23	.12	.10	.09	.08	.07		-II-	.09	.08		.06		-11	.09	.08
.24	-12	.10	,09	.08	.07		.11	.10	.08		.07		-11	.09	.08
.25	.12	. 10	.09	.08	.07		-11	.10	.08		.07		-11	.10	.08
. 26	.13	. 11	.09	.08	.07		.12	.10	.09		.07		.11	.10	.09
.27	-13	. 11	.09	.08	.07		.12	.10	.09		.07		.12	, 10	.09
.28	.13	so 11	.09	.08	.07		.12	.10	.09		.07		. 12	. 10	.09
.29	-13	.11	.09	.08	.08		.12	.10	.09		.07		.12	.10	.09
.30	.14	.11	.09	.08	.08		.12	. 10	.09		.07		.12	.10	.09
.31	.14	. 11	.10	.08	.08		.12	.10	.09		.07		.12	.10	.09
.32	.14	-1Ī	.10	.09	.08		.13	:11	.09		.07		.13	.10	.09
.33	.14	.12	.10	.09	.08		.13	-11	.09		.07		.13	.11	.09
.34	.14	. 12	.10	.09	.08		. 13	-11	.09		.07		.13	. 11	.09
.35	.14	.12	-10	.09	.08		.13	-11	.09		.07		.13	.11	.09
.36	-15	.12	. 10	.09	.08		.13	.11	.09		.07		NO	TE:	1157
-37	- 15	.12	.10	.09	.08		.13	-11	.10		.07		NO	1 6	
.38	.15	.12	.10	.09	.08		.13	H	.10		.07		USE	THI	5
.39	. 15	.12	.10	.09	.08		. 14	пΠ	.10		.08		COLI	MN	WITH
.40	. 15	.12	.10	.09	.08		.14	-11	.10		.08		THE	LAST	TWO
.41	.15	.12	.10	.09	.08		.14	:11	.10		.08		COLL	MNS	of
. 42	.16	.12	.10	.09	.08		.14	-11	.10		.08		TABL	ES	
.43	.16	.12	.11	.09	.08		.14	.12	.10		.08		WF.	(a) At	ND (b)
.44	.16	.13	.11,	.09	.08		.14	.12	.10		.08		ONL	Y.	
.45	.16	.13	.11	.09	.08		.14	.12	.10		.08				-
.46	.16	.13	.11	.09	.08		.14	.12	.10		.08		1		
.47	.16	.13	.11	.09	.08		.14	.12	.10		.08				
.48	.16	.13	.11	.09	.09		.15	.12	.10		.08				
.49	.16	.13	.11	.10	.09		.15	.12	.10		.08				
.50	.17	.13	.11	.10	.09		.15	.12	.10		.08				

FRAME		LL F		. ,					FICIE BET					F. 2	
					HERM				IVITY	_	F INSULAT	ION	k : .		<u>(~)</u>
*				TTS PL		Т	_	NKETS			BLANKETS		FOIL	BACI	
COEFFICIENT WITH NO				SIDE			SEPA AIR S	RATING	. EACH		BATTS OR FILL; NO AIR SPACE.		BLANT	REP. SE	R BATTS PARATING ACES AST 3/4
INSULATION BETWEEN STUDS.		SPACE	+ -	INSUL			INSUL ATION (EXTERI		SPACES	124	EXT. INT.		INSUL-		SPACES
THICKNESS +	- 1"	11/2"	2*	21/2"	3"		1"	1/2"	2"		35/8"		1"	11/2"	2"
.11	.08	.07	.06	.06	.05		.07	.07	.06		.05		.07	.07	.06
.12	.08	.07	.07	.06	.06		.08	.07	.06		.05		.08	.07	.06
- 13	.09	.08	.07	.06	.06	1	.08	.07	.07		.06		.08	.07	.07
.14	.09	.08	.07	.07	.06		.09	.08	.07		.06		.09	.08	.07
. 15	.10	. 08	.08	.07	.06		.09	.08	.07		.06		.09	.08	.07
.16	.10	.09	.08	.07	.06		.09	.08	.07		.06	4	.09	.08	.07
.17	.10	.09	.08	.07	.07		.10	.09	.08		.06	200	.10	.09	.08
.18	.11	.09	.08	.07	.07		.10	.09	.08		.06		.10	.09	.08
.19	.11	.10	.08	.08	.07		.10	.09	.08		.07		.10	.09	.08
.20	.12	. 10	.09	.08	.07		.11	.09	.08		.07		.11	.09	.08
.21	.12	.10	.09	.08	.07		.II	.09	.08		.07		.11	.09	.08
.22	.12	. 10	.09	.08	.07		-11	.10	.09		.07	6	-,11	.10	.09
.23	.12	. 11	.09	.08	.07		+11	.10	.09		.07		-11	.10	.09
. 24	.13	11+	.09	.08	.08		.12	.10	.09		.07		.12	.10	.09
. 25	.13	. !!	.10	.08.	.08		.12	.10	.09		.07	3	.12	. 10	.09
. 26	.13	11.	.10	.09	.08		.12	.10	.09		.07		.12	.10	.09
.27	.14	.11	.10	.09	.08		.12	.10	.09		.07		.12	.10	.09
.78	.14	.12	.10	.09	.08		.13	-11	.09		.07		.12	П	.09
.29	.14	.12	.10	.09	.08		.13	.11	.09		.08		.13	.11	.09
.30	.14	.12	.10	.09	.08		.13	.11	.10		.08		.13	-11	.09
.31	.14	.12	.10	.09	.08		.13	.11	.10		.08	ė	.13	.11	.10
.33	.15	.12	.10	.09	.08		.13	.11	.10		.08		.13	.11	.10
.34	.15	.12	.10	.09	.08		.13	.11	.10		.08		.13	.11	.10
.35	.15	.12	.11	.09	.08		.14	.11	.10		.08		.13	.11	.10
.36	.15	.13	.11	.09	.09		.14	.12	.10		.08				
-37	.16	.13	.11	.10	.09		.14	.12	.10		.08		NO.	TE:	
.38	.16	.13	.11	.10	.09		.14	.12	.10		.08		Her	. THI	6
.39	.16	.13	.11	.10	.09		.14	.12	.10		.08			UMN	
.40	.16	.13	-11	.10	.09		.14	.12	.10		.08			LAST	
.41	.16	.13	.11	.10	.09		.15	.12	.10		.08			IMNS	-
.42	.16	.13	.11	.10	.09		.15	.12	-11		.08		TABL		
.43	.17	.13	.11	.10	.09		.15	.12	.II		.08			(a) A1	ND (b)
.44	.17	.14	.11.	.10	.09		.15	-12	-11		.08		ONL		(-)
.45	.17	.14	.11.	.10	.09		.15	.12	.11		.08				
.46	.17	.14	.11	.10	.09		.15	.13	.11		.08				
.47	.17	.14	.12	.10	.09		.15	.13	.11		.08		17 8		
.48	.17	.14	.12	.10	.09		.15	.13	-11		.09				
.49	.18	.14	.12	.10	.09		.15	.13	.11		.09		100		
.50	.18	.14	.12	.10	.09		.16	.13	.11		.09				

