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MANOEUVRING MODEL TESTS OF THE USCGC HEALY (MODEL 546) IN LEVEL ICE

LM-2006-03

Michael Lau

March 2006

ABSTRACT

A complete set of resistance, propulsion, and manoeuvring model tests of the USCGC Healy (Model 546) were conducted in 2001 for correlation with the full-scale data collected during the sea trial of the same vessel conducted in the previous year (Frederking et al, 2001). Jones (2005) has reported the results of the resistance and propulsion portions of the model test series. This report, accompanying the fore-mentioned report, documents the result of the manoeuvring tests.

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MANOEUVRING MODEL TESTS OF THE USCGC HEALY (MODEL 546) IN LEVEL ICE

1.0 INTRODUCTION

A complete set of resistance, propulsion, and manoeuvring model tests of the *USCGC Healy* (Model 546) were conducted in 2001 for correlation with the full-scale data collected during the sea trials of the same vessel conducted in the previous year (Frederking et al, 2001). Jones (2005) and Jones and Lau (2006) have reported the results of the resistance and propulsion portions of the model test series. This report, accompanying the fore-mentioned report, documents the results of the manoeuvring tests.

2.0 USCGC HEALY

The *USCGC Healy* was launched on November 15, 1997, from Avondale Industries in New Orleans. She was delivered to the US Coast Guard on November 10, 1999, departed New Orleans on January 26, 2000, and proceeded north for extensive full-scale ice trials before arriving in Seattle on August 9, 2000.

The essential details of the *Healy* are shown in Table 1.

Table 1. Characteristics of *USCGC Healy*

Length, Overall	420 ft (128 m)
Beam, Maximum	82 ft (25 m)
Draft, Full Load	29 ft 3 in (8.9 m) at delivery
Displacement, Full Load	16,000 LT at delivery
Propulsion	Diesel Electric, AC/AC Cycloconverter
Generating Plant	4 Sultzer 12Z AU40S
Drive Motors	2 AC Synchronous, 11.2 MW
Shaft Horsepower	30,000 Max
Propellers	2 fixed pitch, 4 bladed
Fuel Capacity	1,220,915 gal. 4,621,000 L
Speed	17 knots @ 147 RPM
Endurance	16,000 NM @ 12.5 knots
Icebreaking Capability	4.5 ft (1.4 m) @ 3 knots (continuous) 8 ft (2.44 m) Backing and Ramming
Accommodations	19 Officers, 12 CPO, 54 Enlisted, 35 Scientists, 19 Surge, 2 Visitors

The designed icebreaking capability of the *Healy* was for continuous icebreaking at 3 knots through 4.5 ft (1.37 m) of ice of 100 psi (690 kPa) strength. The full-scale trials were designed to test this capability.

2.1 Model Construction

Model 546 was constructed, in accordance with IOT's standard method, at a scale of 1:23.7. This scale was chosen so that we could use an existing set of propellers, namely our R-Class propellers 66L and 66R. The model's principal dimensions were:

Table 2. Particulars of Model 546

Overall length (LOA)	5.40 m
Length between perpendiculars (LBP)	5.10 m
Maximum beam	1.05 m
Depth at midships (D)	0.54 m
Design waterline (DWL)	0.36 m
Draft at even trim	0.37 m
Vertical C. of G. (VCG)	0.416 m
Displacement	1240 kg

A non-removable ice knife and two bossings, also non-removable, were fitted, together with the twin rudders and propellers. The model's lines plan is shown in Figure 1, the model is shown in the ice tank in Figure 2, and the stern arrangement is shown in Figure 3.

The manoeuvring tests were conducted at a friction coefficient of 0.034, corresponding to the high friction resistance tests conducted during the earlier phase (Jones, 2005). The ice density was maintained constant for two ice sheets (see Table 3, Sheets Healy17 and Healy18) at $867 \pm 1 \text{ kg/m}^3$. For unknown reasons, one ice sheet (Healy16) had a higher density of 916 kg/m^3 .

USCGC Healy (Model 546) in Ice

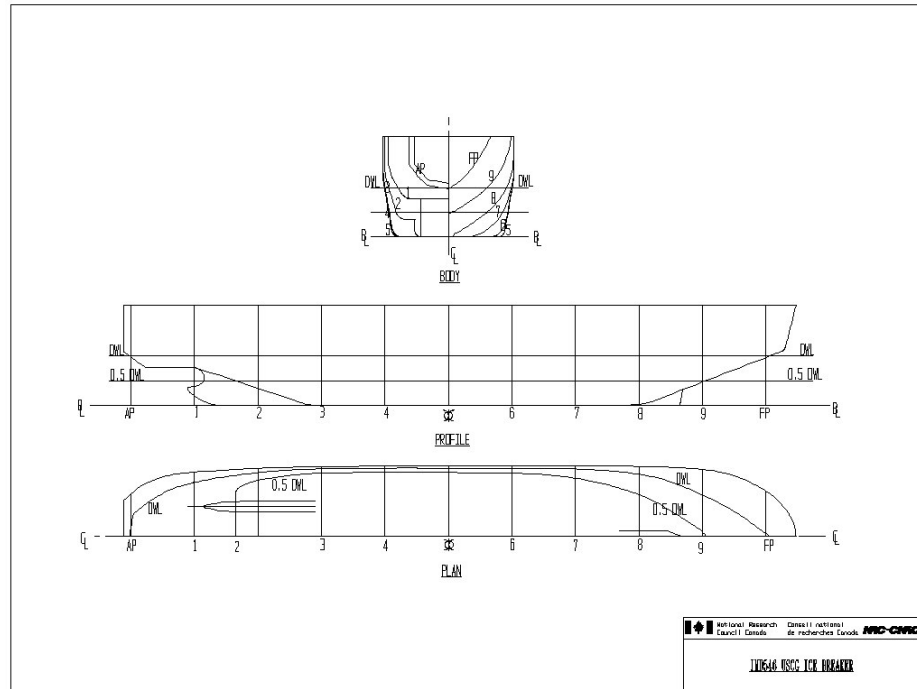


Figure 1. Lines plan of *USCGC Healy*

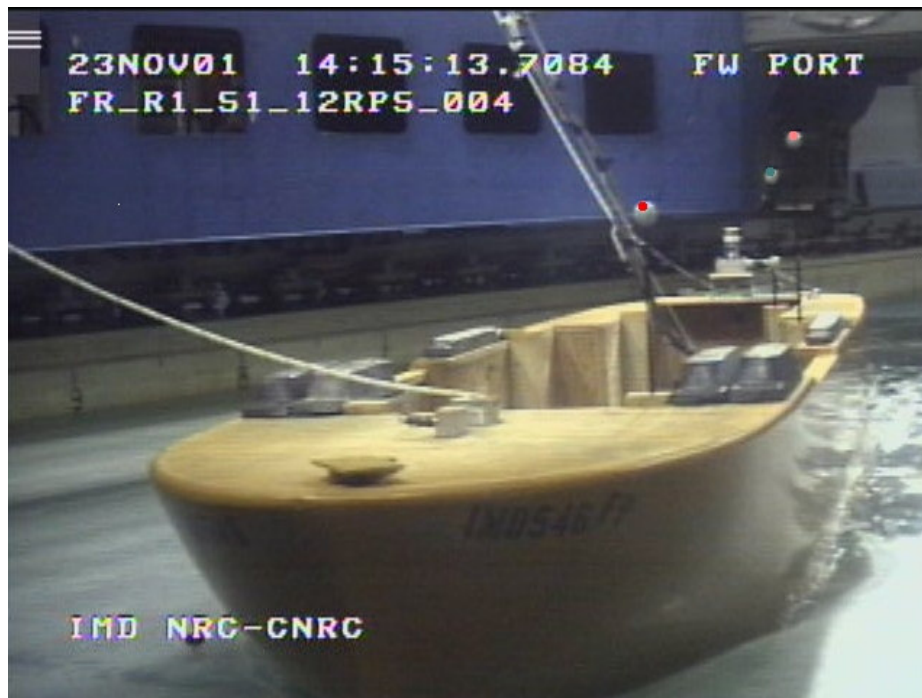


Figure 2. The *Healy* Model 546 shown in the ice tank



Figure 3. The stern arrangement of the *Healy* Model 546

3.0 TEST PLAN

A total of 8 self-propelled manoeuvring runs were conducted in the three ice sheets. In addition, open water bollard (overload tests carried out at zero speed) and shaft friction tests were conducted. Selected test conditions from the sea trial were duplicated for the manoeuvring tests and the turning diameters were measured. Performance predictions were then made and compared to the full-scale data previously collected. Table 3 shows details of the three ice sheets (given in full scale) that were used for the tests. Table 4 summarizes the test conditions and the results for each run. The first three runs were conducted at a target ice thickness of 75 cm and an ice strength ranging from 483 to 683 kPa. Shaft speed was varied from 9 to 10 to 12 rpm for these runs. The rest of the tests were conducted at a target ice thickness of 100 cm and an ice strength ranging from 417 to 1081 kPa. The rudder angle was kept at 30 degrees, the same as that used in the sea trial. The delivered power was kept at around 30,000 hp for most tests, which was consistent with the delivered power employed during the sea trial.

Table 3. Details of ice sheets used

Name	Date	Thickness (h)	Strength (σ_f)	Density	E/σ_f
		cm	kPa	Mg/m ³	
Healy16	23 Nov 01	74	562	0.916	1938
Healy17	27 Nov 01	100	749	0.866	2156
Healy18	29 Nov 01	97	667	0.868	1256

Table 4. Summary of test results

Run	Shaft rpm	Ice Thickness	Ice Strength	Turning Diameter	Rudder Angle	Power	HP
	rpm	cm	kPa	m	degree	kW	hp
Healy16-1	12	74.9	519	1321	29.6	22703	30433
Healy16-2	10	74.7	683	1329	29.9	14592	19560
Healy16-3	9	73.7	483	1337	30.4	9291	12455
Healy17-1	12	99.1	1081	1756	30.1	19551	26208
Healy17-3	12	100.7	417	1757	29.9	18546	24860
Healy18-1	12	96.7	621	1738	29.7	23698	31767
Healy18-2	12	97.4	751	1738	29.6	24228	32478
Healy18-3	12	97.6	628	1745	29.8	23630	31676

4.0 RESULTS

The detailed test log, the statistics, and the time histories for each test run are given in Appendix A. The ice sheet details are given in Appendix B.

4.1 Turning Circle Diameter

The channel profile was measured immediately after each test in one-meter intervals along the x-axis of the tank. The diameters corresponding to the inner and the outer channel edges were computed from a set of x-y coordinate pairs based on the least squared method. Details of the channel data are given in Appendix C. The turning diameter for each run is given in Table 4.

4.2 Power Level

The delivered power, $P_D = \pi \sum Q_i rps_i$, was computed from the measured torque, Q_i , and the shaft's rps, rps_i , where the subscript i denotes the port or starboard propulsion, and then scaled up to full-scale. The delivered power is given in Table 4.

4.3 Full-Scale Sea Trials

The sea trial results have been reported in Frederking et al (2001). They are summarized in Table 5 for completeness.

Table 5. Summary of manoeuvring runs from the sea trials

Test #	Ice Thickness Cm	Power HP	Diameter m	Dia./B	h/B	Dia/L
000420_1740	87	20780	1538	61.5	0.0348	12.0
000421_1348	95	28377	1538	61.5	0.0380	12.0
000421_1901	95	28830	1388	55.5	0.0380	10.8
000506_0015	140	23848	1666	66.6	0.0560	13.0
000515_1258	132.5	29254	2174	87.0	0.0530	17.0
000515_1400	132.5	29414	2128	85.1	0.0530	16.6
000515_1532	70.5	27222	470	18.8	0.0282	3.7
000515_1532	70.5	23234	528	21.1	0.0282	4.1
000515_1532	70.5	23440	1142	45.7	0.0282	8.9
000515_1615	70.5	29299	1274	51.0	0.0282	10.0
Average	96.4	26370	1385	55.4	0.0386	10.8

4.4 Comparison With Full-Scale Data

Figure 4 gives the non-dimensional turning diameter as a function of the non-dimensional ice thickness for the model and full-scale data. Despite the discrepancy in ice strength and power level tested between the model tests and sea trials, the model test data agree well with the sea trial data except for the three data points identified in the figure. These 3 outliers should be further investigated; they are possibly due to large-scale cracks in the ice sheet.

A multi-variance regression of the turning diameter conducted for the eight test runs as a function of ice thickness, ice strength, and the power level gives the following equation:

$$D = -2.502 + 21.67h_i - 0.226\sigma_f - 0.0095P_D \quad (1)$$

where D is the turning diameter (m), h_i is the ice thickness (cm), σ_f is the flexural strength of ice (kPa), and P_D is the power level (kW). The influences of ice thickness and delivered power on the turning circle are expected; however, it is not clear why increasing ice strength would result in decreasing turning diameter. In any case, the model test data show only a slight influence of ice strength on the turning diameter.

Full-scale turning circle diameters obtained from similar ice thicknesses, i.e., Runs 00515_1532, 00515_1615, 00421_1348, and 00421_1901, were selected for direct comparison with the model test data. Table 6 gives the turning diameters computed from Equation 1 and their corresponding full-scale measurement for the selected runs. Despite a small sample size, the comparison shows consistency.

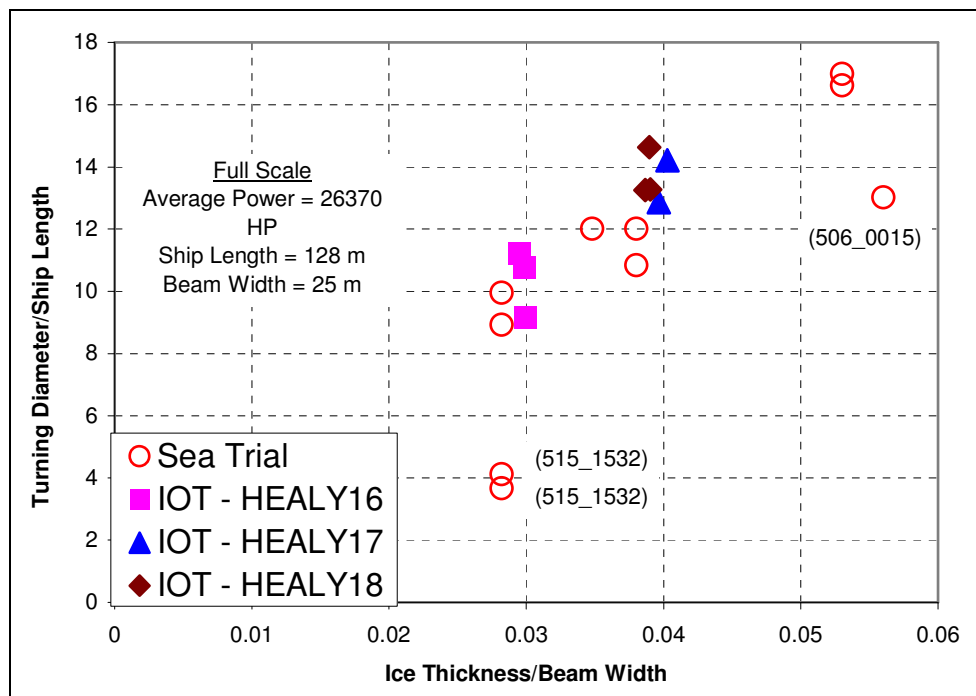


Figure 4. The non-dimensional turning diameter as a function of non-dimensional ice thickness for the sea trial and model test data

Table 6. Predictions from model test data (Equation 1) in comparison with selected full-scale data measurements

Test	Prediction from Model Scale Data (Equation 1)							Measured Average Dia./L
	Ice Thickness	Ice Strength	Average Power	Average Diameter, Dia.	Dia./B	h/B	Dia./L	
#	Cm	kPa	HP	m				
00515_1532 & 00515_1615	70.5	300	26370	1208	48.3	0.0282	9.4	9.4
00421_1348 & 00421_1901	95	262	28600	1726	69.0	0.038	13.5	11.4

5.0 DISCUSSIONS AND CONCLUSION

An analysis of the *USCGC Healy* manoeuvring tests data showed a good correlation between the model tests and the sea trial results. Multi-variance regression was performed with the model test data and the result compared with selected full-scale measurements. The turning diameter obtained during the model tests was the same in one case and slightly larger than its counterpart measured at sea trial in another case. The three outliers associated with the sea trial results (identified in Figure 4) warrant closer re-examination of these data points. The hull friction (0.034) used in the model tests was slightly lower than the target of 0.05. The effect of this discrepancy was not incorporated in the analysis.