FRAME	ERA W	VI I	S						BET					ABLI	
T DANGE		766	<u> </u>						IVITY			1011		F. 2 (<u>()</u>
	TBLAN	IKETS	OR BA	ITTS P				NKETS	-	T .	INSULAT	ION	K:	BAC	/ E F
	AGA1	NST E	LITHER	SIDE	<u>-</u> ,				TERED,		BLANKETS BATTS OR		INTE	BIOR F	INIS
COFFERENCE	WITH	ONE	AIR S	SPACE				RATINO			FILL; NO		BLAN	KETS (PARA
COEFFICIENT WITH NO									, EACH		AIR SPACE.		TWO	AIR SP	ACES
INSULATION			11 1001				A! L	EAST			INSULATION				
BETWEEN	AIR	SPACE		INSUL	AT ION		INSUL	FI MATERIAL	SPACES				INSUL	1	CAIR
STUDS.							ATION	41							5 17.10
	E.X	TERIOR	-41	INTER	NOB.		EXTERI		5		CHIEF .	10			
THICKNESS +	1"	11/2"	2"	2 1/2"	3"	1	1º	11/2"	1 2"	1	3 58"		EXT.	11/2"	1 2
.II	.08	.07	.07	.06	.06	1	.08	.07	.06	-			1		
.12	.09	.08	.07	.06	.06	1	.08	.07	.00		.05		.08	.07	.00
.13	.09	.08	.07	.07	.06	-	.09	-08	.07		.06		.08	.07	.0
.14	.10	.08	.08	.07	.06	1	-	.08	-		.06		.09	.08	.0
.15	.10	.09	.08	.07	.00	1	.09	.08	.07		.06		.09	.08	.0
.16	.10	.09	.08	.07	.07			.08	.08		.06	1	.09	. 08	.08
.17	.11	.09	.08	.08	.07	1	.10	.09	.08		.06		.10	.09	30.
.18	.11	.10	.09	.08	.07	1	.10	.09	.08		.07		.10	.09	.08
.19	.12	.10	.09	.08	.07		11.	.09	.08		.07		.10	.09	.08
.70	.12	.10	.09	.08	.07		. 11	.10	.09		.07		.11	.10	.08
.21	.12	-11	.09	.08	.08		.11	.10	.09			1			.09
.72	.13	.11	.09	.08	.08		.12	.10	.09		.07		.11	.10	.09
. 23	.13	-11	.10	.09	.08		.12	.10	.09		.07		.11	.10	.00
.24	.13	,11	.10	.09	.08		.12	.10	.09		.07	- /	.12	.10	.09
. 25	.14	.11	.10	.09	.08		.12	.11	.09		.08		.12	.11	.00
.26	.14	.12	. 10	.09	.08		.13	.11	.10		.08		.12	.11	.10
.27	.14	.12	.10	.09	.08		.13	.11	.10		.08		.13	.11	.10
.28	.14	.12	.10	.09	.08		.13	-11	.10		.08		.13	.11	.10
.29	.15	.12	11	.09	.09		.13	.11	.10		.08		.13	.11	. 10
.30	.15	.12	+11	.10	.09		.13	.11	.10		.08		.13	.11	.10
.31	.15	.13	»II	.10	.09		. 14	.12	.10	-	.08		.13	.11	.10
.32	.15	.13	.11	.10	.09		.14	.12	.10		.08		.14	.12	.10
.33	.16	.13	.II	.10	.09		.14	.12	. 10		.08		.14	.12	.10
.34	.16	.13	.11	.10	.09		.14	.12	.10		.08		.14	.12	.10
.35	.16	.13	.11	.10	.09		.14	.12	.11		.08		.14	.12	.10
.36	.16	.13	-11	.10	.09		. 15	.12	.11		.08		NO	TE:	
.37	.16	.13	,11	.10	.09		.15	.12	.11		.09		NO	1	
.38	.17	.14	.12	.10	.09		.15	.12	.11		.09		USE	THIS	5
.40	.17	.14	.12	.10	.09		.15	.12	-11		.09			MN I	
	.17	.14	.12	.10	.09		.15	.13	-11		.09			LAST	
.41	-17	.14	.12	.10	.09		.15	.13	.11		.09		1	IMNS	0 %
.42	.17	.14	.12	.10	.09		.15	.13	.11.		.09		TABL		
.43	.18	.14	.12	.11	.10		.16	.13	.11		.09			(a) AN	10 (F
.44	.18	.14	.12	.11	.10		.16	.13	.11		.09		ONL	Υ.	
	.18	.14	.12	.11	.10		.16	.13	.11		.09		1		
.46	.18	.15	.12	-11	.10		.16	.13	.11		.09				
.47	.18	.15	.12	.11_	.10		.16	.13	.11		.09				
.48	.18	.15	.12		.10		.16	.13	.11		.09				
.49	.19		.13	.11	.10		.16	.13	.12		.09		1		
.50	.19	.15	.13	.11	.10		.16	.14	.12		.09				

OVERALL HEAT TRANSMISSION COEFFICIENTS "U" FRAME WALLS REFLECTIVE INSULATION BETWEEN STUDS

TABLE WF. 3

INSIDE DESIGN TEMP. 70°, OUTSIDE DESIGN TEMP. -10°, EMISSIVITY & REFLECTIVE SURFACES .05

The state of	FOILS RE	FLECTIVE TW	O SIDES	FOILS REFLECTIVE ONE SIDE
COEFFICIENT VITH NO NSULATION BETWEEN STUDS	TWO AIR SPACE EACH FACED	THREE AIR SPACE TWO FACED ONE SIDE AND ONE FACED BOTH SIDE	FOUR AIR SPACES TWO FACED ONE	TWO AIR SPACES THREE AIR SPACES FOUR AIR SPACES ONE FACED ONE TWO FACED ONE THREE FACE SIDE WITH SIDE WITH REFLECTIVE MATERIAL. MATERIAL.
	EXTERIOR INTERIO	R EXTERIOR INTERIOR	EXTERIOR INTERIOR	EXTERIOR INTERIOR EXTERIOR INTERIOR EXTERIOR INTERIOR
.11	.08	1.07	1.06	EXTERIOR INTERIOR EXTERIOR INTERIOR EXTERIOR INTE
. 12	.08	.07	.06	.09 .08 .07
.13	.09	.07	.06	.10 .08 .07
.14	.09	.08	.06	.10 .08 .07
.15	.10	.08	.07	.11 .09 .07
. 16	.10	.08	.07	.11 .09 .08
.17	.10	.08	.07	.12 .10 .08
. 18	.11	.09	.07	.12 .10 .08
.19	- 11-	.09	.08	.13 .10 .08
. 20	.12	.09	.08	.13 .10 .09
.71	-12	.09	.08	.14 .11 .09
.22	.12	.10	.08	.14 .11 .09
. 23	.13	.10	.08	.15 .11 .09
. 24	.13	.10	.08	.15 .12 .09
.25	.13	. 10*	.08	.16 .12 .10
.26	. 14	. 10	.09	.16 .12 .10
.27	.14	.11	.09	.17 .12 .10
. 28	.14	, 11	.09	.17 .13 .10
.29	.14	_ II _	.09	.18 .13 .10
.30	.15	. 11	.09	.18 .13 .10
.31	.15	-11	.09	.18 .13 .10
.37	.15	.11	.09	.19 .13 .11
.33	.16	. 12	.09	.19 .14 .11
.34	.16	. 12	.09	.19 .14 .11
.35	.16	. 12	.09	.20 .14 .11
.36	.16	.12	.10	.20 .14 .11
.37	.16	.12	.10	.21 .14 .11
.38	.17	.12	,10	.21 .14 .11
.39	.17	.12	.10	.21 .15 .11
.40	.17	.12	.10	.21 .15 .11
.41	.17	.13	.10	. 22 . 15 . 11
.47	.17	.13	.10	.22 .15 .12
.43	.18	.13	.10	221512
.44	.18	.13	.10	.23 .15 .12
	. 18	.13	.10	.23 .16 .12
.46	.18	. 13	.10	. 23 . 16 . 12
.47	. 18	. 13	.10	.23 .16 .12
.48	.18	. 13	.10	.24 .16 .12
.50	.19	. 13	.10	.24 .16 .12
, 50	1.17	. 13	.11	.24 .16 .12 T-N-B- JAN/51

OVERALL HEAT TRANSMISSION COEFFICIENTS "U" FRAME WALLS USING FOIL BACKED INTERIOR FINISH WITH REFLECTIVE INSULATION BETWEEN STUDS

TABLE WF.4

INSIDE DESIGN TEMP. 70°, OUTSIDE DESIGN TEMP. -10° EMISSIVITY of REFLECTIVE SURFACES .05

	FOILS RI	EFLECTIVE TWO	O SIPES	FOILS REFLECTIVE ONE SIDE
COEFICIENT WITH NO INSULATION BETWEEN STUDS.	ONE FACED ON SIDE AND ON FACED BOTH SID WITH REFLECTIV MATERIAL.	ES THREE AIR SPACES IE ONE FACED ONE E SIDE AND TWO ES FACED BOTH SIDES VE WITH REFLECTIVE MATERIAL.	ONE FACED ONE SIDE AND THREE FACED BOTH SIDES WITH REFLECTIVE MATERIAL.	ONE FACED BOTH ONE FACED ONE TWO FACED ON SIDES WITH SIDE AND ONE SIDE AND ONE REFLECTIVE FACED BOTH SIDES FACED BOTH SIDE WITH REFLECTIVE WITH REFLECTIVE MATERIAL.
11.	.09	.07	.06	10 .08 .07
.12	.09	.07	.06	.10 .08 .07
.13	.10	.08	.07	.11 .09 .07
.14	.10	.08	.07	.12 .09 .08
.15	.it	.09	.07	.13 .10 .08
.16	.11.	.09	.08	.13 .10 .08
.17	1.12	.09	.08	.14 .11 .09
.18	.12	.10	.08	.15 .11 .09
.19	.13	.10	.08	.15 .12 .09
.20	.13	.10	.08	.16 .12 .10
.21	.14	.11	.09	.16 .12 .10
.22	.14	.11	.09	.17 .13 .10
. 23	.15	.11	.09	.18 .13 .10
.24	.15	111.	.09	.18 .13 .10
.25	.15	.11	.09	.19 .14 .11
.76	.16	.12	.09	.19 .14 .11
.27	.16	.12	.10	.20 .14 .11
.28	.16	.12	.10	.21 .14 .11
.29	.17	.12	.10	.21 .15 .11
.30	.17	.13	.10	.22 .15 .11
.31	.18	.13	.10	.22 .15 .12
.32	.18	.13	.10	.23 .15 .12
-33	.18	.13	.10	.23 .16 .12
-34	.18	.13	.10	.24 .16 .12
-35	.19	.14	.11	.24 .16 .12

SOLID OVERALL HEAT TRANSMISSION COEFFICIENTS "U" TABLE MASONRY WALLS WM. I NO INSULATION EXTERIOR FINISH INTERIOR FINISH MAIN WALL 3/4" TO 2" FURRING STRIPS, AS REQUIRED FOR INSULATION 1/2" PLASTER 1/2 PLASTER 1/2"PLASTER BOARD, REFLECTIVE INTERIOR SIDE BOARD, REFLECTIVE BOTH SIDES BOARD BOARD BOARD PLASTER EITHER PLAIN WALL NO INTERIOR FINISH WALL THE ADDITION & STUCCO EXTERIOR INCREASES THE THERMAL RESISTANCE SO SLIGHTLY THAT FIGURES FOR "NO EXTERIOR FINISH" MAY BE USED WITH NO APPRECIABLE ERROR. NO EXTERIOR PLASTER PLASTE LATH, LATH, FINISH WINSULATION BOARD LATH, NO INSULATION INSULATION INSULATION OR 1/2 BOARD L PLASTER, DIRECT BOARD " STUCCO * BOARD LATH 3/4" 3/4" PLYWOOD PLYWOOD INSULATION GYPSUM GYPSUM LATH, LATH, 1, INSULATION GYPSUM RIGID FO RIGID RIGID MUSYPE 400M METAL FOIL FOIL 0 2 FOR MASS INSUL. USE TABLE WM.4 SOLID CONCRETE FOR REFLECTIVE INSUL. USE TABLE WM.4 ----.79 .71 .41 .40 .27 .23 .19 .40 .38 .39 .42 .39 .26 .22 .19 .32 .25 .28 6" SOLID CONCRETE, SAND & GRAVEL AGGREGATE .70 .64 .38 .37 .26 .22 .19 .38 .36 .36 .39 .37 .25 .21 .18 .31 .24 .27 8" SOLID CONCRETE, " " .63 .58 .36 .35 .25 .21 .18 .36 .34 .34 .37 .35 .24 .20 .18 .29 .23 .26 10" SOLID CONCRETE, " " HOLLOW CONCRETE 8" HOLLOW CONCRETE BLOCK SAND & GRAVEL AGGREGATE 56 52 34 33 24 20 .17 .33 32 .32 .34 .32 .23 .20 .17 .28 .22 .24 BLOCK 49 46 31 30 22 19 17 31 29 30 32 30 22 19 16 26 20 23 12" HOLLOW CONCRETE BLOCK " 41 .39 .28 .27 .21 .18 .16 .27 .26 .26 .28 .27 .20 .17 .15 8" HOLLOW CONCRETE BLOCK CINDER AGGREGATE 38 36 26 26 20 17 15 26 25 25 26 25 19 17 .15 .22 .18 12" HOLLOW CONCRETE BLOCK " 8" HOLLOW CONCRETE BLOCK . SLAG AGGREGA .36 .34 .25 .25 .19 .17 .15 .25 .24 .24 .26 .24 .19 .16 .15 .22 .17 .19 34 33 24 24 19 16 15 24 23 24 25 24 18 16 12" HOLLOW CONCRETE BLOCK " .14 .21 .17 HOLLOW CLAY 41 39 28 27 21 .18 .16 .27 .26 .26 .28 .27 .20 .17 .15 .23 .19 8" HOLLOW CLAY TILE 2 CELLS THICK 40 38 27 27 20 18 16 27 26 26 27 26 20 17 15 23 18 10" HOLLOW CLAY TILE 2 " .31 .29 .72 .72 .18 .15 .14 .72 .71 .72 .73 .72 .17 .15 .14 .20 .16 .17 12" HOLLOW CLAY TILE 3 " SOLID STONE .70 64 38 37 26 22 19 38 36 36 39 37 25 21 18 31 24 .27 8" SOLID STONE 57 .53 .34 .33 .24 .20 .18 .34 .32 .33 .35 .33 .23 .20 .17 .28 .22 .25 12" SOLID STONE .49 .45 .31 .30 .22 .19 .17 .30 .29 .29 .31 .30 .22 .19 .16 .26 .20 . 23 16" SOLID STONE

VENEER MASONRY WALLS

OVERALL HEAT TRANSMISSION COEFFICIENTS "U"

TABLE WM. 2

M	ASONRY W	ALLS NO IN	5 U.	LA	71	ON	/								WN	1.	2	
EXT	ERIOR FINISH	MAIN WALL				ľđ		INT				NI			W.			
					3/4	TO	2"	FURR	ING	STRI	PS,	AS P	LEQU	JIREI	F01	RINS	SULA	TIOI
VEN	NEER FACING*	FOR VENEER MASONRY WALLS THE MORTAR BETWEEN BACKING AND FACING HAS NOT BEEN INCLUPED IN THE CALCULATION of "" VALUES, SINCE THE APPITIONAL RESISTANCE IS CONSIDERED UNIMPORTANT.	PLAIN WALL , NO INTERIOR FINISH	1/2" PLASTER, DIRECT ON WALL	38" GYPSUM BOARD		1/2" RIGID INSULATION BOARD	INSULATION BOA	I'' RIGID INSULATION BOARD	PLY	GYP	TAL LATH, 34" P	WOOD LATH, 34" PLASTER	BOARD LATH, 1/2"	LATH, 12	FOIL BOARD REFECTIVE INTERIOR SIDE	BOARD, REFLECTIVE BOTH SI	FOIL BACKED 3/8"
	17/							LAT							W.4		1	A 57
								NSUL	11.10		- A	-			IVM.		co	LUM
	\mathbf{H}	6" SOLID CONCRETE, SAND & GRAVEL AGGREGATE 8" SOLID CONCRETE, " " "						.20 .20									7.21	
3	1750	4" COMMON BRICK	50	46	131	130	77	.19	17 2	1 .29	3 30	32	.30	22	.19 .1	6 2	6.20	1.2
12		8" COMMON BRICK	1.35	.34	.20	2.25	1.19	17	15 .7	15 .24	4 .24	.25	.24	.19	16 .1	4 .7	2 .17	.19
VENEER		12" COMMON BRICK	.78	. 26	1.21	1.720	1,17	.15	13	21 .28	J]. 20) .21	1.20	,16	.14 .	13 .10	8 .15) -10
. 1		4" HOLLOW CLAY TILE I CELL THICK	.45	.42	.20	1.29	22	.19	16 .	29.28	3 28	3.30	.28		. 18 .			0.2
0		6" HOLLOW CLAY TILE 2 CELLS THICK	.36	.34	- 25	.25	.19	.17	15	25 -24 24 -23	4 .24	.25	-24	.19	.16 .1			1 . 1
BRICK		8" HOLLOW CLAY, TILE 2 " "	35 34	.32		24				24 2						4 .2	$\overline{}$	
W		4" HOLLOW CONCRETE BLOCK SAND & GRAVEL		.48		2-31					0.31		.31	.22		7 .2		
FACE	1937	8" HOLLOW CONCRETE BLOCK " "	.45	.42	-			_		29 .21		28				5 2	5 .20 3 .19	_
*		4" HOLLOW CONCRETE BLOCK CINDER AGGREGATE	.45	.42	.29	29	.22	.19	16 .	29 .2	8 .28	3 -30	.28	-21				-
A		8" HOLLOW CONCRETE BLOCK " "	35	-33		24				24 .2 23 .2		24				14 .2 14 .2	1.0	-
		8" HOLLOW CONCRETE BLOCK SURNED CLAY	.31	.30	.23	.22	-18	.16	.14 .	23 .2	2 .24	2 .23	.22	-17	.15 .	14 .7		-
		12" HOLLOW CONCRETE BLOCK " "	.30	-	_	1 .22	_	15 NSU	7			_					7-10	0 +1
								VE .										AST
Ш		G" SOLID CONCRETE, SAND & GRAVEL AGGREGATE	.63	.58	3 .36	6 .35	.25	.21	18	36.3	4 .3	4.37	-35	.24	20	18 .2	29 .2:	3 .2
~		8"SOLID CONCRETE, " " "	.57	1.53	.34	1.33	.24	20	18	34 .3	2 3	3 .35	.33	1.23	20	17 1.2	28 .2	2 .2
VENEER		4" COMMON BRICK	.53	.49	3.30	2 32	.23	20	.17	32 -3	0 -3	1 .33	.31	.22	.19	17 2	27.2	1 .2
NE		8" COMMON BRICK 12" COMMON BRICK	.37	.35	1 2	0 25	1 .17	.17	.15 .	26 .2 21 .2	5 2 0 .2	1 -22	-21	-19	.17 .	15 .1	9 11	5 -1
7		TE COMMENT DISCON																
E		4" HOLLOW CLAY TILE I CELL THICK	48	.44	4 .30	0 -30	-22	.19	.17	30 .2	9 .2	9.31	.29	.21	.18 .	16 .2	25 -2	0 .7
STONE	Marie and the second	6" HOLLOW CLAY TILE 2 CELLS THICK	1.36	.34	F -21	5 .25	5 -19	.17	.15 .	25 .2	4 2	4.26	1.25	.19	.16 .	15 .7	22 .18	8 .1
S		10" HOLLOW CLAY TILE 2 "	-35	34	1.2	5 . 25	5 -19	-17	.15 -	25.2	4 .24	4 .25	.24	.19	.16 .	14 .7	22 .1	7 .1
**		4" HOLLOW CONCRETE BLOCK SAMP & GRAVE	56	51	1.3	4 - 32	3 -24	-20	-17 -	33 .3	1 .3	2 .34	-32	.23	.19 .	17 5	28 - 7 75 - 7	
A	1937	8" HOLLOW CONCRETE BLOCK " "	.43	.40	2	8 .28	3 .21	.19	.16 .	28 -2	7.2	7 .29	1.27	.20	.18	16 .	24 .19	9 .7
		4" HOLLOW CONCRETE BLOCK CINDER AGGREGA	14.48	1.4	4 3	0 .30	222	2 .19	.17	30 .2	9 .2	9 31	1.29	1.21	.18	16 .	25 . 2	0 -
7.9		8" HOLLOW CONCRETE BLOCK " " " " " " " " " " " " " " " " " " "	1.34	1.37	7 2	4 .24	4 .18	.17	.14 .	24 .2	3 .2	3 .24	.23	-18	.16	14 .7	21 .1	7 .1
		8" HOLLOW CONCRETE BLOCK SLAG AGGREGATE	. 37	.3	1.2	3 .23	3 -18	.16	.14	23 .2	2 -2	3 .24	23	.18	.16	14 .7	20 .1	7 .1
		12" HOLLOW CONCRETE BLOCK " "	1.31	-30	0 .2	3 .27	2 .18	.16	.14	22 .2	2 2	2 .23	-22	-17	-15	14 .	20 .1	6