6.0 REFERENCES

- Frederking, R., Kubat, I., and G. Timco (eds.), 2001. *Proceedings of POAC '01*, National Research Council of Canada, Ottawa, Vol. 2, p.891-973.
- Jones, S.J., 2005. "Resistance and propulsion model tests of the USCGC Healy (model 546) in ice," Institute for Ocean Technology Report LM-2005-02, National Research Council of Canada, St. John's.
- Jones, S.J., and Lau, M., 2006. "Propulsion and Manoeuvring Model Tests of the *USCGC Healy* in ice and correlation with full-scale," *International Conference and Exhibition on Performance of Ships and Structures in Ice*, July 16-19, 2006, Banff, Alberta.

Appendix A

Test log, data statistics and time histories

Test Log

TEST NAME	DAS FILE NAME	DATE	START TIME	DAC_TEST_DESCRIPTION	SEL_T1	SEL_T2	Carriage Tach Velocity	Rudder Angle	PORT THRUST	STBD THRUST	PORT TORQUE	STBD TORQUE	PORT RPS	STBD RPS	Pitch	Roll
					s	s	m/s	deg	N	N	Nm	Nm	rps	rps	deg	deg
Healy 16-1	fr_r1_s1_12rps_004	23-Nov-01	14:14:25	12rps (FRM) 30mm 30kpa	33.88	46.74	0.83	30	61.9	20.3	4.1	-1.5	-12.1	12.1	0.5	2.5
Healy 16-2	fr_r2_s1_12rps_006	23-Nov-01	15:07:27	12rps (FRM) 30mm 30kpa run 2	75.56	97.08	1	30.4	43.6	18.2	3	-0.9	-10	10.3	0.3	2.5
Healy 16-3	fr_r2_s1_9rps_007	23-Nov-01	15:39:14	9rps (FRM) 30mm 30kpa run 3	92.38	119.6	0.85	30.9	37.3	14.5	2.4	-0.7	-8.9	9.2	0.2	2.4
Healy 17-3	fr_r4_s2_12rps_011	27-Nov-01	15:20:48	12rps (FRM) 40mm 40kpa run 4	63.2	89.36	1.03	30.4	62.7	71.8	3.7	-1.2	-12	12.2	0.6	2.8
Healy 18-1	fr_r1_s3_12rps_014	29-Nov-01	13:03:45	sheet 3 healy17 40mm30kpa run 1 12rps	52.78	77.58	0.81	30.2	70.5	68.5	4.1	-1.8	-12	12.3	0.6	2.5
Healy 18-2	fr_r2_s3_12rps_015	29-Nov-01	13:50:53	sheet 3 healy17 40mm30kpa run 2 12rps	56.06	78.16	1.09	30.1	69.8	68.1	3.9	-1	-12.1	12.4	0.6	2.4
Healy 18-3	fr_r3_s3_12rps_016	29-Nov-01	14:50:14	sheet 3 healy17 40mm30kpa run 3 12rps	60.56	81.08	1.02	30.1	68.3	69.2	5.1	-1.4	-12.1	12.3	0.6	4.4

----- Tare Segment -----

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 Segment End Time = 13.240 seconds

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Video Sync	volts	0.36637	0.38514	0.37927	0.0016840	1
Carriage Tach Velocity	m/s	-0.0065273	0.011493	0.0010224	0.0015123	2
Rudder Angle	deg	0.016981	0.75620	0.37418	0.060126	3
PORT THRUST	N	0.43570	7.1624	3.7839	1.5612	4
STBD THRUST	N	-0.16193	3.5741	1.8729	0.66534	5
PORT TORQUE	Nm	-0.16579	0.17840	0.038439	0.075756	6
STBD TORQUE	Nm	-0.030992	0.077475	0.027308	0.011643	7
PORT RPS	rps	0.039387	0.18551	0.091698	0.010514	8
STBD RPS	rps	-0.15524	0.091353	-0.0078290	0.018863	9
pitch	deg	-0.11294	0.29574	-0.0057787	0.10026	10
Roll	deg	-0.55483	1.0880	0.36496	0.43738	11

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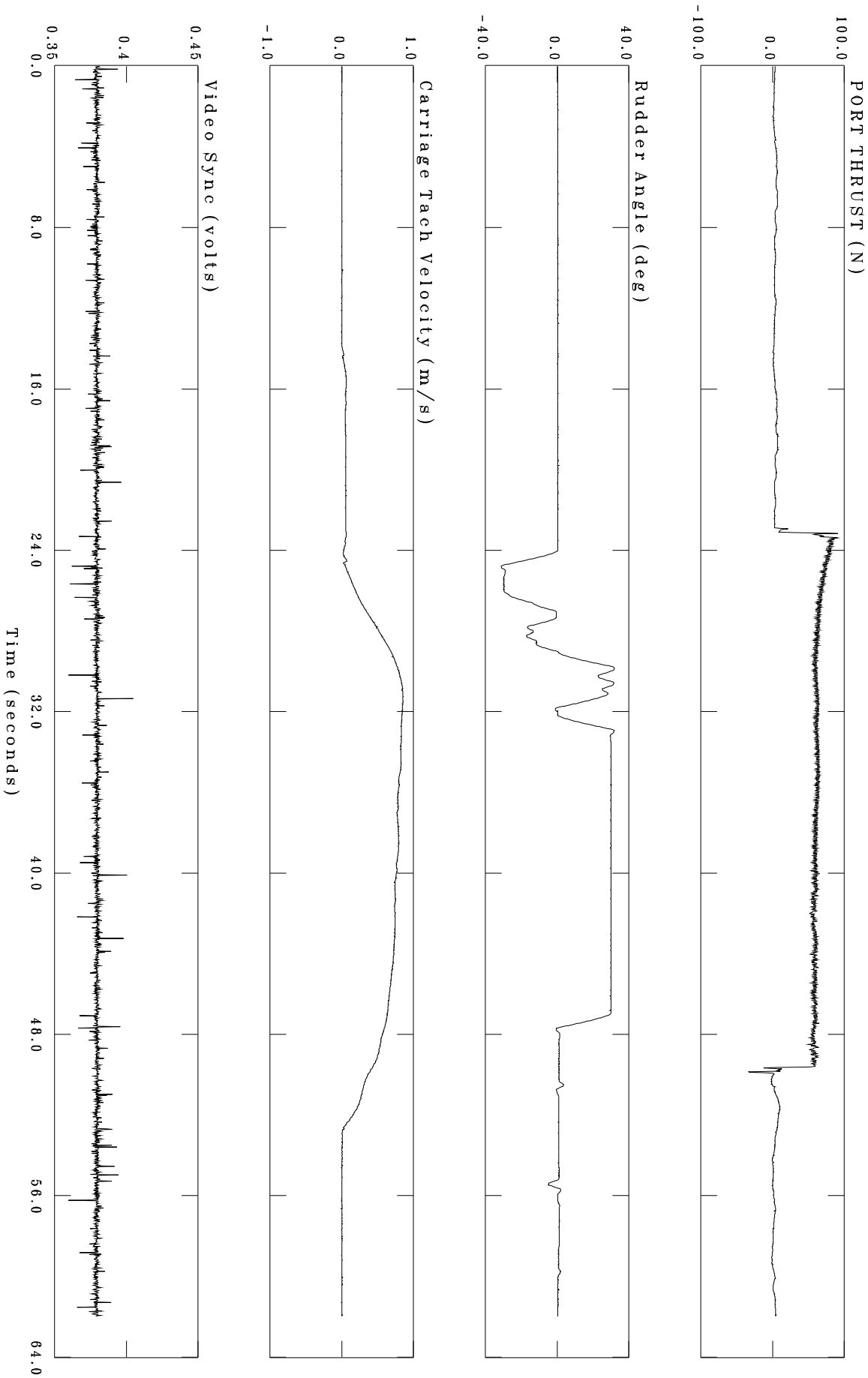
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 Segment End Time = 46.740 seconds

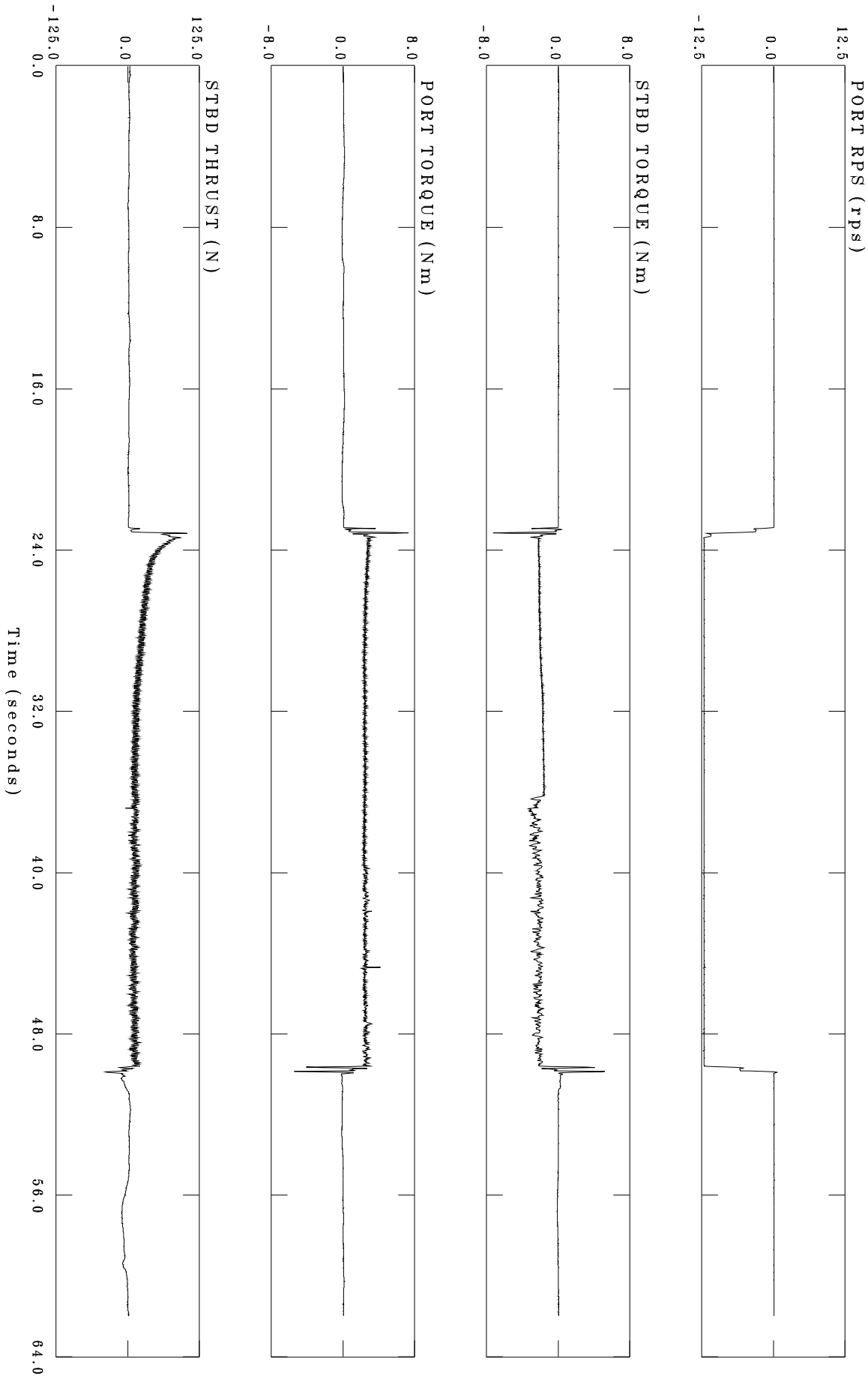
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Rudder Angle	deg	29.597	30.336	29.948	0.043089	3
PORT THRUST	N	51.618	65.713	59.948	2.7533	4
STBD THRUST	N	-3.8572	22.186	11.415	4.5003	5
PORT TORQUE	Nm	2.0318	4.1665	2.4530	0.16152	6
STBD TORQUE	Nm	-3.2992	-1.4962	-2.1703	0.40355	7
PORT RPS	rps	-12.215	-11.972	-12.090	0.022808	8
STBD RPS	rps	11.755	12.126	11.978	0.042837	9
pitch	deg	-0.12908	0.48305	0.16581	0.10385	10
Roll	deg	-1.8559	2.8898	0.44961	0.78684	11