CAVITY OVERALL HEAT TRANSMISSION COEFFICIENTS "U" MASONRY WALLS NO INSULATION

TABLE WM 3

XT.	ERIOR WALL	INTERIOR WALL						INT	ERI	OR	FI	NIS	H					
					3/4"	TO	2"	FURR	ING	STRI	ps,	AS R	EQUII	RED !	OR	INSL	LAT.	101
NO	EXTERIOR FINISH OR 1" STUCCO*	IN CALCULATIONS of "U" VALUES FOR THE CAVITY WALLS, THE THERMAL TRANSMISSION of THE TIES BETWEEN EXTERIOR AND INTERIOR WALLS HAS NOT BEEN INCLUDED SINCE IT HAS LITTLE EFFECT UPON THE "U" VALUE of THE WALLS SHOWN	PLAIN WALL , NO INTERIOR FINISH	1/2" PLASTER, DIRECT ON WALL	36" GYPSUM BOARD	1/2" GYPSUM BOARD	1/2" RIGID INSULATION BOARD	INSULATION BOAR	00 0		1	LATH, 3/4" PLASTE	, 3/4" PLASTER	7 INSULATION BOARD LATH, 7 PLASTER 32"INSULATION BOARD LATH, 1/2 PLASTER	BOARD LATH,	FOIL BOARD, REFLECTIVE INTERIOR SIDE	7, REFLECTIVE BO	FOIL BACKED %"
	2							IL. U					1				LA:	
-		4" COMMON BRICK						.16							14	21	COL	
X/OX		8" COMMON BRICK	.27	.26	.20	.20	.16	.14	13 5	20 .20	20	21	20.1	6 .14	.13	.18	.15	-
																	16	
0		4" HOLLOW CLAY TILE I CELL THICK 6" HOLLOW CLAY TILE 2 CELLS THICK	.37	30	23	.23	.18	.16 .	13 0	20 .20	20	21	20 1	6 .14	13	.18	.16	. 1
FACE		8" HOLLOW CLAY TILE " "						.14		20 .19	-19	.20	20 -1	6 -14	.13	. 18	-15	. 1
1		4" HOLLOW CONCRETE BLOCK SAND & GRAVEL							15 .	25 24	.24	25	24 .1		.14			
		8" HOLLOW CONCRETE BLOCK " "							14 .	23 .27	2 .22	23	23 .1	8 .15	.14			
4		4" HOLLOW CONCRETE BLOCK AGGREGATE 8" HOLLOW CONCRETE BLOCK " "				.23		.16 .	14 1	23 .22 20 .19	.19	.23	20 1		_		.15	
		8" HOLLOW CONCRETE BLOCK BURNED CLAY OR						14	12	19 -18	.18	-19	18	5 .13	12		.14	
47E		4" HOLLOW CLAY TILE I CELL THICK	79	28	122	1.22	1.17	-15	14 .	22 21	1.21	1.22	21 .1	7 .15	-13	.19	.16	.1
AEG		6" HOLLOW CLAY TILE 2 CELLS THICK	.25	.24	.19	.19	.16	.14	13 -	19 .19	1-19	20	19 .1	5 .14	.12	.17	.14	1.
& GRAVEL AGGREGATE		8" HOLLOW CLAY TILE " "	25	.24	.19	.19	.15	.14	13 -	19 -18	-19	-19	19 .:	5 .14	-12	1.17	.14	1.1
22	<i>F3</i> /2-7	4" HOLLOW CONCRETE BLOCK SAND & GRAVEL						.16		73 .20	2 .23	.24	23 -	8 .10	.14	.70	-17	
18		8" HOLLOW CONCRETE BLOCK " "	.29					.15 .		22.2		.22					.16	. 1
10		4" HOLLOW CONCRETE BLOCK AGGREGATE 8" HOLLOW CONCRETE BLOCK " "	25	.24	. 19	.19	.15	.14 .	13	19 .18								-
CINDER AGGREGATE SAND		8" HOLLOW CONCRETE BLOCK SURVED CLAY OR	.23	-22	18	.18	.15	.13	12	18 .1	.17	-18	.18	14 .13	12	.16	-13	
34	/B/1855	4" HOLLOW CLAY TILE I CELL THICK	127	1.76	20	70	16	1.15	13	20 20	5 .20	21	20	6 .14	1.13	1.18	.15	1.1
GAY		G" HOLLOW CLAY TILE 2 CELLS THICK	.23	.22	.18	.18	.15	.13 .	12 .	18 -18	18	.19	.18 .	15 -13	-12	.16	.14	
GRE		8" HOLLOW CLAY TILE " " - "	.23	.22	18	-18	.15	.13	12 .	18 1.	1-18	18	.18 .	14 .1	3 .12	.16	.13	
AG	To the same of the	4" HOLLOW CONCRETE BLOCK SAND & GRAVEL	179	.78	1.22	172	1.17	.15	14	22 .2	1 .21	1.22	211.	17 .11	-13	1.19	.16	T.
ZE	[B][S]	8" HOLLOW CONCRETE BLOCK " "	.27	1.20	,20	20	-16	.15	13 .	20 .21	20	21	20 .	16 .14	1.13	-18	.15	
12,		4" HOLLOW CONCRETE BLOCK AGGREGATE	-27	.26	.20	.20	.16	.15	13	20 2	0 20	21	.20 .	16 .14	1.13	-18	.15	ŀ
U		8" HOLLOW CONCRETE BLOCK " " 8" HOLLOW CONCRETE BLOCK SURVEY CLAY OF	21	.21	18	.13	14	.13	12 .	17 -16	17	17	17	14 1	2 -11	.15	13	
7	-	O HOLLOW CONORETE DECON SIAZ AZZAZZAJI	T											J.				
7175	44	4" HOLLOW CLAY TILE / CELL THICK	.27	.20	20	20	-16	.15	13	20 .2	0 .20	21	.20 .	16 -14	1-13	.18	-15	1.
		8" HOLLOW CLAY TILE 2 CELLS THICK	.23	.22	1.18	18	-15	.13	.12 .	18 .1	7 .18	3 18	.18 .	14 .1	3 .12	.16	.13	
5	Marie Militarian	4" HOLLOW CONCRETE BLOCK SAND & GRAVEL	70	79	3 77	200	17	.15	14	22 2	1 7	1 22	.21	17 .11	5 .13	1.19	.16	T.
4" HOLLOW CLAY		8" HOLLOW CONCRETE BLOCK "	27	.20	20	1.20	16	.15	13 .	20 .2	0 .20	0 .21	.20 .	16 .14	4 .13	.18	.15	
770		4" HOLLOW CONCRETE BLOCK GINDER	27	.20	6 .20	20	16	-15	13 .	20 .2	0.2	0 -21	.20	16 .1	4 .13	-18	.15	
		8" HOLLOW CONCRETE BLOCK " "	.23	100	71.18	31.18	1.15	.13	19	18 1	1 .18	3 1 18	.18 .	14 .1	31-12	1.16	1.13	J.

MASONRY WALLS WITH INSULATION BETWEEN FURRING STRIPS.

TABLE WM.4

		MA	155	1	NSL	JLA'	TION	1		EAG	REFLECTI CH AIR SPACE	VE L AT LE	AST 34"	LATI		.05
	Fi	NOMIN IRRIN	G.	2		-	L FUI		G.					IN'	LECTIV TERIO INISH	
COEFFICIENT WITH NO INSULATION IN FURRING SPACE	I"	BATT SLANI IPRES	KET,		BAT OR LANK		2' OR B (COM		ET,	FAC SID RE	AIR SPACE LED ONE PE WITH FLECTIVE TERIAL.	EACH F SIDE REFLI	IR SPACES FACED ONE WITH ECTIVE RIAL.	ONE I SIDE, FACE WITH	AIR SP FACED , AND D BOTH REFLI ERIAL	ONE ONE SIDES CTIVE
	EXTERIO	DR II	TEBIOR	EXTERI		TERIOR	EXTERIO	OR IN	TERIOR	EXTE	RIOR INTERIOR					ERIOR
K VALUE	k-24	k-27	K-30	k ·24	k.27	K-30	K · 24	k · 27	K-30	C	UTSIDE D	ESIGN	TEMPER	ATUF	RE - 1	o°
.11	.09	.09	.09	.08	.08	.08	.06	.07	.07		.09		.08		.08	
.12	.09	.10	. 10	.08	.08	.09	.07	.07	.07		.10		.08		.09	
.13	.10	.10	- 11	.08	.09	.09	.07	.07	.08		.11		.09		.10	-
.14	,11	-11	- 11	.09	.09	.10	.07	.08	.08		.12		.09		.10	
.15	-11	.12	. 12	.09	.10	+10	.07	.08	.08		.13		.10		.11	
.16	.12	.12	. 13	.10	- 10	.10	.08	.08	.09		.13		.10		.11	
.17	.12	.13	- 13	.10	-10	* II	.08	.08	.09	1	.14		.10	0.1	.12	
.18	.13	-13	. 14	.10	.11	-11	.08	.09	.09		.15		.11		.12	
.19	.13	-14	. 15	.11	. II	-12	.08	.09	.09		.15		.11		-13	-
.20	. 14	.15	.15	a H	» II	.12	.08	.09	-10		.16		.12		.13	_
. 21	.14	. 15	.16	, 11	.12	-12	.09	.09			.17		.12		.14	-
.27	.15	.16	. 16	-, 11	.12	-13	.09	.09		-	.18	-	.12		.14	
.23	.15	-16	.17	.12	.12	.13	.09	.10	. 10		.18	-	.13		.15	
.24	.16	.17	.17	.12	.13	-13	.09	.10	. 10	-	-19	-	.13		.15	
.25	.16	.17	. 18	.12	.13	.14	.09	.10	11.	-	.20	+		-	.16	-
.26	.16	.17	.18	.12	.13	.14	.09	.10	. 11	-	.20	-	.14	100	.16	
.27	-17	-18	. 19	-13	-14	.14	10	-10	11.	-	.21		.14		.17	
.78	.17	-18	. 19	.13	.14	-14	.10	- 10	11.	-	.27		.14	-	.17	
. 29	.18	-19	. 20	-13	.14	. 15	.10	-11	- 11	-	.23		.15		.17	
.30	. 18	.19	. 20	.13	.14	-15	.10	-11	111	-			.15		.18	
.31	.18	.20	. 21	. 14	.14	.15	.10	.11	. 12	-	.23		.15		.18	
.32	.19	.20	. 21	.14	.15	.16	.10	. 11	. 12	-	.25	-	.16		.18	
.33	.19	.20	. 22	14	.15	.16	.10	- 11	. 12	-	.25		.16		.19	172
.34	.19	.21	.72	.14	.15	.16	.10	a 11	. 12	-	.26		.16		.19	
.35	.20	.21	.22	-14	.15	.16	-	- 11	-12	-	, 20				1/	
.36	.20	.22	.23	.14	.15	- 16	.10	-11	.12					NO.	TE:	
-37	.20	.22	.23	-15	.16	-17	-11	-12	.12					ı	JSE T	HIS
.38	-	-	. 24	1	+	.17	-11	.12	.13						UMN	
.40	.21	.23	. 24	. 15	.16	.17	-11	.12	.13						T TW	
	.21	.23	.25		.16	.17	-11	.12	.13					WM.	1, W	1.2
.41	.22	.24	.25	-	.16	.18	-11	.12	.13					ANI	VM	. 3
.43	.22	.24	.26	_	.17	.18	-11	.12	-13							
.44	.22	.24	.26	_	.17	.18	- 11	.12	-13							
.45	.23	.24	.26	-	.17	. 18	-	.12	-13							
.46	.23	.25	-	.16	_	- 18		.12	.13	1						
.47	.23	.25	. 27	16	.17	.18	-	- 12	-13							
.48	.23	.25	.27	.16	1	.19	-	.12	. 13							
.49	.23	.26	-	-	+	.19		.12	_							
.50	. 24	_	_	-	_	.19		.12						1	B JAN	

.06 .06

.07 .07 .07 .07

.07 .07 .06 .06

.07 .07

.07 .07

K = .27

K = .30

.07 .07

OVERALL HEAT TRANSMISSION COEFFICIENTS "U" TABLE F. 1 NO FINISH BELOW FLOOR JOISTS FLOORS FINISH INTERIOR INSULATION HARDWOOD, BUILDING
AND SOFTWOOD.

AND SOFTWOOD.

AND SOFTWOOD.

AND SOFTWOOD.

PAPER AND SOFTWOOD.

AND YA PLYWOOD.

AND YA PLYWOOD. NOTE: FIGURES BELOW ARE BASED ON VENTILATED CRAWL SPACE BELOW FLOOR JOISTS, AND ARE CORRECTED FOR 2" x8" JOISTS @ 16" O.C. SOFTWOOP HARDWOOD PLYWOOD 22 34 .25 .31 .31 .35 .35 37 .39 NO INSULATION .09 .09 .09 .09 .09 .09 k = .24.10 .10 MASS .10 .10 .09 .10 .10 K = .2710 .10 .10 MASS INSULATION INSULATION .11 .10 .10 .10 .11 .11 K = .30.11 .07 .07 .07 .07 .07 .07 .07 k = .24.07 VAPOUR BARRIER .07 .08 .08 .08 .08 k = .27 .08 .08 .08 MASS INSULATION .08 .08 .08 .08 .08 .09 .08 K = .30.08 .06 .06 .06 .06 .06 .06 .06 .06 K = .24MESH SUPPORT

INSULATION

MASS

REFLECTIVE	TIVE IN	SULATIO	N	/N:	SIDE D	ITY of I SURFA ESIGN	CES TEMP	·05								
ONE SIDE	BOTH SIDES			OUT	TSIDE D	ESIGN	TEMP.	-10°	_		-	_	-		-	
M	7	FOILS REFLECTIVE	ONE	. AIR	SPACE	, FACED	ONE	SIDE	.14	.15	.14	.12	.13	.13	.14	.14
	 	FOILS REFLECTIVE BOTH SIDES	н	н	140	н	0.	и	.12	.12	.11	.10	Ш	.11	.12	.12
		FOILS REFLECTIVE	(9)	u	11	FACED	вотн	SIDES.	.14	.14	.13	.12	.13	.13	.14	.14
	***************************************	FOILS REFLECTIVE BOTH SIDES	H.	n	ou.	п	ń	ij	.12	.12	.11	.10	.11	.11	:11	.11
		FOILS REFLECTIVE ONE SIDE	TWO	AIR	SPACES,	EACH FA	CED OI	NE SIDE.	.09	.09	.08	.08	.08	.08	.08	.08
	***************************************	FOILS REFLECTIVE BOTH SIDES	ar.	×.0	13			NE SIDE	.08	.08	.07	.07	.07	.07	.07	.07
The same of the sa		FOILS REFLECTIVE	11	п	П	ONE FA			.08	.08	.08	.08	.08	.08	.08	.08
	**************************************	FOILS REFLECTIVE. BOTH SIDES	и	n	II	EACH FAC	LED BO	TH SIDES	.07	.07	.07	.07	.07	.07	.07	.07
Muuma	M	FOILS REFLECTIVE.	THRI	E A	IR SPACE	S, EACH F	ACED	ONE SIDE.	.06	.06	.06	.06	.06	.06	.06	.06
		FOILS REFLECTIVE BOTH SIDES	и	n	n	ONE FAC		NE SIDE BOTH	.06	.06	.06	.05	.05	.05	.06	.06
	A COMMITTER OF THE PARTY OF THE	FOILS REFLECTIVE	ü	11	11	TWO FA		NE SIDE	.06	.06	.06	.06	.06	.06	.06	.06
		FOILS REFLECTIVE	u	и	n	EACH FA	CED B	OTH SIDES	.06	.06	.05	.05	.05	.05	.05	.05

OVERALL HEAT TRANSMISSION COEFFICIENTS "U" FLOORS WITH FINISH ON UNDER SIDE of FLOOR JOISTS

TABLE F. 2

	INSULATIO	N	FIN	1/4" SH 0		LY		000		0/575	_				SIDE		0AF	
			$\overline{}$	INT		_		INI				IN'	TER	IOR		IN	SH	
	NOTE: FIGURES BELOW, BASED ON A VENTILATE SPACE BELOW FLOOR, A CORRECTED FOR 2"x8" @ 16" 0.c.	D CRAWL	13/16 HARDWOOD	7, PLYWOOP	25/3, SOFTWOOP	HARDWOOD, BUILDING PAPER AND SOFTWOOD.	18" LINOLEUM, BUILDING PAPER AND SOFTWOOD.	18" ASPHALT TILE, BUILDING PAPER AND SOFTWOOD.	1	18 ASPHALT TILE, BUILDING PAPER AND 1/2" PLYWOOD.	13/" HARDWOOD	1/2" PLYWOOD	25/32" SOFTWOOP	HARDWOOD, BUILDING PAPER AND SOFTWOOD.	1/8" LINOLEUM, BUILDING PAPER AND SOFTWOOD.	18" ASPHALT TILE, BUILDING PAPER AND SOFTWOOD.	1/8" LINOLEUM, BUILDING PAPER AND 1/2" PLYWOOD.	1/8" ASPHALT TILE, BUILDING PAPER AND 1/2" PLY WOOD.
	NO INSULATION		.24	.25	.23	.19	.21	.22	.23	.23	.18	.19	.18	.15	.17	.17	.18	.18
MACC		k = .24	.09	.09	.08	.08	.08	.08	.08	.08	.08	.08	.08	.07	.07	.07	.08	.08
MASS	2" MASS INSULATION -	k = .27	.09	.09	.09	.08	.09	.09	.09	.09	.08	.08	.08	.07	.08	.08	.08	.08
INSULATION		k = .30	.09	.10	.09	.09	.09	.09	-10	.10	.09	.09	.08	.08	.08	.08	.09	.09
		k = .24	.07	.07	.07	.06	.07	.07	-07	.07	.06	.06	.06	.06	-	.06	.06	.06
	3" MASS INSULATION	k = .27	.07	.07	.07	.07	.07	.07	.07	.07	.07	.07	.06	.06	-	.06	.07	.07
M		k = .30 $k = .24$.08	.08	.08	.07	.07	.07	.08	.08	.07	.07	.07	.06	.07	.07	.07	.07
	4" MASS INSULATION	K = .24 $K = .27$.06	.06	.06	.05	.06		.06	_	.05	.05	.05	.05	.05	.05	.05	.05
	T MASS MISCENTION	k = .30	.07	.07	.06	.06	.06	_	.06	.06	.06	.06	.06	.06	.06	.06	.06	.06
	2" EXPANDED VERMICULIT		.12	.12	.12	-11	.12	.12	-12	.12	.11	.11	.10	.09	.10	.10	.10	.10
/	3" EXPANDED VERMICULIT		_	.10	.10	.09	.09	.10	.10	.10	.09	.09	.09	.08	.09	.09	.09	.09
A-5-	4" EXPANDED VERMICULIT	E k = .48	.09	.09	.08	.08	.08	.08	.08	.08	.08	.08	.08	.07	.07	.08		-08