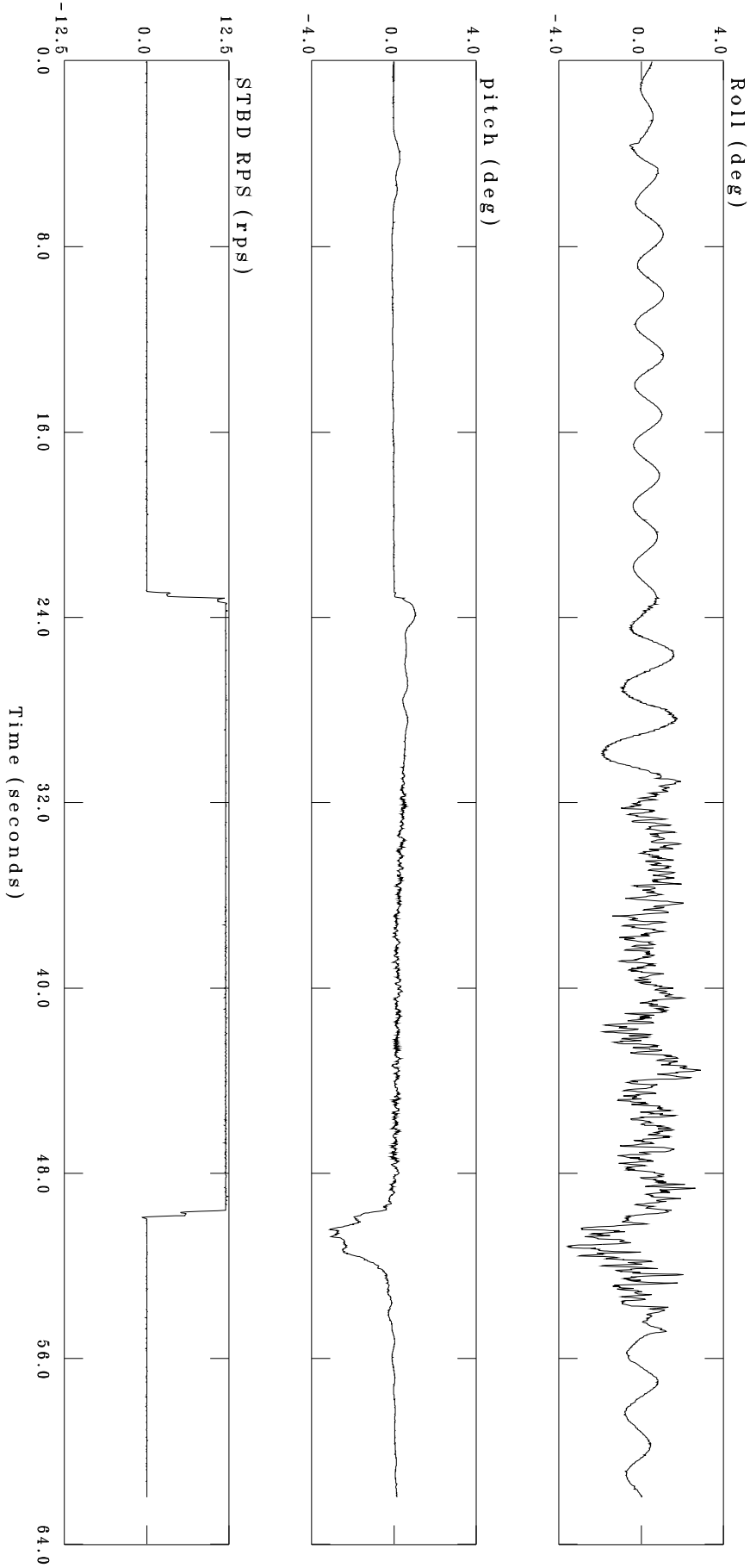
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 Segment End Time = 46.740 seconds

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Video Sync	volts	-0.013812	0.021131	0.00030134	0.0019196	1
Carriage Tach Velocity	m/s	0.64270	0.82679	0.75178	0.045787	2
Rudder Angle	deg	29.223	29.962	29.574	0.043089	3
PORT THRUST	N	47.835	61.929	56.164	2.7533	4
STBD THRUST	N	-5.7301	20.313	9.5417	4.5003	5
PORT TORQUE	Nm	1.9934	4.1281	2.4145	0.16152	6
STBD TORQUE	Nm	-3.3265	-1.5236	-2.1976	0.40355	7
PORT RPS	rps	-12.306	-12.063	-12.182	0.022808	8
STBD RPS	rps	11.763	12.134	11.986	0.042837	9
pitch	deg	-0.12330	0.48883	0.17159	0.10385	10
Roll	deg	-2.2208	2.5249	0.084649	0.78684	11







----- Tare Segment -----

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Ladder Angle	deg	-0.51731	0.2P686	-0.11963	0.058872	3
ROTI TFUST	N	-0.677P9	P.3376	2.67P1	1.8111	8
STBD TFUST	N	-13.595	3.9730	-2.0875	8.3512	5
ROTI TOQUE	Nm	-0.16961	0.125P0	-0.01061P	0.0732P7	P
STBD TOQUE	Nm	-0.10503	0.099768	0.0132P1	0.0378P2	7
ROTI RS	r/s	0.000P3P57	0.1P371	0.07P05P	0.010629	9
STBD RS	r/s	-0.197P8	0.17565	0.0072032	0.025P67	6
Pitch	deg	-0.16699	0.25966	0.0095110	0.075P83	10
Roll	deg	-0.2P9P6	0.71178	0.25113	0.21035	11

----- Before Taring -----

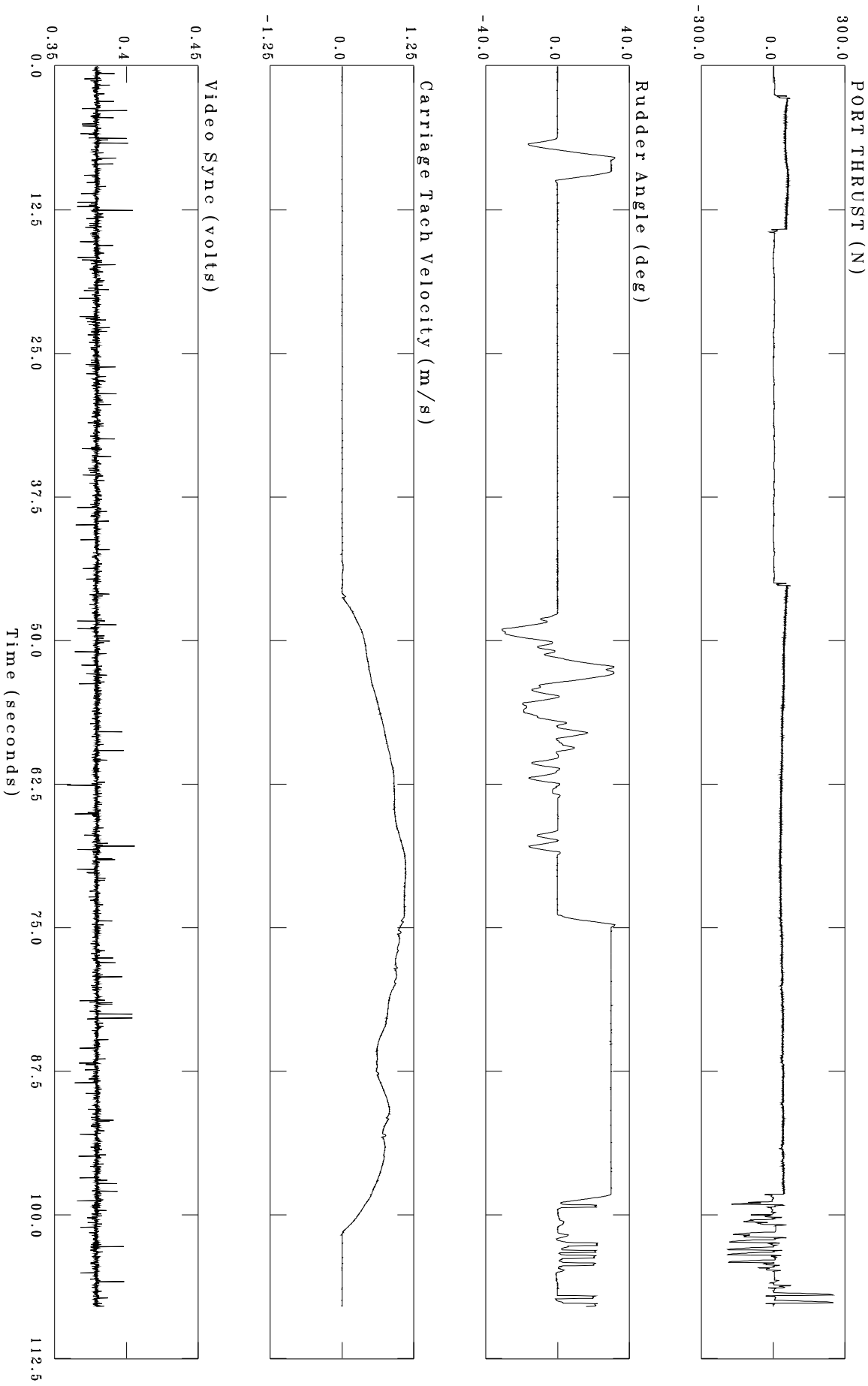
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 Output File = P-H-2_S1_12-RS_00P.DAT
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 Segment Start Time = 75.5P0 seconds
 Segment End Time = 67.090 seconds

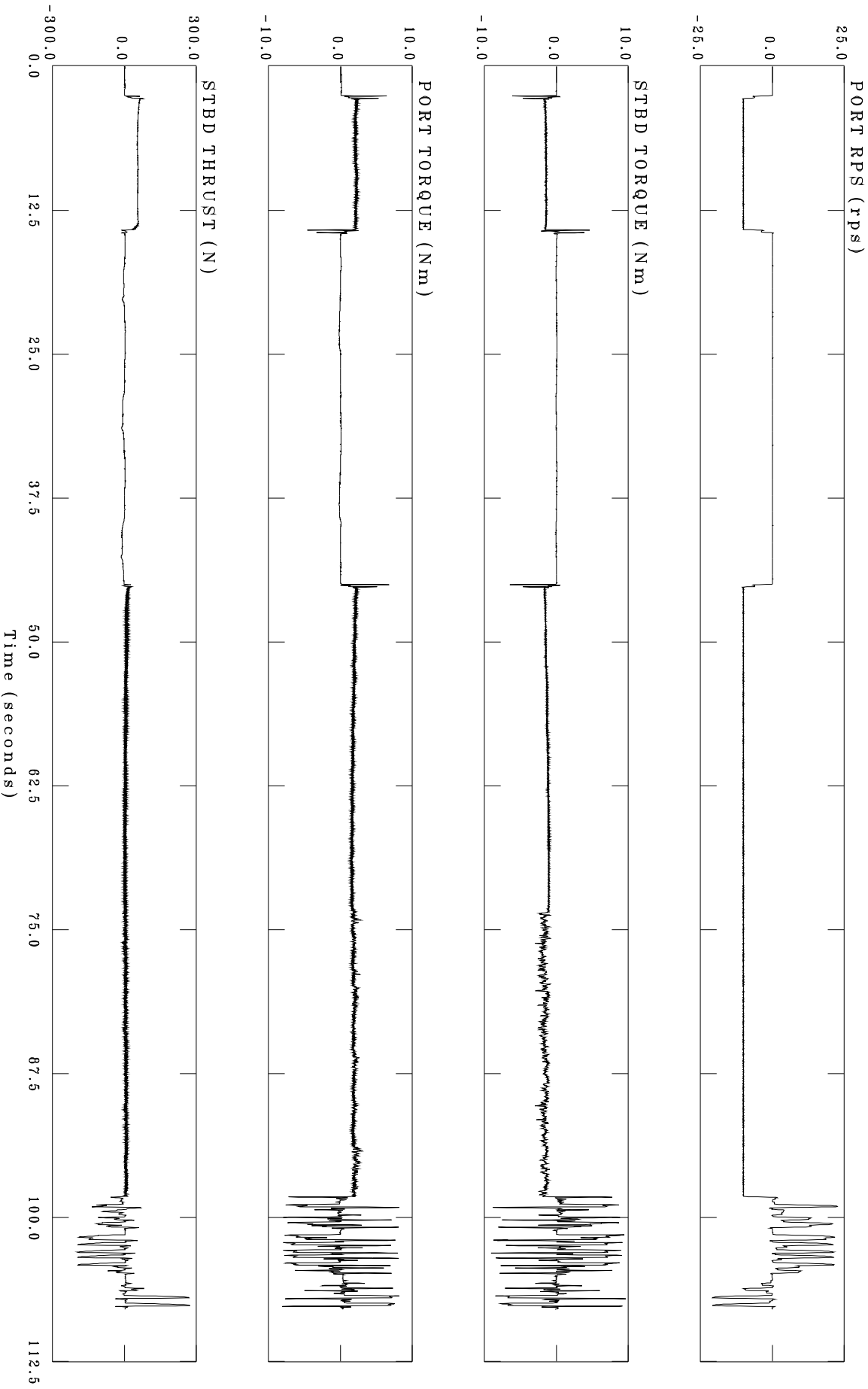
Description	Unit	Min	Max	Mean	S.D.	Chan
Video Sync	volts	0.3P363	0.80821	0.37636	0.0022862	1
Carriage Tach Velocity	m/s	0.56881	1.0011	0.77181	0.11P57	2
Ladder Angle	deg	26.356	30.256	26.762	0.083P10	3
ROTI TFUST	N	2P.021	8P.P16	36.870	2.679P	8
STBD TFUST	N	-9.7752	1P.192	5.5151	8.7507	5
ROTI TOQUE	Nm	1.8970	2.6888	1.6150	0.20983	P
STBD TOQUE	Nm	-2.6775	-0.98790	-1.1P207	0.3207P	7
ROTI RS	r/s	-10.210	-6.6726	-10.0P8	0.023852	9
STBD RS	r/s	6.7517	10.386	6.69P8	0.086P07	6
Pitch	deg	-0.25231	0.35081	0.083068	0.068966	10
Roll	deg	-2.7876	2.7317	0.16607	0.90973	11

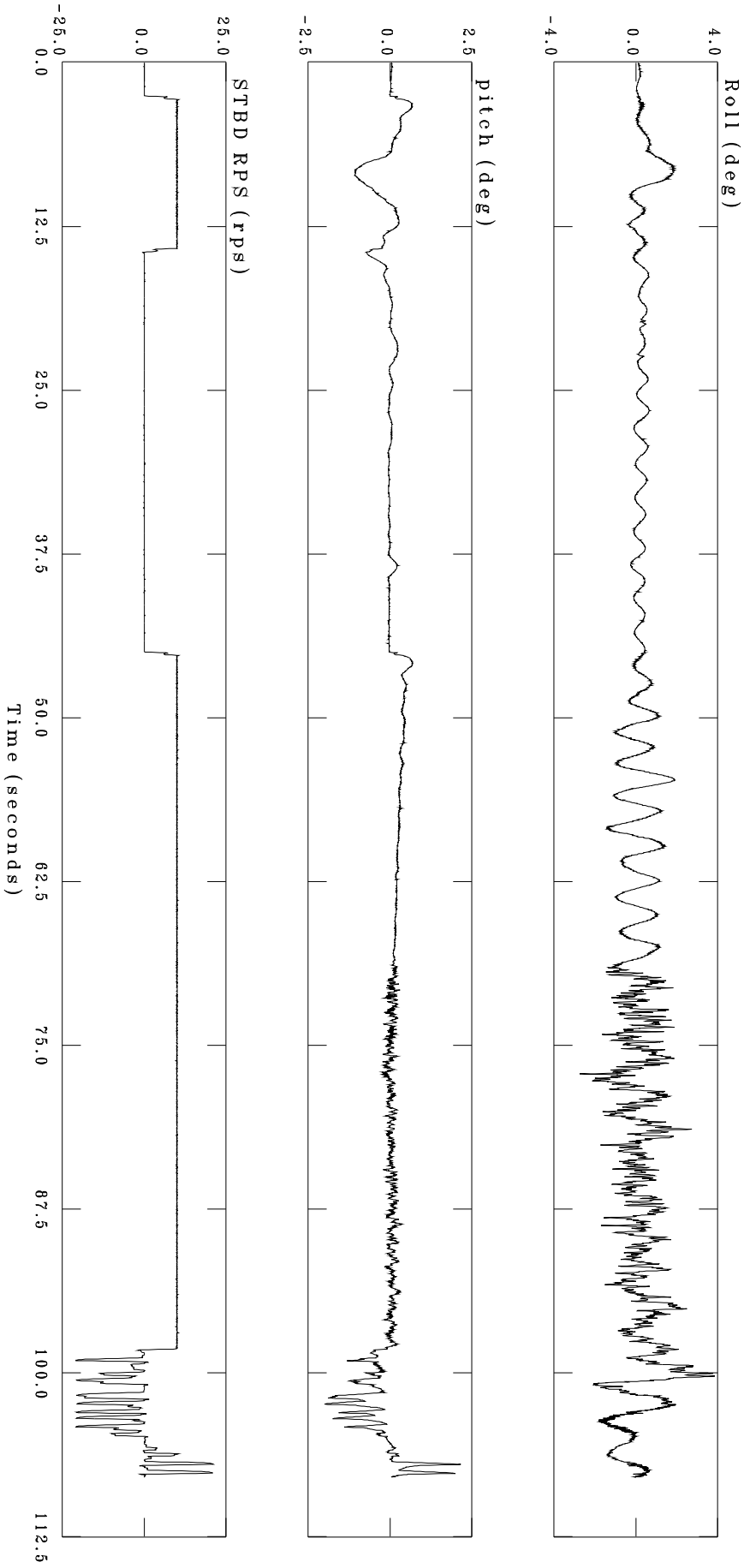
----- After Taring -----

Analysis Date/Time = 17-DEC-2005 13:30:0P
 Acquired Date/Time = 23-NOV-2001 15:07:27
 Input File = CF_S2_TA^ED
 Output File = P-H-2_S1_12-RS_00P.DAT
 Number of Samples = 1077
 Segment Start Time = 75.5P0 seconds
 Segment End Time = 67.090 seconds