REFLECT	The state of the s				5	SUR	FAC	refle Es	.05	5					Ī		1	
FOILS REFLECTIVE	FOILS REFLECTIVE BOTH SIDES		INSIDE DESIGN TEMP															
Marin		FOILS REFLECTIVE	.12	.12	.12	.10	.11	41	.12	.12	.10	.10	.10	.09	.10	.10	.10	.10
<u> </u>		Paul O Breiserius											10-70					
M M.	M M	FOILS REFLECTIVE	.11	-11	.10	.09	.10	.10	.10	.10	.09	.09	.09	.08	.09	.09	.09	.09
	<u></u>	FOILS REFLECTIVE BOTH SIDES	.09	.09	.08	.07	.07	.07	.08	.08	.07	.07	.07	.06	.07	.07	.07	.07
		FOILS REFLECTIVE ONE SIDE	.10	.10	.10	.09	.10	.10	.10	.10	.09	.09	.09	.08	.10	.10	.09	.09
	<u> </u>	FOILS REFLECTIVE BOTH SIDES	.08	.08	.07	.07	.07	.07	.07	.07	.07	.07	.07	.06	.07	.07	.07	.07
		FOILS REFLECTIVE ONE SIDE	.07	.07	.07	.07	.07	.07	.07	.07	.06	.06	.06	.06	.06	.06	.06	.06
<u></u>	\\)	FOILS REFLECTIVE BOTH SIDES	.06	.06	.06	.05	.05	.06	.06	.06	.05	.05	.05	.05	.05	.05	.05	.05
	11 11 11 11 11 11 11 11 11 11 11 11 11	FOILS REFLECTIVE	.07	.07	.07	.06	.07	.07	.07	.07	.06	.07	.06	.06	.06	.06	.06	.06
	The state of the s	FOILS REFLECTIVE BOTH SIDES	.06	.06	.05	.05	.05	.05	.05	.05	.05	.05	.05	.05	.05	.05	.05	.05

21

.15

.14 .24 .20

.13 .12 .17 .15

TABLE TRANSMISSION COEFFICIENTS OVERALL HEAT C. 1 NO FLOORING ABOVE CEILING JOISTS CEILINGS INTERIOR FINISH INSULATION PLASTER SES SIDE PLASTER 門兄 BOARD ď PLAST S REFLECTIVE INTERIOR BACKED 3/8", 'M" PLASTER PLASTER REFLECTIVE BOTH 25 2 30 LATH, PLAST BOARD LATH, 2 NOTE: FIGURES BELOW ARE BASED ON INSULATION INSULATION INSULATION BOARD BOARD VENTILATED ATTIC SPACE BETWEEN
CEILING & ROOF AND ARE CORRECTED
FOR 2"xG" JOISTS @ 16" O.C. LATH, BOARD BOARD 4 34 PLY WOOD PLYWOOD GYPSUM MUSAYD LATH, INSULATION LATI MUSYPA LATH, 34" INSULATION NSULATION BOARD, BOARD, RIGID RIGID R1617 PSUM METAL MOOD FOIL FOIL 38 30 3 2 GYI 4 10 .70 .62 .33 .26 .22 .56 .46 .49 .35 .27 .22 .66 .59 .61 .68 .64 INSULATION NO .09 .08 .10 .10 .09 .08 -11 .10 .10 .11 . 10 .09 .10 k = .24.11 .09 .11 MASS 11. .12 .11 .11 -12 -11 .10 .09 .09 .11 .11 k= . 27 .12 .10 .09 .09 2" MASS INSULATION II. INSULATION .12 .10 .09 .12 .12 .12 k = . 30 .12 -11 .10 .09 .12 .12 .12 -13 .11 13 .08 .07 .07 .06 .08 .08 .08 .07 .08 .08 .08 .08 .07 k = . 24 .08 .08 .07 .08 .09 3" MASS INSULATION K = . 27 09 09 .08 .07 .07 .09 .08 09.09 .09 .07 .08 .08 .09 .09 .09 .09.09 .08 .08 .07 .09 .09 .09 K= . 30 .09 .09 .08 .08 .07 .06 .05 .07 .06 .06 .07 .06 .06 .06 .05 .06 .06 06 k = .24.07 .06 .06 .06 .06 .07 .07 .06 .07 .07 .07 .06 .06 .06 .07 .07 10. .07 4" MASS INSULATION K= . 27 .07 .08 .06 .06 .07 k = .30 .08 .08 .07 .06 .06 08 .07 .08 .08 .07 -07 .07 .12 .17 .14 .13 -16 2" EXPANDED VERMICULITE k = .48.17 .14 .13 .12 .17 .16 .13 K = .48.13 11 .10 .10 .13 -13 .13 .13 13 .11 10 .09 .13 .13 3" EXPANDED VERMICULITE .13 .09 .09 .08 .10 .10 .10 4" EXPANDED VERMICULITE K = .48.11 -11 .09 .09 .08 .11 .10 .10 .11 .10

REFLECTIVE FOILS REFLECTIVE ONE SIDE	E INSULAT FOILS REFLECTIVE BOTH SIDES.	ION	IN	SIL	E	DE	516	N	TEA	CTI 1PE PER	RA	TUR	E	ACE 70 - 10	o°	05		
м м	м м	FOILS REFLECTIVE	.33	.32	.23	.19	47	.33	.31	.32	.34	.32	.22	.18	.16	.31	.30	.31
	XX	FOILS REFLECTIVE BOTH SIDES	.30	.29	.21	.18	.16	.29	.28	.28	.30	.28	.20	-17	.15	.27	.27	.28
М М		FOILS REFLECTIVE ONE SIDE	.33	.32	.23	.19	.16	.33	.31	.31	.34	.31	.22	.18	.16	.30	.30	.31
		FOILS REFLECTIVE BOTH SIDES	.29	.28	.21	.18	.15	.29	.27	.28	.30	.28	.20	.17	.15	.27	.27	.28
		FOILS REFLECTIVE ONE SIDE	.21	.21	.16	.14	.13	.21	.20	.20	.21	-21	.16	.14	.12	.20	.20	.20
		FOILS REFLECTIVE BOTH SIDES	.19	.19	.15	.13	.12	.19	.18	.19	.20	-19	.15	.13	.12	.18	.18	- 19
		FOILS REFLECTIVE	.21	.21	.16	.14	.13	.21	.20	.20	.21	.20	.16	.14	.12	.20	.20	.20
<u> </u>	<u> </u>	FOILS REFLECTIVE BOTH SIDES	.19	.19	.15	.13	-12	.19	.18	.19	.19	.19	.15	.13	-12	.18	.18	.19
	## M	FOILS REFLECTIVE	.15	-15	.13	.11	.10	.15	.15	.15	.15	.15	.12	.11	.10	.15	.14	.15
<u></u>	······································	FOILS REFLECTIVE BOTH SIDES	.14	.14	.12	.11	.10	.14	.14	.14	.14	.14	.11	.11	.10	.14	.14	.14
<u> </u>	##M###################################	FOILS REFLECTIVE ONE SIDE	.15	.15	.13	-11	.10	.15	.15	.15	.15	.15	.12	.11	.10	.14	.14	.15
The state of the s	<u> </u>	FOILS REFLECTIVE	.14	.14	.12	.11	.10	.14	.14	.14	.14	.14	.12	.11	.10	.14	.14	.14

ON TOP of JOISTS ON TOP of JOISTS.

1/2" RIGID INSULATION BOARD,

RIGID INSULATION BOARD.

.25 .25 -19

.18 .18 .15 -13

.15 .25 .24 .24 .26 .24 .18 .16

.12 -18

.17 .18 .18 .18 .14

.17

SIDES

TABLE

C. 2

NSULATION BOARD LATH, 1/2" PLASTER

BOARD, REFLECTIVE INTERIOR SIDE

NSULATION BOARP LATH, 1/2" PLASTER

HEAT TRANSMISSION COEFFICIENTS OVERALL 25/42 WOOD FLOORING, CEILINGS ABOVE CEILING JOISTS. INTERIOR FINISH INSULATION BOARD LATH, 1/2" PLASTER EB BB BOARD BOARD BOARD PLASTE PLASTER PLASTER NOTE: FIGURES BELOW ARE BASED ON VENTILATED ATTIC SPACE BETWEEN CEILING & ROOF AND ARE CORRECTED FOR 2'xG" JOISTS @ 16"O.C. INSULATION INSULATION INSULATION 2. BOARD BOA LATH, 3/4" 34. PLYWOOD PLYWOOD GYPSUM GYPSUM AL LATH, GYPSUM NSULATION LATH, RIGID RIGID RIGID A

	NOTE: FIGURES BELOW ARE BASE VENTILATED ATTIC SPACE CEILING & ROOF AND ARE CORRECTED FOR 2'xg" Jois	BETWEEN	3/8" GYPSUM BOARD	1/2" GYPSUM BOARD	1/2" RIGID INSULATION BOAR	34" RIGIP INSULATION BOAR	I' RIGID INSULATION BOAR	1/4" PLYWOOD	3%" PLYWOOD	36" GYPSUM LATH, 1/2" PLAST	METAL LATH, 3/4" PLASTER	WOOD LATH, 34" PLASTER	1/2" INSULATION BOARD LATH, 1/2" PLA	34" INSULATION BOARP LATH, 1/2" PLA	I" INSULATION BOARD LATH, 1/2 PLA	FOIL BOARD, REFLECTIVE INTERIOR	RP, REFLECTIVE	GYPSUM LATH, 1/2" PLASTER
$\overline{\mathbb{M}}$.	NO INSULATION		.30	.29	.21	.18	.16	.19	.28	.28	.30	.28	.21_	-18	.16	.27	.23	.23
MASS	2" MASS INSULATION	k = . 24 k = . 27	.09	.09	-	-	.07	.09	.09	-	.09	.09	_		.07		.09	.09
INSULATION	L MINGS INSSERTION	k = . 30 k = . 24	.10	.10	+	_	.08	.10	.10	-	.10	.10	.09	.08	.08	.10	-	.10
	3" MASS INSULATION	k = . 27 k = . 30	.08		.07	.07	.06	.08	_	.08	.08	-	.07	.07	.06	.08	.07	-
	4" MASS INSULATION	k = . 24 k = . 27 k = . 30	-	.06	.06	.05	.05	-	.06	-	.06	.06	.06	.06	.05 .05	.06	.06	.06
	2" EXPANDED VERMICULITE 3" EXPANDED VERMICULITE	k = .48 k = .48	-	13	.11	Ш	.10	.13	.13	.13	.14	.13	.11	.10	.10	.13	.13	.13
	4" EXPANDED VERMICULITE	k = .48	.09	.09	.08	.08	.07	.09	.09	.09	.09	.09	.08	.08	.07	.09	.09	.09

REFLECTIVE INSULATION					EMISSIVITY of REFLECTIVE SURFACES .05 INSIDE DESIGN TEMPERATURE 70°													
FOILS REFLECTIVE	FOILS REFLECTIVE BOTH SIDES		04	175	DE	DE	516	N 7	TEM.	PER	RATA	URE		10°				
M		FOILS REFLECTIVE ONE SIDE	.24	.24	-18	.16	.14	.24	.23	.24	.25	.24	.18	.15	.14	.23	.23	.23
<u> </u>																		
-M	M	FOILS REFLECTIVE	.20	.20	.16	.14	.13	.20	.20	.20	.20	.20	.16	.14	.12	.19	.19	.20
- Management Management	<u> </u>	FOILS REFLECTIVE BOTH SIDES	.17	.17	.14	.12	-11	.17	.17	.17	.17	.17	.13	.12	.11	.16	.16	. 16
-M-M	M	FOILS REFLECTIVE	.20	.20	.16	.14	.13	.20	.19	.20	.20	.20	.15	.14	.12	.19	.19	.20
	<u> </u>	FOILS REFLECTIVE BOTH SIDES	.17	.17	.14	.12	-11	.17	.16	.16	.17	.17	.13	.12	.11	.16	.16	.16
77777		FOILS REFLECTIVE ONE SIDE	.15	.15	.12	:41	.10	.15	.15	.15	.15	.15	.12	-11	.10	.14	.14	.15
<u>\\\\</u>	 \/\ \/\ 	FOILS REFLECTIVE BOTH SIDES	.13	.13	-11	.10	.09	.13	.13	.13	.13	.13	-11	.10	.09	.12	.12	.13
		FOILS REFLECTIVE ONE SIDE	.15	.15	.12	:11	.10	.15	.15	.15	.15	.15	.12	11.	.10	.14	.14	.15
		FOILS REFLECTIVE BOTH SIDES	.13	.13	.11	.10	.09	.13	.13	.13	.13	.13	.11	.10	.09	.12	.12	.13

APPENDIX A

CALCULATIONS

General

The tables on the preceding pages contain the overall heat transmission coefficients recommended for use in the computation of heat losses through building sections. In the tables covering building sections having no air spaces, or having air spaces bounded by ordinary materials, the coefficients have been calculated according to the procedure and formula recommended in the Heating, Ventilating and Air Conditioning Guide. In the tables for building sections containing air spaces faced one or both sides with reflective material, the calculations have been made according to the procedure outlined in Appendix D, "Calculation of Building Section Heat Transmission Coefficients", Technical Circular No. 7, Revised January 1947, published by the Federal Housing Administration, Washington, D. C.

The following notes apply to all tables:

- No allowance has been made for the resistance to heat flow provided by vapour barrier materials, since it is so small when compared with the total resistance of the whole wall section.
- 2. The inside surface conductance used is that for still air. The outside surface conductance used is that for a wind velocity of 15 miles per hour in tables for frame and masonry walls, and for ceilings and floors is that for still air.
- 3. With all types of insulation, the coefficients have been corrected for the influence of 2 by 4 studs on 16-inch centres. Corrections applied to floors and ceilings are noted in the tables.
- For frame and masonry walls with foil-backed interior finish and reflective insulation, the foil-backed interior finish has been considered as one of the reflecting surfaces.

Published yearly by the American Society of Heating and Ventilating Engineers, New York.

Overall Heat Transmission Coefficients of Building Sections

In the determination of the theoretical heat loss of buildings, the overall heat transmission of any building section, such as a wall, ceiling or floor, is expressed by the equation:

$$H= U \times A \times (t_1 - t_2)$$

where:

H = Heat loss, in B.t.u./ hour

U = Overall heat transmission coefficient, in B.t.u./ hour / sq. ft./ °F. difference between air temperatures inside and outside.

A = Area of section, in square feet.

t₁ = Average air temperature, inside, in °F.

to = Average air temperature, outside, in °F.

The surface area (A) of the building section, and the average air temperature inside and outside the section (t_1 and t_2) may be measured.

The determination of the theoretical overall heat transmission coefficient (U) however, is generally more difficult, especially for the more complex building sections. The calculation involves the use of a formula (see Page 22), and usually a reference to tables to ascertain the thermal conductivities of the materials involved, the thermal conductances of air spaces, and the interior and exterior surface conductance coefficients.

Symbols Used in Calculation of Overall Heat Transmission Coefficient

- k = thermal conductivity; the amount of heat transmitted in one hour through a one square foot area of homogeneous material one inch thick, for each degree F. temperature difference between the two surfaces of the material. Unit expressed in B.t.u./hour/ square foot/°F./inch of thickness.
- $\frac{1}{k}$ = Resistivity; the reciprocal of thermal conductivity of a homogeneous material one inch thick.
- x = Resistance; the reciprocal of thermal conductance of a homogeneous material "x" inches thick.

- C = Thermal conductance; the amount of heat transmitted in one hour through a one square foot area of material, or combination of materials of given thickness, for each degree F. temperature difference between the two surfaces. Unit expressed in B.t.u./hour/square foot/°F.
- $\frac{1}{C}$ = Resistance; the reciprocal of thermal conductance.
- f = Film or surface conductance; the amount of heat transmitted in one hour from one square foot surface to the air immediately adjacent to it (or from the air to the surface) for each degree F. temperature difference between the surface and the adjacent air. Unit expressed in B.t.u./hour/square foot/°F. Inside surface conductance is denoted by f1 and outside surface conductance by f0.
- $\frac{1}{f}$ = Film or surface resistance; the reciprocal of film or surface conductance.
- a = Thermal conductance of an air space; the amount of heat transmitted in one hour from one square foot of surface bounding one side of an air space to one square foot of surface bounding the opposite side of the air space for each degree F. temperature difference between the two surfaces.

 Unit expressed in B.t.u./hour/square foot/°F.
- 1 a = Resistance of an air space; the reciprocal of thermal conductance
 of an air space.
- U = Overall Heat Transmission Coefficient; the amount of heat transmitted in one hour through one square foot of a building section (wall, ceiling or floor) for each degree F. temperature difference between air on the inside and air on the outside of the building section.

 Unit expressed in B.t.u./hour/square foot/°F.
- $\underline{\underline{1}}$ = Overall Resistance; the reciprocal of the overall heat transmission coefficient.

Calculation of Overall Heat Transmission Coefficient

The overall heat transmission coefficient 'U' of a building section is equal to the reciprocal of the sum of the resistances of the individual materials, air spaces and surface films, comprising the building section. This is expressed by the equation:

$$U = \frac{1}{f_0} + \frac{x_1}{k_1} + \frac{x_2}{k_2} + \cdots + \frac{1}{c_1} + \frac{1}{c_2} + \cdots + \frac{1}{a_1} + \frac{1}{a_2} + \cdots + \frac{1}{f_1}$$

Where: $\frac{1}{f_0}$ = Resistance of outside surface film.