Description	Unit	Min	Max	Mean	S.D.	Chan
Video Sync	volts	-0.015227	0.025057	0.00023935	0.0022862	1
Carriage Tach Velocity	m/s	0.56302	0.66672	0.77002	0.11P57	2
Ladder Angle	deg	26.879	30.379	26.611	0.083P10	3
ROTI TFUST	N	23.088	83.P83	3P.868	2.679P	8
STBD TFUST	N	-P.7277	19.226	7.5P2P	8.7507	5
ROTI TOQUE	Nm	1.8676	2.6553	1.62P0	0.20983	P
STBD TOQUE	Nm	-2.6609	-0.9P10P	-1.1P380	0.3207P	7
ROTI RS	r/s	-10.29P	-10.086	-10.180	0.023852	9
STBD RS	r/s	6.7885	10.382	6.6762	0.086P07	6
Pitch	deg	-0.2P092	0.38160	0.038593	0.068966	10
Roll	deg	-2.6661	2.890P	-0.0520P7	0.90973	11







----- Tare Segment -----

Analysis Date/Time = 17-DEC-2005 13:31:30
 Acquired Date/Time = 23-NOV-2001 15:34:11
 InPut Hile = C_S1
 OutPut Hile = HP2_S1_4P_S_007_DAT
 NumOer f6 Samples = 785
 Segment Start Time = 23.720 secnds
 Segment End Time = 34.000 secnds

Descriptifn	Unit	Min	Max	Mean	S_D_b	Chan
Videf Sync	vflts	0.38500	0.34124	0.37941	0.0014239	1
Carriage Tach Velfcity	m/s	-0.0091848	0.011418	0.0017007	0.0025024	2
Pudder Angle	deg	-0.91300	-0.21357	-0.55295	0.015828	3
* OPT T_PUST	N	2.0323	9.3741	5.1243	1.5142	1
STBD T_PUST	N	0.78112	8.2505	2.4037	1.2053	5
* OPT TOPQUE	Nm	0.18430	0.81841	0.55713	0.012517	8
STBD TOPQUE	Nm	-0.031785	0.081111	0.017422	0.015737	7
* OPT P_S	rFs	-0.095715	0.085221	-0.017994	0.010275	9
STBD P_S	rFs	-0.083113	0.27145	0.049290	0.022311	4
Fitch	deg	-0.051210	0.14133	0.035793	0.059291	10
Pfll	deg	-0.078445	0.18355	0.18841	0.12150	11

----- Before Taring -----

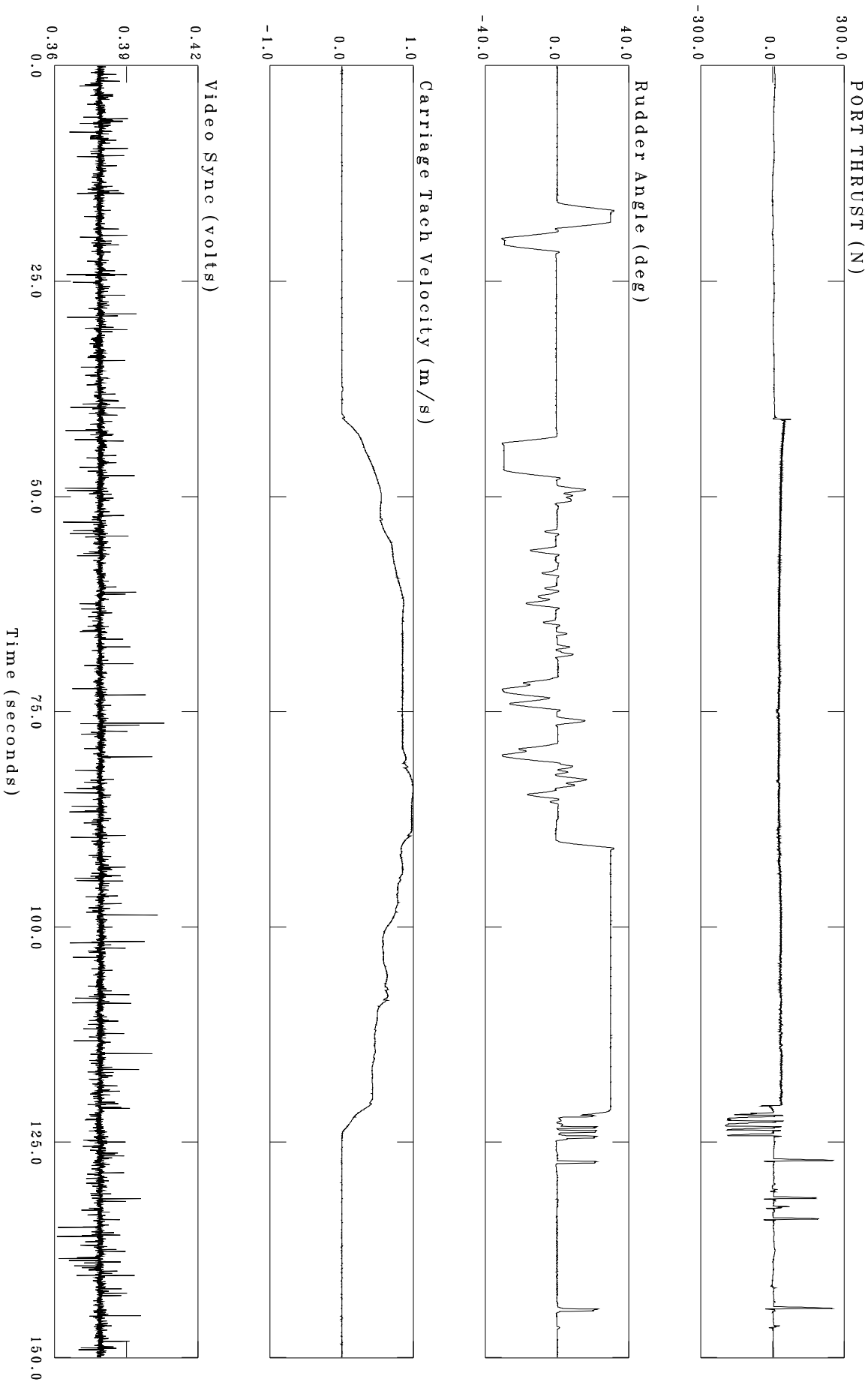
Analysis Date/Time = 17-DEC-2005 13:31:32
 Acquired Date/Time = 23-NOV-2001 15:34:11
 InPut Hile = C_S2
 OutPut Hile = HP2_S1_4P_S_007_DAT
 NumOer f6 Samples = 1382
 Segment Start Time = 42.390 secnds
 Segment End Time = 114.80 secnds

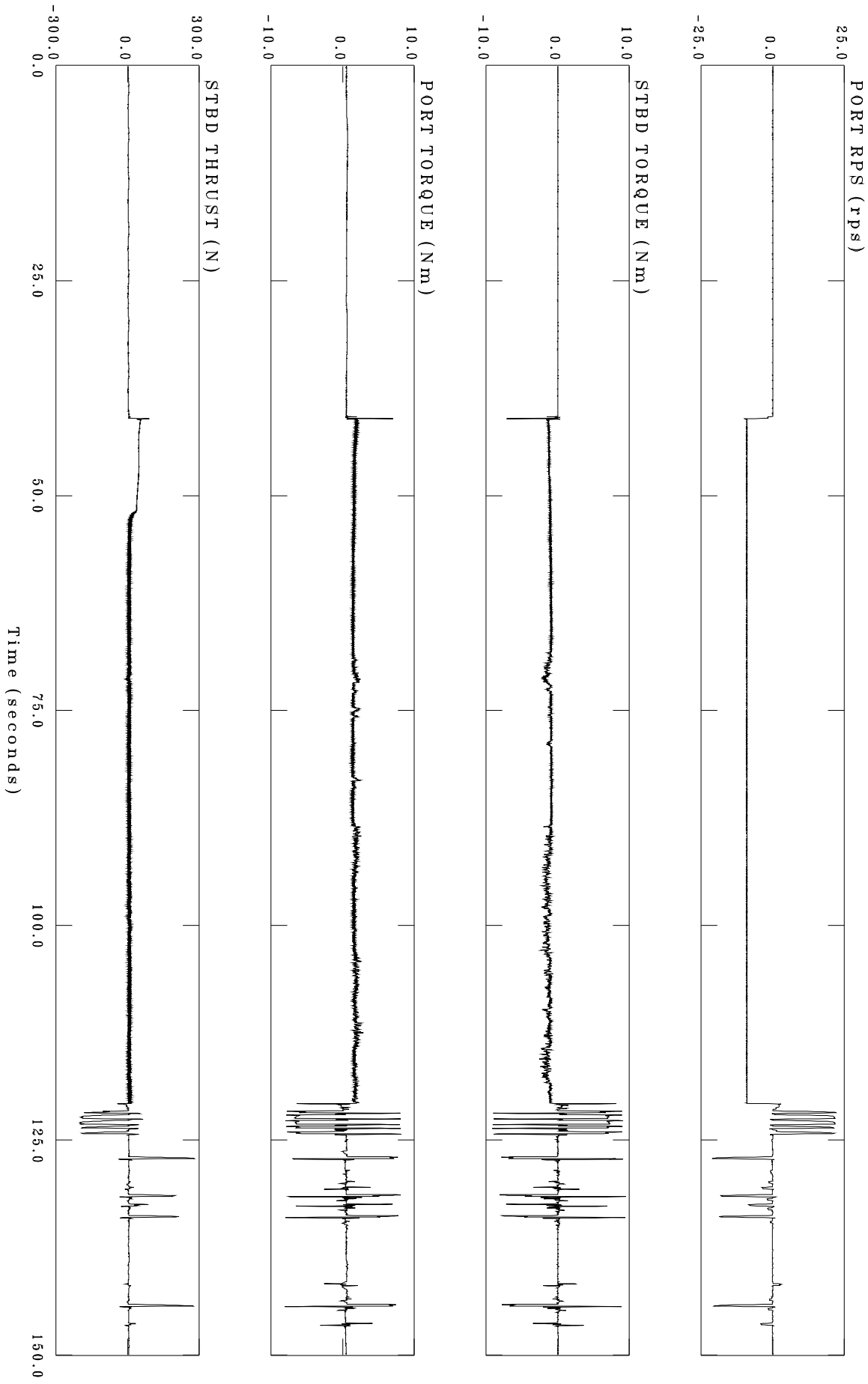
Descriptifn	Unit	Min	Max	Mean	S_D_b	Chan
Videf Sync	vflts	0.38837	0.10311	0.37425	0.0020512	1
Carriage Tach Velfcity	m/s	0.11914	0.95598	0.54349	0.13109	2
Pudder Angle	deg	24.518	30.319	24.929	0.015119	3
* OPT T_PUST	N	22.180	12.542	33.913	2.9919	1
STBD T_PUST	N	-5.195	17.541	7.320	5.1777	5
* OPT TOPQUE	Nm	1.5934	2.4043	1.5223	0.21548	8
STBD TOPQUE	Nm	-2.5003	-0.83229	-1.5838	0.24880	7
* OPT P_S	rFs	-4.5743	-9.4500	-4.0555	0.023120	9
STBD P_S	rFs	9.5997	4.3094	9.5410	0.011137	4
Fitch	deg	-0.21801	0.2510	0.015118	0.074708	10
Pfll	deg	-2.1217	2.5171	0.17451	0.77241	11

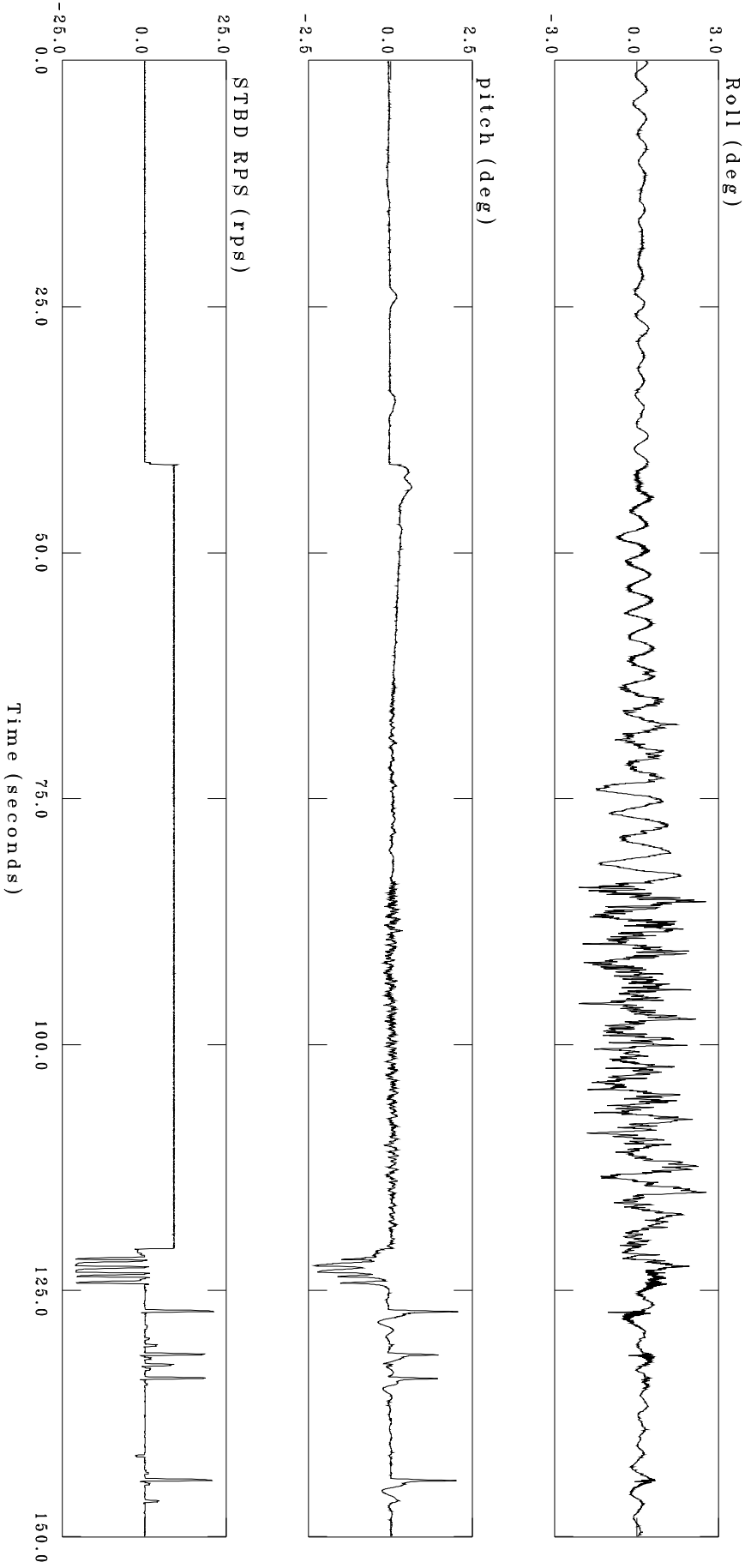
----- After Taring -----

Analysis Date/Time = 17-DEC-2005 13:31:38
 Acquired Date/Time = 23-NOV-2001 15:34:11
 InPut Hile = C_S2_TAPED
 OutPut Hile = HP2_S1_4P_S_007_DAT
 NumOer f6 Samples = 1382
 Segment Start Time = 42.390 secnds
 Segment End Time = 114.80 secnds

Descriptifn	Unit	Min	Max	Mean	S_D_b	Chan
Videf Sync	vflts	-0.012571	0.021201	0.00031028	0.0020512	1
Carriage Tach Velfcity	m/s	0.11814	0.95118	0.54229	0.13109	2
Pudder Angle	deg	30.084	30.971	30.391	0.015119	3
* OPT T_PUST	N	17.031	37.583	29.711	2.9919	1
STBD T_PUST	N	-9.8222	11.197	1.5292	5.1777	5
* OPT TOPQUE	Nm	0.12819	2.4514	1.1814	0.21548	8
STBD TOPQUE	Nm	-2.5192	-0.85020	-1.5918	0.24880	7
* OPT P_S	rFs	-4.1811	-9.4321	-4.0378	0.023120	9
STBD P_S	rFs	9.8405	4.2107	9.5459	0.011137	4
Fitch	deg	-0.21454	0.21152	0.011989	0.074708	10
Pfll	deg	-2.2998	2.3902	0.12570	0.77241	11







----- Tare Segment -----

Analysis Date/Time = 17-DEC-2005 13:30:52
 AcquireN Date/Time = 27-OV4-2001 15:20:IP
 Fhdt File = CR_S1
 VdtHdt File = P_I S2_12' bS_P011 DAT
 Qgmfer 68 Samples = 1c03_P
 Segment Start Time = 1_P000 segnNs
 Segment EnN Time = 35_C10 segnNs

Descripti6n	Mnit	xin	xah	xean	S D o CVan
4iNe6 Syng	96lts	-0.012PIF	0.013PFC	-0.000II251	0.0017U32 1
Carriage TaqV 4el6 qity	m/s	-0.005273	0.012033	0.002PP3P	0.001233P 2
*qNner Angle	Neg	-0.370U3	0.10P55	-0.000U2I30	0.012I03 3
bV T TR MST	O	-0.23173	11.7U2	7.132I	3.30cc I
STBD TR MST	O	1.331U	U.0c05	c.032I	0.0c0U1 5
bV T TV QME	Om	0.0cU30	0.71c0I	0.5P3C7	0.0175I2 c
STBD TV QME	Om	-0.05PPI7	0.0cP0I3	0.01cc0c	0.02010I 7
bV T *bS	rHS	-0.00U170	0.05230I	-0.02002U	0.00U0CP p
STBD *bS	rHS	-0.0c70I3	0.2c5U5	0.102Pc	0.01UUI7 U
HitqV	Neg	-0.05cU2U	0.05IC53	0.001ICUp	0.00PI035 10
*611	Neg	0.011Pc	0.0c7U7	0.03IU52	0.02cP2I 11

----- Be86re Taring -----

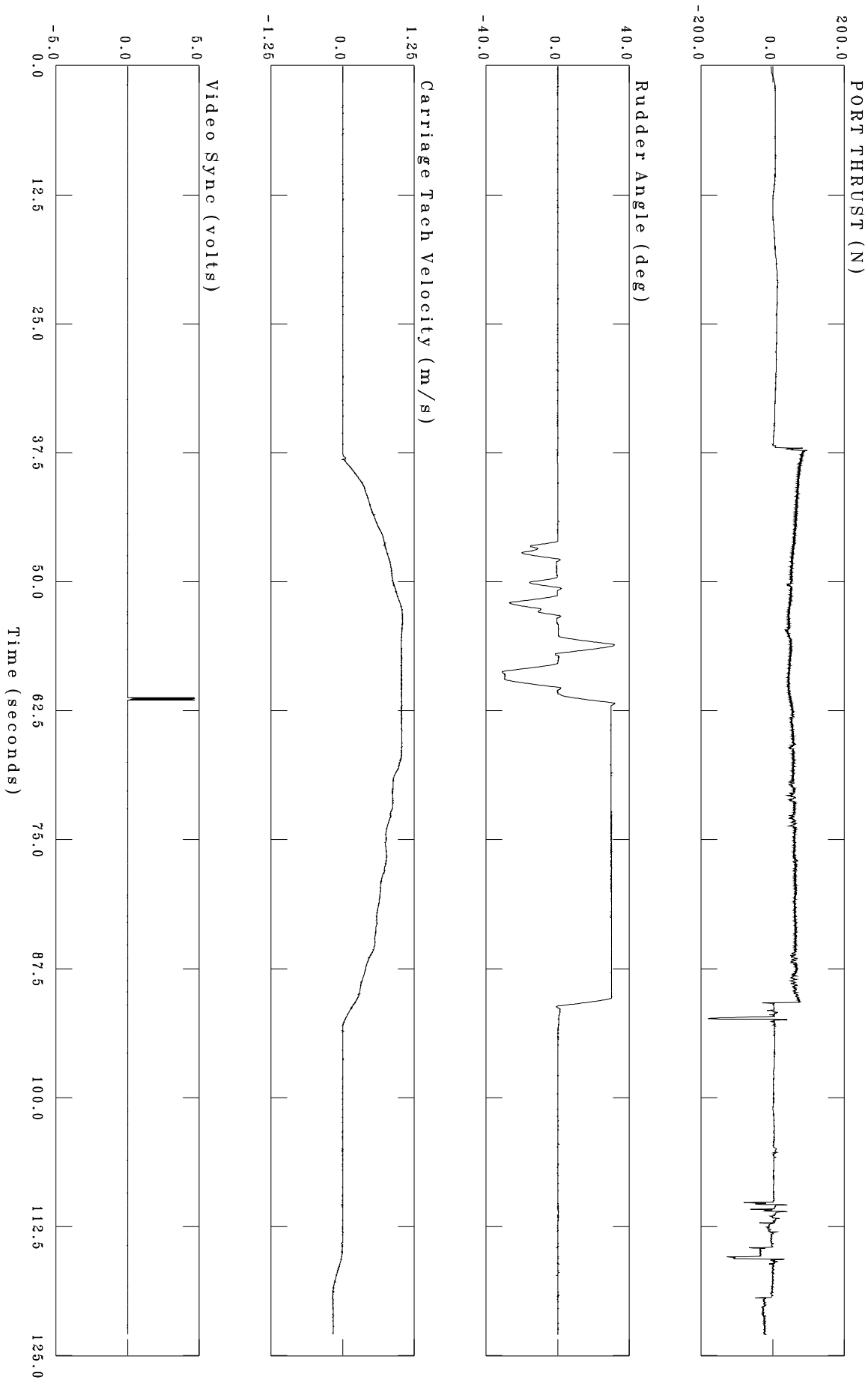
Analysis Date/Time = 17-DEC-2005 13:30:55
 AcquireN Date/Time = 27-OV4-2001 15:20:IP
 Fhdt File = CR_S2
 VdtHdt File = P_I S2_12' bS_P011 DAT
 Qgmfer 68 Samples = 13BU_P
 Segment Start Time = C3_200 segnNs
 Segment EnN Time = PU_3C0 segnNs

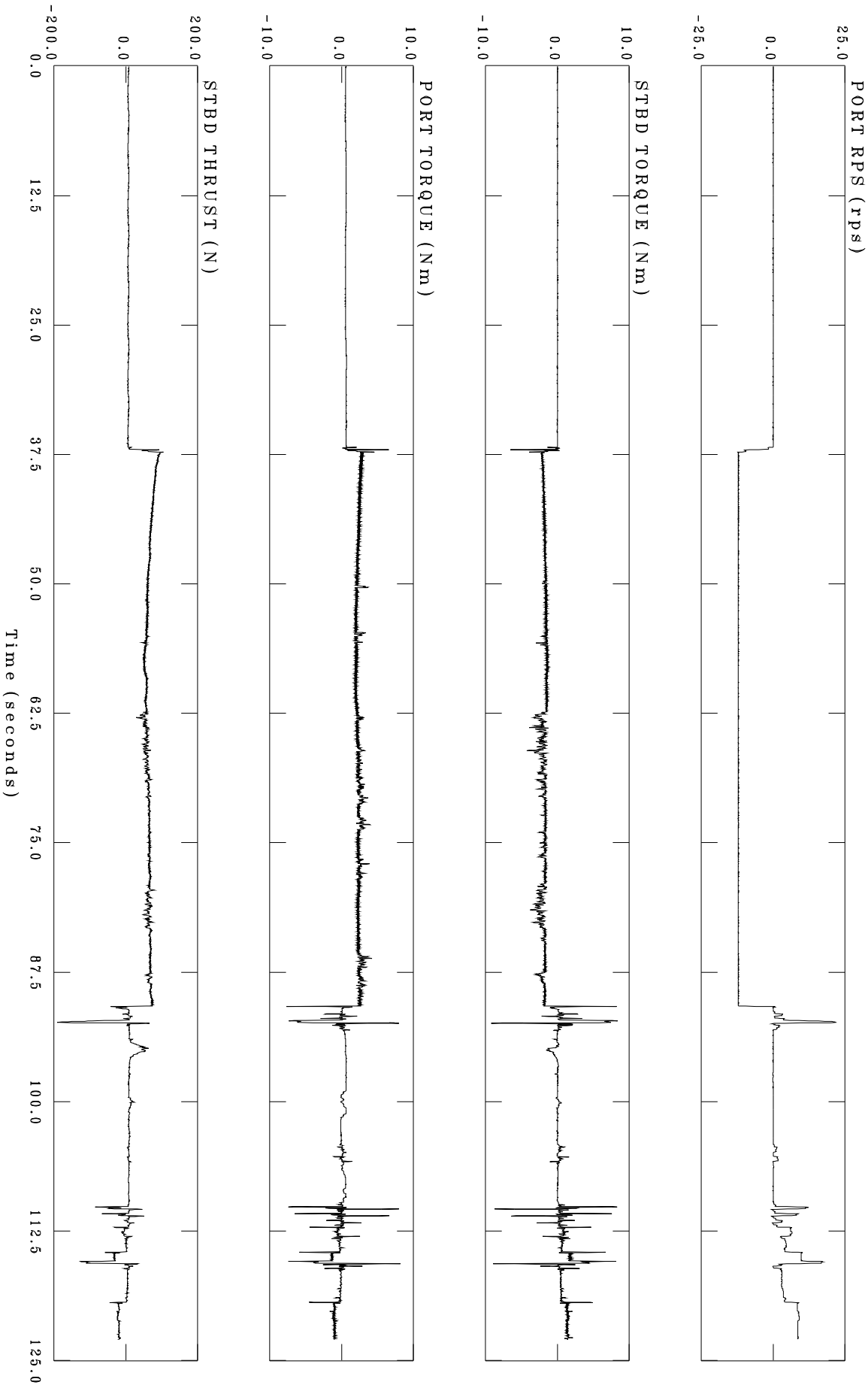
Descripti6n	Mnit	xin	xah	xean	S D o CVan
4iNe6 Syng	96lts	-0.0170U0	0.0225P3	-0.00032P2I	0.001PU23 1
Carriage TaqV 4el6 qity	m/s	0.310I0	1.035I	0.73UI2	0.200I3 2
*qNner Angle	Neg	2U.12P	30.37c	2U.pPI	0.07P3II 3
bV T TR MST	O	11.0PI	70.0PI	5U.c32	1.1030 I
STBD TR MST	O	17.007	7P.cC2	C3.c5c	1.0PPI0 5
bV T TV QME	Om	1.015U	1.23P0	2.032U	0.02203 c
STBD TV QME	Om	-1.055c	-1.0225c	-1.03c7	0.03U1Up 7
bV T *bS	rHS	-12.230	-11.0U7I	-12.0Up	0.023c3P p
STBD *bS	rHS	11.7U5	12.00P	11.0Pc	0.01IC02 U
HitqV	Neg	-0.0273P	0.57313	0.103C2	0.045I72 10
*611	Neg	-1.0cUp	3.0U72	-0.0UI3U	1.02c21 11