 $\frac{x_1}{k_1}$, $\frac{x_2}{k_2}$, etc. = Resistances of the materials having thickness x inches and thermal conductivity k.

 $\frac{1}{C_1}$, etc. = Resistances of the materials having thermal conductance C.

 $\frac{1}{a_1}$, $\frac{1}{a_2}$, etc. = Resistances of air spaces.

 $\frac{1}{f_1}$ = Resistance of inside surface film.

APPENDIX B

Conductance of Air Spaces, Faced Both Sides with Non-Reflective Materials

The amount of heat transferred across an enclosed air space depends upon several factors. Among these, the emissivity of the surfaces enclosing the air space, the difference in temperature across the air space, and the direction of heat flow, are the most important. The shape and width of an air space also affect the heat transfer but it has been found by experience that increasing the width beyond $\frac{3}{4}$ inches has a negligible effect upon the conductance of the air space.

In the following table, average conductance values are given for air spaces faced with ordinary materials, for the three directions of heat flow, viz., horizontal or lateral flow across a vertical air space, upward flow across a horizontal air space and downward flow across a horizontal air space. These figures are average values for air spaces having approximately parallel surfaces.

Average Conductance of Air Spaces Bounded by Approximately Parallel Surfaces of Ordinary Materials.

Direction of Heat Flow	Average Conductance (a)
Horizontal (wall) Upward (ceiling) Downward (floor)	1.10 1.32 .94

APPENDIX C

Conductance of Air Spaces Faced One or Both Sides with Reflective
Material

In order to function as insulation, reflective materials must always be accompanied by air spaces adjacent to the reflective surfaces. The width of air space generally recommended is from inch to inch and experience has shown that increasing the width beyond inches will have little or no effect on the insulating value. If this air space is not provided adjacent to the reflective surface the insulating value depends solely upon the thermal resistance of the reflective material itself, which, in practically all cases, is extremely low.

The reflective insulation tables in this booklet have been based on reflective material having an emissivity of .05. Should the surface become covered with dust, etc. to a degree which will raise its emissivity the insulating value will decrease in proportion. Should the emissivity approach .90, which is approximately the value for ordinary non-reflecting surfaces, the reflective materials would function, as insulation, simply as an air space bounded by ordinary materials.

The amount of heat transferred across an enclosed air space faced one or both sides with reflective material, as in the case of air spaces bounded by ordinary materials, depends upon the emissivity of the surfaces enclosing the air space, the difference in temperature across the air space, the mean temperature of the air space, the direction of heat flow and the width and shape of the air space.

A procedure for the calculation of the overall heat transmission coefficient of building sections containing air spaces faced one or both sides with reflective material has been evolved (2) based on the average effective emissivity of the air spaces faced with reflective material, the average temperature difference across the individual air spaces, and the sum of the resistances of the building section components other than the air spaces faced with reflective material. This procedure has been followed in this booklet in the computation of the overall heat transmission coefficients for building sections containing air spaces faced with reflective material, assuming an emissivity of .05 for the reflective material and an emissivity of .90 for the ordinary non-reflective surfaces.

In cases where it is desired to compute the overall heat transmission coefficient of building sections other than those given in this booklet without going through this detailed procedure, it may be sufficiently accurate to use the approximate figures given in the following table. These figures are based on the mean temperature of the air space, the temperature difference across the air space, and the resistance of the components other than the air spaces faced with reflective material which are to be found in "typical" frame wall, ceiling and floor constructions.

Approximate Conductances of Air Spaces Faced one or Both Sides With Reflective Material (emissivity = .05)

	Design	Temperation O°F.	ure 20°F.
Horizontal Heat Flow (Walls)			V
l space faced l side	.49	.46	.43
l space faced both sides	.48	.45	.42
2 spaces each faced 1 side	.23	.22	.20
2 spaces (1 faced 1 side) (1 faced both sides)	.22	.21	.20
3 spaces (2 faced 1 side) (1 faced both sides)	.14	.13	.12
3 spaces (1 faced 1 side) (2 faced both sides)	.14	.13	.12
4 spaces each faced one side	.10	.10	.09
Upward Heat Flow (Ceilings) (Attic space not considered as air space)			
l space faced l side	.68	.65	.60
2 spaces (1 faced 1 side) (1 faced both sides)	.31	.29	.27
3 spaces each faced 1 side	.20	.19	.17
3 spaces (2 faced 1 side) (1 faced both sides)	.19	.18	.16
4 spaces each faced 1 side	.14	.13,	.12
Downward Heat Flow (Floors) (Crawl space not considered as air space)			fa-
l space faced l side	。22	.21	.19
2 spaces each faced 1 side	.10	.09	.09
2 spaces (1 faced 1 side) (1 faced both sides)	.09	.09	.08
3 spaces each faced one side	.06	.06	.06

APPENDIX D

Film or Surface Conductance Values

The film of air in immediate contact with the surface of any material offers resistance to the passage of heat from the surface to the surrounding air, or vice versa. The thermal conductance of this air film is known as film or surface conductance, and its value depends upon various factors such as the physical nature of the surface, the direction of heat flow, the temperature of the surface, the temperature difference between the surface and surrounding air and the velocity of air passing over it. The surface conductance values given in this appendix are average values and are considered sufficiently accurate for all practical purposes.

Inside surface conductance values (f) are given for interior surfaces of average texture, and are based on still air. Where the interior finish has a highly reflective surface, the values given for the outside surface conductance of a highly reflective surface in still air may be used.

Outside surface conductance values (f_0) for moving air

are given for four types of surfaces, viz. "rough", such as stucce; "average " such as wood or brick; "smooth", such as glass; and "highly reflective", such as unpainted aluminum. The wind velocity is assumed to be 15 m.p.h. These values are used when the outside surface of the building section is exposed to the weather or, in the case of heat flow downward, when the floor section faces an unheated air space which is completely open; for example, the crawl space of a basementless structure not provided with foundation or curtain walls.

Outside surface conductance values (f₀) for still air are given for average, smooth and highly reflective surfaces. These are used when the outside surface of the building section faces an unheated and vented air space in which the air temperature is assumed to be virtually the same as outside air temperature and the air movement is low enough to be considered as still air; for example, a vented attic space between roof and ceiling, or a vented crawl space of a basementless structure.

Inside Surface Conductance fi

Direction of Feat Flow	Average Conductance
Horizontal (wall) Upward (ceiling) Downward (floor)	1.65 1.95 1.20

Outside Surface Conductance fo

Direction of Heat Flow	Me	oving Air	(15 m.p.h	. Wind)
	Rough Surface	Average Surface	Smooth Surface	Reflective Surface
Horizontal (wall) Upward (roof) Downward (floor)	9.09 9.09 9.09	6.00 6.00 6.00	4.50	5.25 5.25 5.25
Direction of Heat Flow		Still A	ir	
		Average Surface		Reflective Surface
Horizontal (wall) Upward (ceiling) Downward (floor)		1.65 1.95 1.20	1.50	.74 1.16 .44

APPENDIX E

Values for Thermal Conductivity (k) and Thermal Conductance (C) of Common Building Materials

Conductivity (k) expressed in B.t.u./square foot/deg. F. /inch of thickness.

Conductance (C) expressed in B.t.u./square foot/deg. F. for the thickness stated or commonly used.

The following figures indicate values, or the range of values, of "k" and "C" which are generally accepted for the calculation of heat losses.

	°k°	3 C 8
Exterior Finish		
Aluminum Clapboard Asbestos Shingles Asphalt Shingles	1475	6.00 6.66
Brick - common - 4" thick	5.00 9.00	-
Building Paper Insulated Siding (Imitation Brick) Stone	12.50	5.50 .78
Stucco	12.50	1.28 1.28 12.50 2.12 1.59 12.50
Masonry Material		
(Brick - common	5.00 9.00 12.50 12.50 2.96 4.055 4.55 2.44 12.50 1.60	

	'k'	1C1
Hollow Clay Tile - 3"		1.28 1.00 .64 .60 .58 .40
Hollow Concrete Blocks		
Cinder Aggregate - 3"		1.28 1.00 .60 .53
Clay or Slag Aggregate - 8"		.50
Sand and Gravel Aggregate - 4"		1.43 1.00 .80 .61
Roofing Material		
Asbestos Shingles	10.00	6.00 6.66 6.66 1.28
Sheathing		
Building Paper	•33	5.50 - 2.56 2.82 1.02 .86
Insulating Materials - Batts, Blankets or Fill		
Cotton	.24 to .30 .25 to .26 .48 .27 to .33 .26 to .31	** ** ** ** ** ** ** ** ** ** ** ** **

Insulating Materials Rigid Insulation	¹k¹	1C1
Corkboard	.25 to .34 .40 .27 .23 .33 .46 to .77	
Interior Finish		
Gypsum Plaster	3.30 .33 .80	3.23 2.12 3.70 2.82 2.40 4.40 2.50
Flooring Materials		
Maple or Oak Pine or Fir Plywood Vitreous Tile or Terrazzo 1/4" Linoleum 1/2" Plywood 25/32" Pine or Fir 13/16" Maple or Oak	1.15 .80 .80 12.50	1.35 1.59 1.02
Asphalt Tile	650	1.40

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