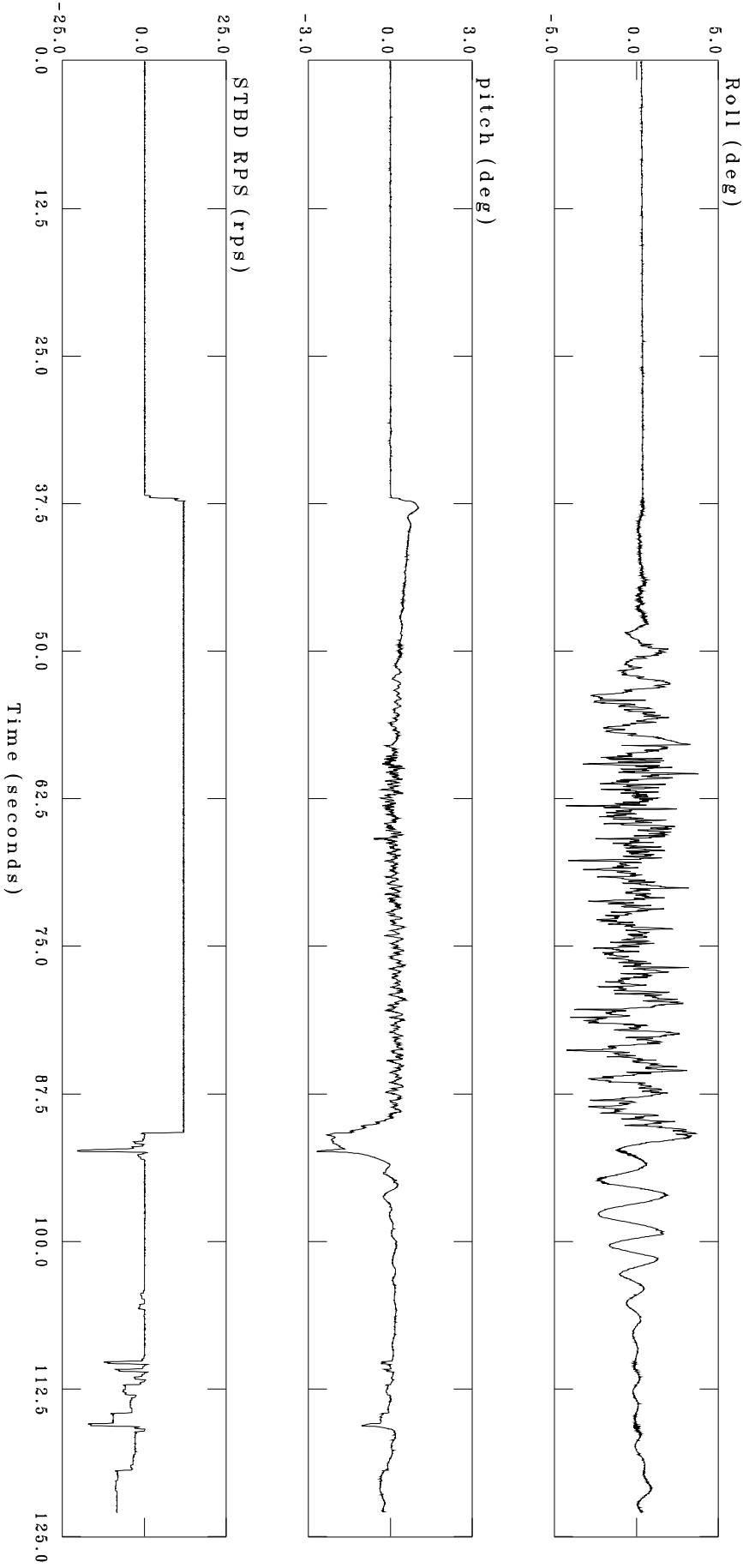
----- A8ter Taring -----

Analysis Date/Time = 17-DEC-2005 13:30:5U
 AcquireN Date/Time = 27-OV4-2001 15:20:IP
 Fhdt File = CR_S2_TA' ED
 VdtHdt File = P_I S2_12' bS_P011 DAT
 Qgmfer 68 Samples = 13BU_P
 Segment Start Time = C3_200 segnNs
 Segment EnN Time = PU_3C0 segnNs

Descripti6n	Mnit	xin	xah	xean	S D o CVan
4iNe6 Syng	96lts	-0.01ccPI	0.02302c	0.00011I2P	0.001PU23 1
Carriage TaqV 4el6 qity	m/s	0.30751	1.0325	0.73c53	0.200I3 2
*qNner Angle	Neg	2U.13P	30.3Pc	2U.pU3	0.07P3II 3
bV T TR MST	O	33.c51	C2.c52	52.c00	1.1030 I
STBD TR MST	O	10.173	71.0P2P	5c.022	1.0PPI0 5
bV T TV QME	Om	1.0c22	3.05II	1.0U2	0.02203 c
STBD TV QME	Om	-1.0712	-1.0122	-1.0533	0.03U1Up 7
bV T *bS	rHS	-12.210	-11.05I	-12.07P	0.023c3P p
STBD *bS	rHS	11.0U2	12.205	11.0P3	0.01IC02 U
HitqV	Neg	-0.02P5	0.571cc	0.1P215	0.045I72 10
*611	Neg	-1.01U3	2.0PI77	-0.0I3U1	1.02c21 11







----- Tare Segment -----

Analysis Date/Time = 17-DEC-2005 13:20:22
 AcquireN Date/Time = 20-V4I-2001 13:03:P5
 Fhdt File = CR_S1
 4dHdt File = P_1_S3_12* bS_01P.DAT
 Vgmfer 68 Samples = 170_P
 Segment Start Time = 2.200 segnNs
 Segment EnN Time = 30_P20 segnNs

Descripti6n	Mnit	xin	xah	xean	S D o CVan	
IiNe6 Syng	96lts	-0.00P2725	0.00P1200	-0.0002C50C	0.000C1003	1
Carriage TaqV Iel6 qity	m/s	-0.0035050	0.0032022	0.000177Up	0.00070PU0	2
*dNner Angle	Neg	0.021C25	0.037C2	0.032P2C	0.025375	3
b4* T TR MST	V	2.7521	3.5373	3.12P7	0.07C7P3	P
STBD TR MST	V	0.52P0	10.0C15	0.0C0C	0.0C03Pc	5
b4* T T4* QME	Vm	0.0225PP	0.02537U	0.02P03C	0.00203P1	U
STBD T4* QME	Vm	0.021707	0.02P031	0.0233Uc	0.002C020	7
b4* T *bS	rHS	-0.017032	0.07C0P0	0.0005231	0.0120UU	C
STBD *bS	rHS	-0.01030P	-0.027PPP	-0.00CC10	0.01027P	0
HitqV	Neg	-0.00P3037	0.010U00	-0.0077350	0.011Uc1	10
*611	Neg	-0.0002C02C	0.00PPU2	0.02C031	0.01PUUc	11

----- Be86re Taring -----

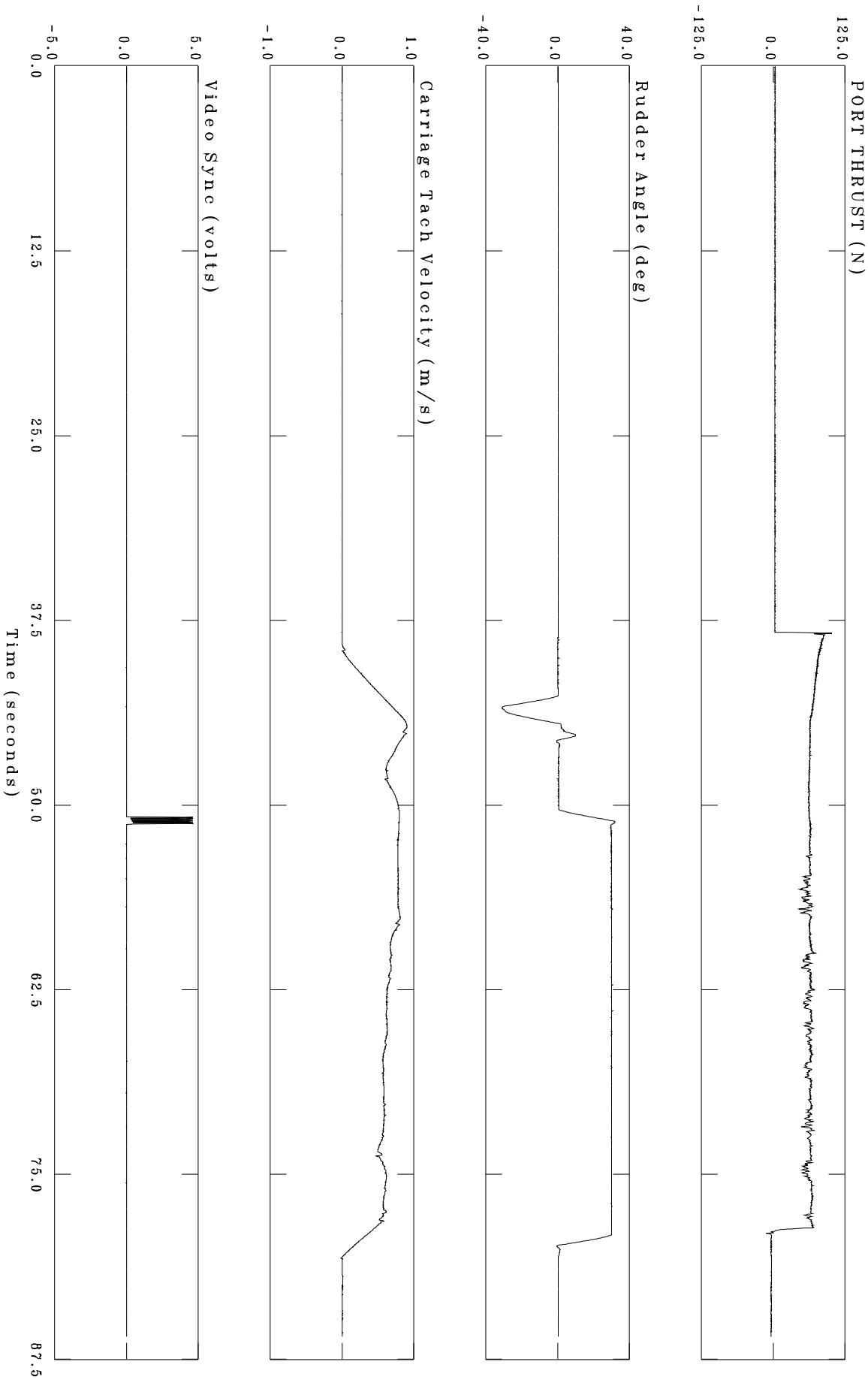
Analysis Date/Time = 17-DEC-2005 13:20:2P
 AcquireN Date/Time = 20-V4I-2001 13:03:P5
 Fhdt File = CR_S2
 4dHdt File = P_1_S3_12* bS_01P.DAT
 Vgmfer 68 Samples = 12P1_P
 Segment Start Time = 52.07C0 segnNs
 Segment EnN Time = 77.0C0 segnNs

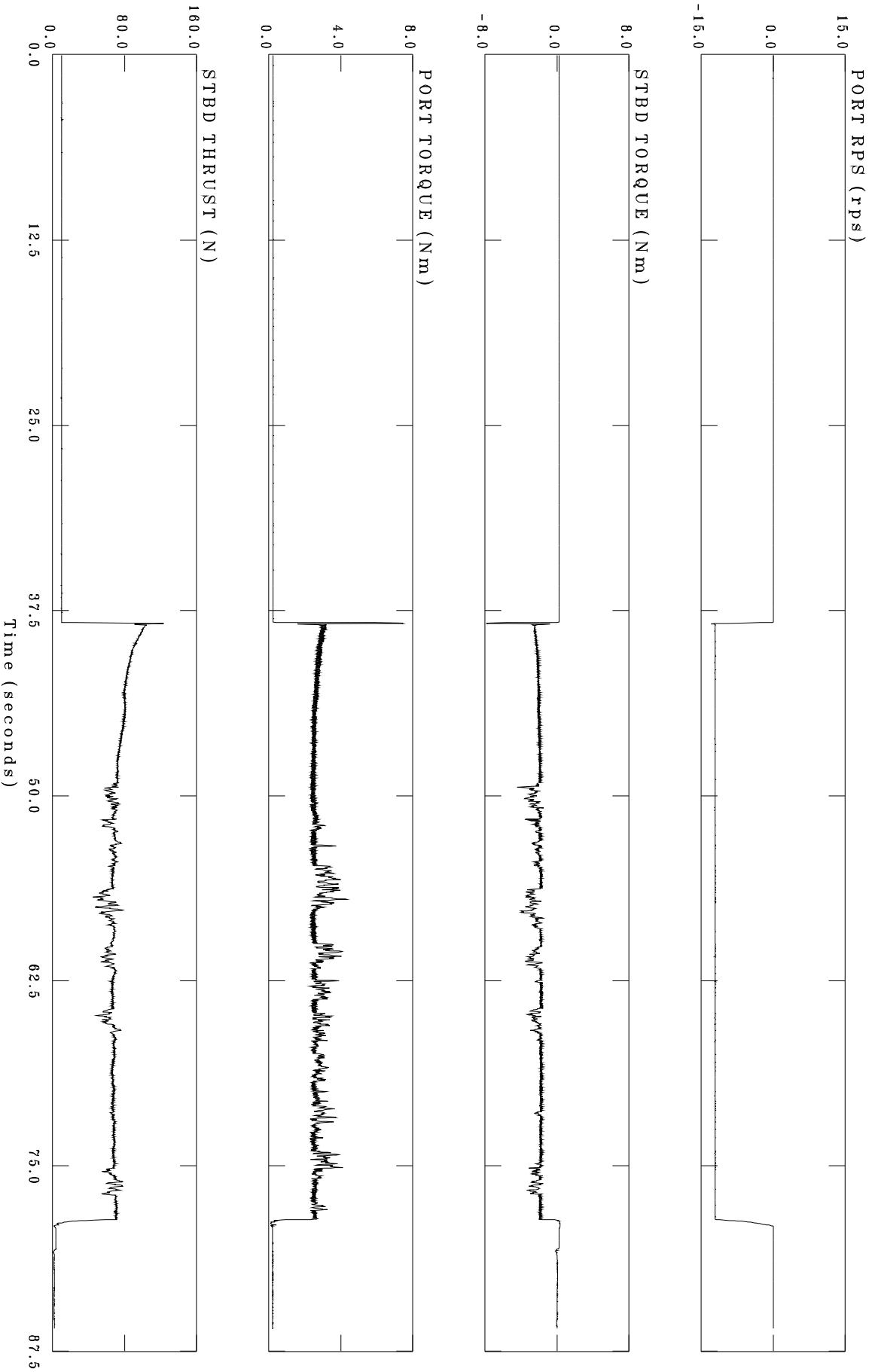
Descripti6n	Mnit	xin	xah	xean	S D o CVan	
IiNe6 Syng	96lts	-0.0155Up	0.02P720	-0.07210E-05	0.0020327	1
Carriage TaqV Iel6 qity	m/s	0.0P7733	0.0C13C0	0.0UpU2U	0.0C3C73	2
*dNner Angle	Neg	20.0U50	30.057P	30.01P	0.0Up201	3
b4* T TR MST	V	PP.0U00	73.0PP	U0.0723	P.02120	P
STBD TR MST	V	P0.010	7C.031	UU.0351	P.01507	5
b4* T T4* QME	Vm	2.05U0	P.0PP1	2.0700	0.0U317	U
STBD T4* QME	Vm	-P.0127	-1.05373	-2.0511	0.0Pc37	7
b4* T *bS	rHS	-12.02P1	-11.0C1	-12.003	0.02P03U	C
STBD *bS	rHS	11.07C0	12.010	11.0CP	0.0P21CP	0
HitqV	Neg	-0.00U53	0.00P7C0	0.02P752	0.0155C2	10
*611	Neg	-3.0U01	2.0C00	-0.00P71	1.010U2	11

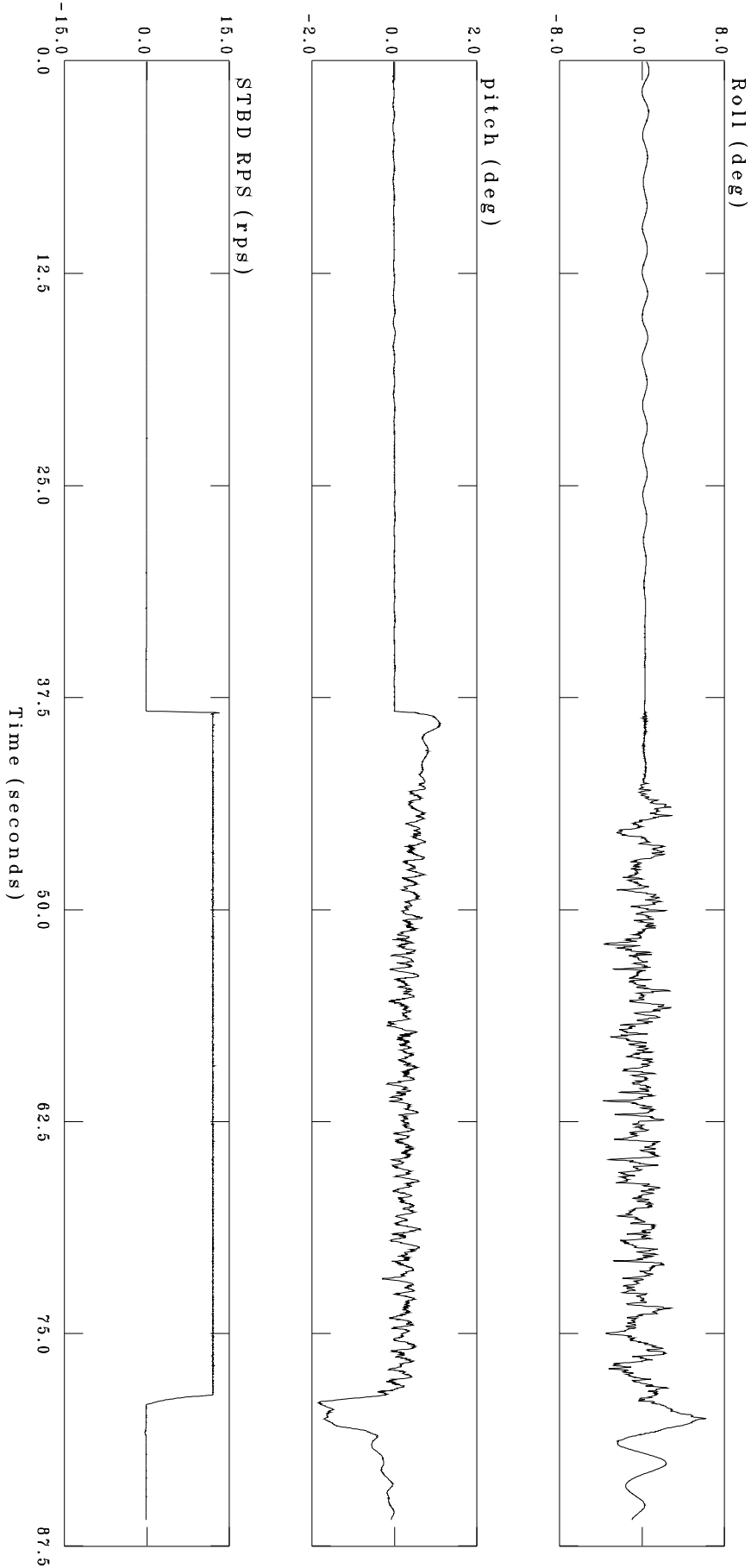
----- A8ter Taring -----

Analysis Date/Time = 17-DEC-2005 13:20:2C
 AcquireN Date/Time = 20-V4I-2001 13:03:P5
 Fhdt File = CR_S2_TA* ED
 4dHdt File = P_1_S3_12* bS_01P.DAT
 Vgmfer 68 Samples = 12P1_P
 Segment Start Time = 52.07C0 segnNs
 Segment EnN Time = 77.0C0 segnNs

Descripti6n	Mnit	xin	xah	xean	S D o CVan	
IiNe6 Syng	96lts	-0.015270	0.025005	0.0002773U	0.0020327	1
Carriage TaqV Iel6 qity	m/s	0.0P7715	0.0C1371	0.0UpU0C	0.0C3C73	2
*dNner Angle	Neg	20.0335	30.0250	20.0U00	0.0Up201	3
b4* T TR MST	V	P1.0P5	70.0510	50.05C	P.02120	P
STBD TR MST	V	35.020	Uc.050	5U.0370	P.01507	5
b4* T T4* QME	Vm	2.01UU	P.0037	2.020U	0.0U317	U
STBD T4* QME	Vm	-P.0PP0	-1.0710	-2.0CPc	0.0Pc37	7
b4* T *bS	rHS	-12.0250	-11.0001	-12.0102	0.02P03U	C
STBD *bS	rHS	11.07C	12.000	12.0073	0.0P21CP	0
HitqV	Neg	-0.00C70	0.003553	0.02552U	0.0155C2	10
*611	Neg	-P.0PP0	2.050PU	-0.0P0102	1.010U2	11







----- Tare Segment -----

Analysis Date/Time = 17-DEC-2005 13:32:52
 Acquired Date/Time = 2N-OV4-2001 13:50:53
 Input File = CH_S1
 Vutput File = FR_R2_S3_12RPS_015.DAT
 Oumber of Samples = 1571
 Segment Start Time = 3.6800 seconds
 Segment End Time = 35.080 seconds

Description	Unit	Min	Max	Mean	S.D.	Chan
4ideo Sync	volts	-0.0115N7	0.013733	0.0013622	0.0017637	1
Carriage Tach 4elocity	m/s	-0.0068510	0.012680	0.0021N9N	0.0019219	2
Rudder Angle	deg	0.038N38	0.65790	0.31226	0.0989N6	3
PVRT THRUST	O	-0.257N0	9.3356	1.5797	0.677N0	9
STBD THRUST	O	3.9N26	N.1035	6.8956	0. N2506	5
PVRT TVRQUE	Om	-0.15810	0.153N2	0.0020897	0.07006N	6
STBD TVRQUE	Om	-0.10032	0.018NN7	-0.031193	0.019593	7
PVRT RPS	rps	0.032N2N	0.1830N	0.10098	0.010571	8
STBD RPS	rps	-0.17199	0.16875	-0.00N3651	0.023371	N
pitch	deg	-0.080231	0.22225	0.0013892	0.063593	10
Roll	deg	-1.1N89	1.6815	0.33913	0.73991	11

----- Before Taring -----

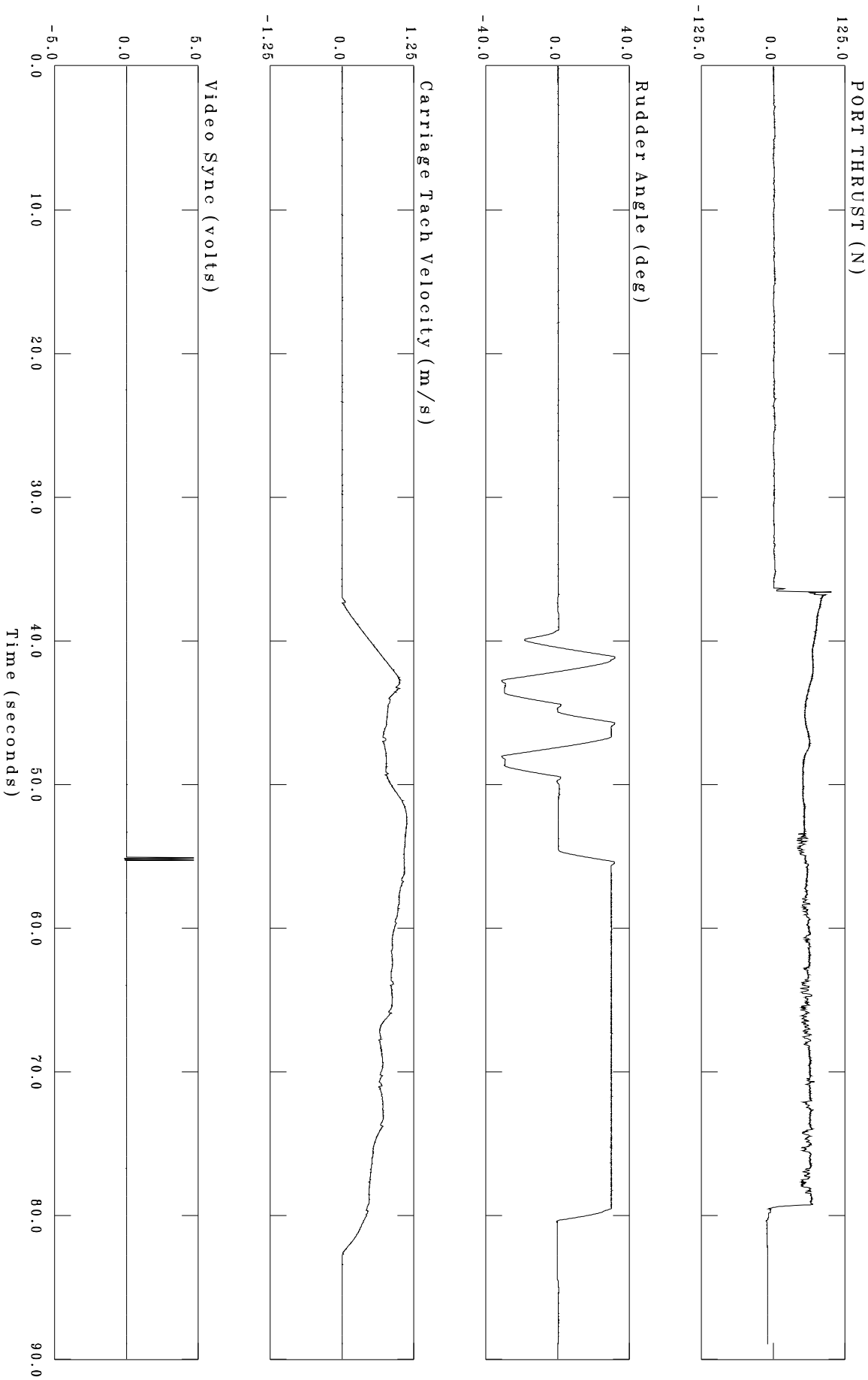
Analysis Date/Time = 17-DEC-2005 13:32:55
 Acquired Date/Time = 2N-OV4-2001 13:50:53
 Input File = CH_S2
 Vutput File = FR_R2_S3_12RPS_015.DAT
 Oumber of Samples = 1106
 Segment Start Time = 56.060 seconds
 Segment End Time = 78.160 seconds

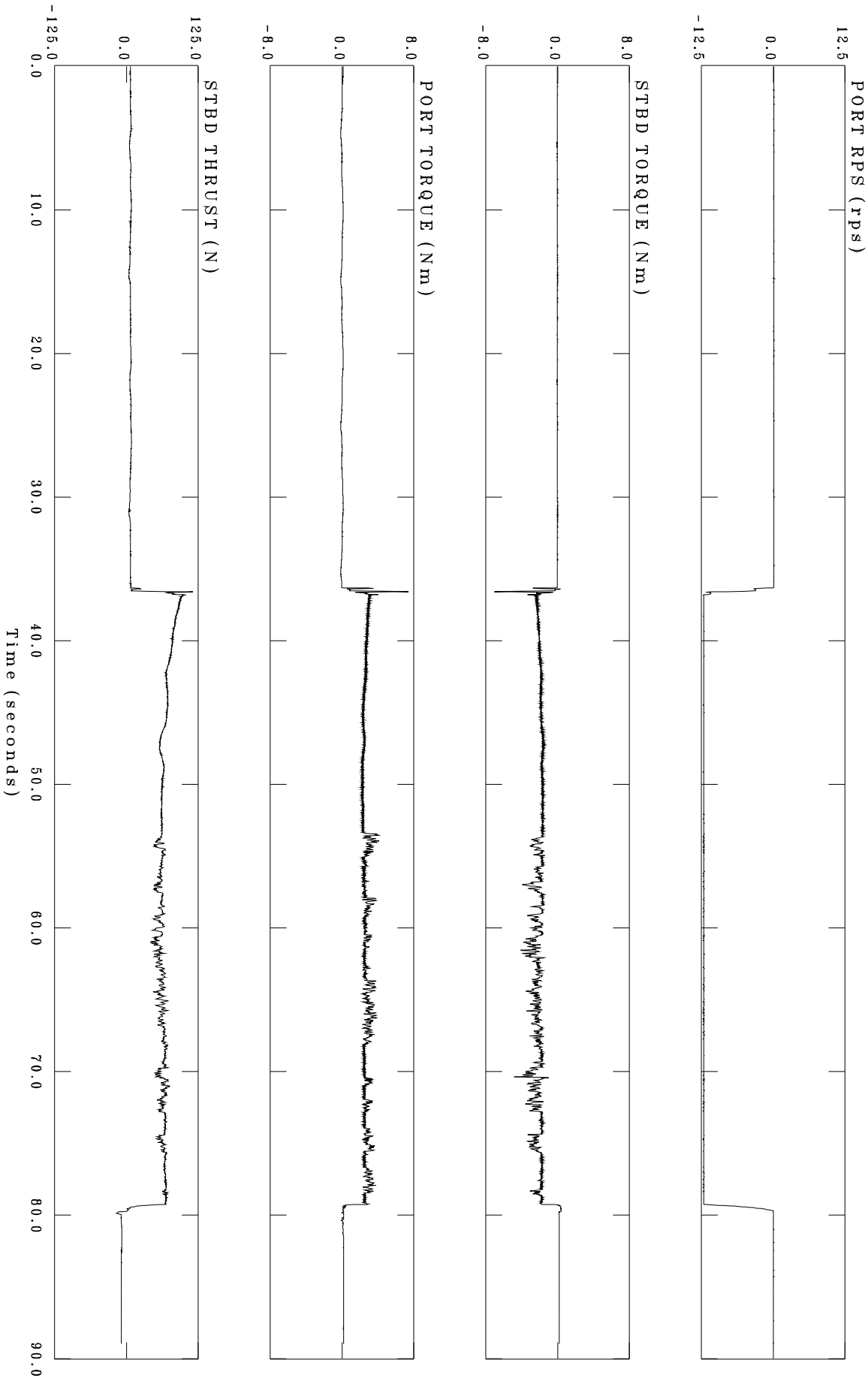
Description	Unit	Min	Max	Mean	S.D.	Chan
4ideo Sync	volts	-0.013886	0.021210	0.0019930	0.0017837	1
Carriage Tach 4elocity	m/s	0.97053	1.0872	0.7697N	0.15N53	2
Rudder Angle	deg	2N.571	30.931	2N.N01	0.096036	3
PVRT THRUST	O	96. N60	71.3N3	60.038	9.2860	9
STBD THRUST	O	91.872	79.8NN	62.020	5.5231	5
PVRT TVRQUE	Om	2.239N	3.8579	2.7221	0.33955	6
STBD TVRQUE	Om	-9.8781	-1.0213	-2.2230	0.503N8	7
PVRT RPS	rps	-12.296	-11. N87	-12.100	0.025329	8
STBD RPS	rps	11.777	12.362	11. NN7	0.051N80	N
pitch	deg	-0.26986	0.69617	0.1N879	0.16300	10
Roll	deg	-9.32N8	2.6N87	-0.15506	1.078N	11

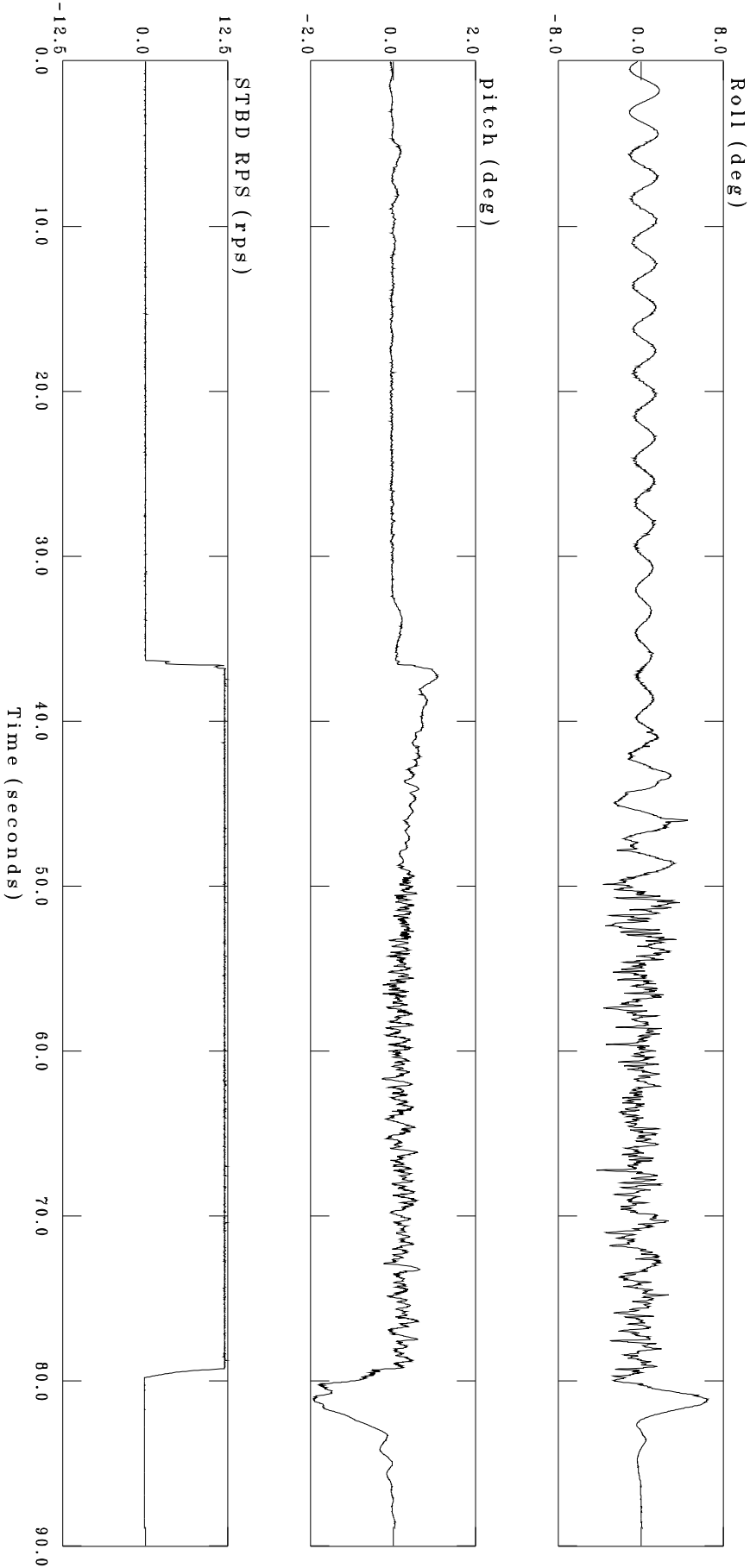
----- After Taring -----

Analysis Date/Time = 17-DEC-2005 13:32:58
 Acquired Date/Time = 2N-OV4-2001 13:50:53
 Input File = CH_S2_TARED
 Vutput File = FR_R2_S3_12RPS_015.DAT
 Oumber of Samples = 1106
 Segment Start Time = 56.060 seconds
 Segment End Time = 78.160 seconds

Description	Unit	Min	Max	Mean	S.D.	Chan
4ideo Sync	volts	-0.015298	0.01N898	0.000080897	0.0017837	1
Carriage Tach 4elocity	m/s	0.96833	1.0850	0.7625N	0.15N53	2
Rudder Angle	deg	2N.25N	30.11N	2N.588	0.096036	3
PVRT THRUST	O	95.385	6N.818	58.969	9.2860	9
STBD THRUST	O	35.026	68.053	55.175	5.5231	5
PVRT TVRQUE	Om	2.2328	3.8553	2.7200	0.33955	6
STBD TVRQUE	Om	-9.896N	-0. NN021	-2.1N1N	0.503N8	7
PVRT RPS	rps	-12.397	-12.088	-12.201	0.025329	8
STBD RPS	rps	11.786	12.371	12.006	0.051N80	N
pitch	deg	-0.26629	0.69978	0.1N736	0.16300	10
Roll	deg	-9.6690	2.35N6	-0.98N18	1.078N	11







----- Tare Segment -----

Analysis Date/Time = 17-DEC-2005 13:35:00
 AcquireN Date/Time = 20-V4I-2001 10:50:10
 PnFdt Hile = C_S1
 4dFdt Hile = HP3_S3_12P_S_01b.DAT
 Vgmfer 68 Samples = 1083 R_R
 Segment Start Time = 0.500 segnNs
 Segment EnN Time = 30.000 segnNs

Descripti6n	Mnit	xin	xah	xean	S D o CVan
IiNe6 Syng	96lts	-0.00001U3	0.017700	0.0030171	0.0010000 1
Carriage TaqV Iel6 qity	m/s	-0.0087c31	0.01cc07	0.0020c5U	0.001ccc5 2
PdNner Angle	Neg	-0.30557	0.7b352	0.15005	0.2b25c 3
*4PT T-PMST	V	-1.0c31	3.0252	1.2300	0.300Ob c
STBD T-PMST	V	2.000c	7.03102	5.5370	0.721U2 5
*4PT T4PQME	Vm	-0.0513U	0.1c0b0	-0.0112c0	0.072133 b
STBD T4PQME	Vm	-0.000c1c	0.020c12	-0.0275c2	0.013700 7
*4PT P S	rFs	0.001cc30	0.173c0	0.005cU5	0.0122b2 U
STBD P S	rFs	-0.000cc	0.1bU75	0.0010533	0.0235cU 0
FitdV	Neg	-0.027U30	0.03300	-0.00b21c2	0.030c53 10
P6 ll	Neg	-1.0b17c	1.02700	-0.030352	0.13bU7 11

----- Be86re Taring -----

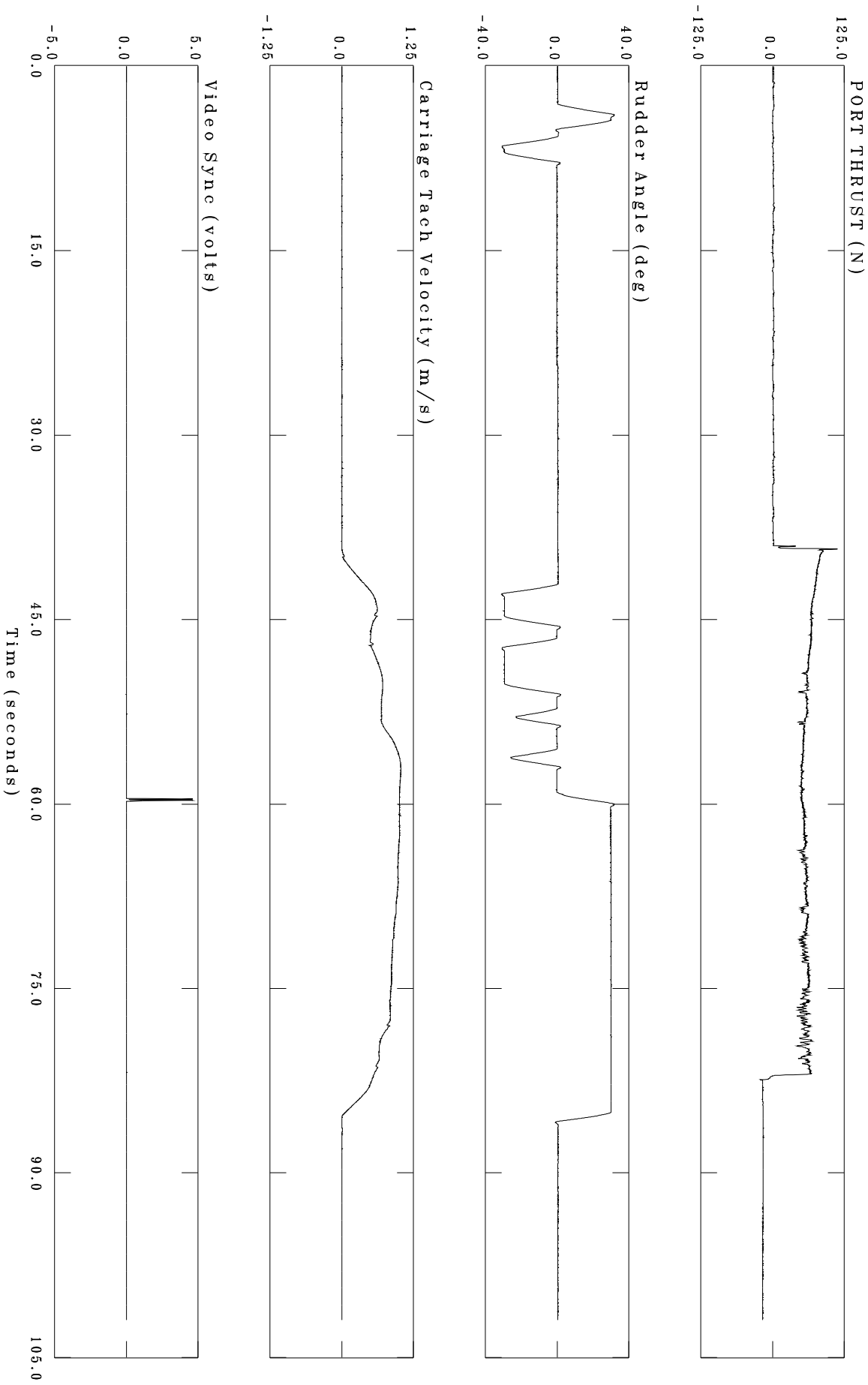
Analysis Date/Time = 17-DEC-2005 13:35:02
 AcquireN Date/Time = 20-V4I-2001 10:50:10
 PnFdt Hile = C_S2
 4dFdt Hile = HP3_S3_12P_S_01b.DAT
 Vgmfer 68 Samples = 1087 R_R
 Segment Start Time = 0.500 segnNs
 Segment EnN Time = 01.000 segnNs

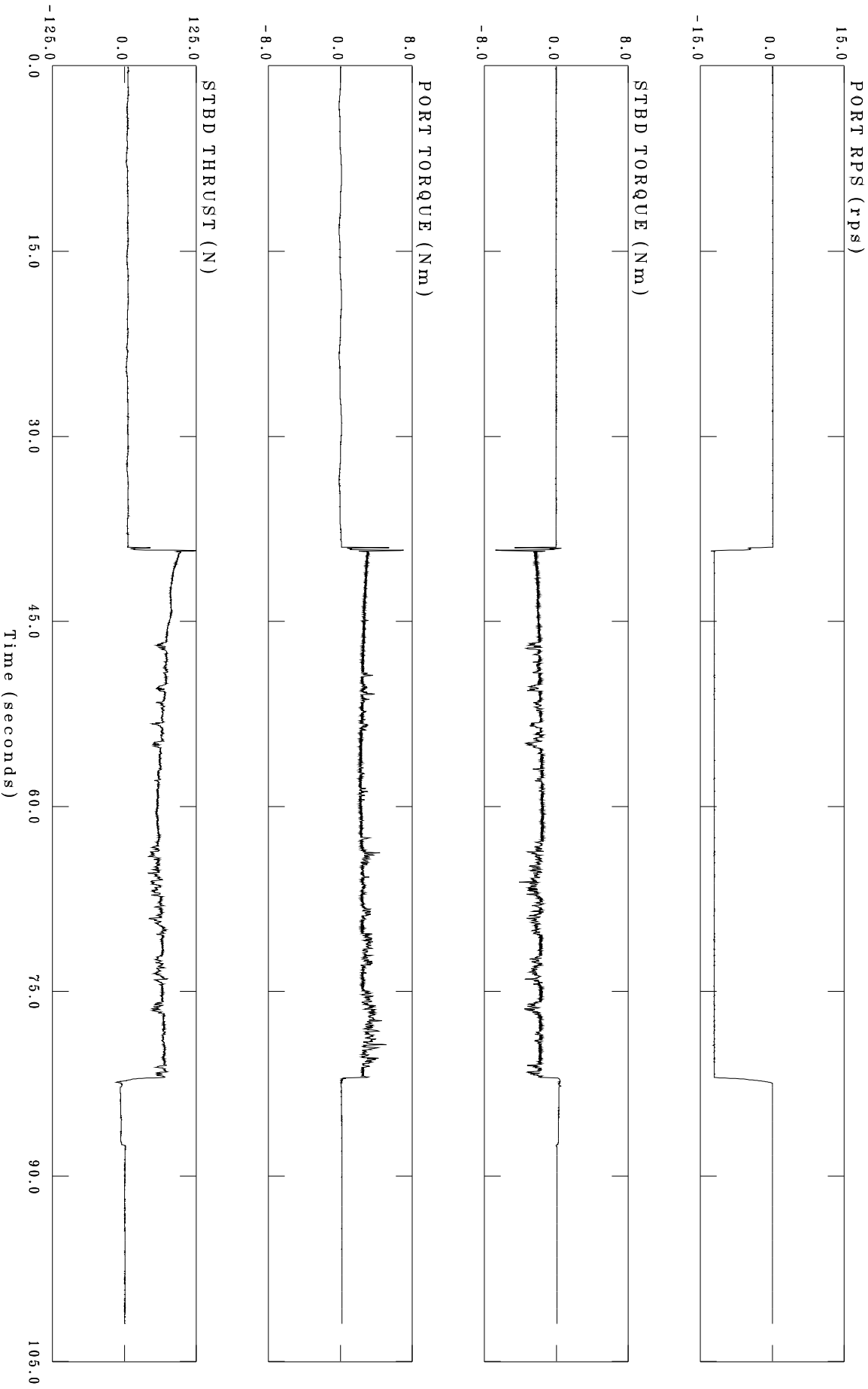
Descripti6n	Mnit	xin	xah	xean	S D o CVan
IiNe6 Syng	96lts	-0.000b07b	0.010bUc	0.00c1Ucc	0.001570b 1
Carriage TaqV Iel6 qity	m/s	0.02cUc	1.023U	0.00003	0.10370 2
PdNner Angle	Neg	20.5c2	30.303	30.003	0.0730UU 3
*4PT T-PMST	V	c2.5c0	b0.57c	57.202	c.30cc c
STBD T-PMST	V	c1.027c	7c.077b	b1.710	b.0073 5
*4PT T4PQME	Vm	2.0bU6	5.0723	2.0722	0.0cc07 b
STBD T4PQME	Vm	-c.035U	-1.0U12	-2.0211	0.030703 7
*4PT P S	rFs	-12.02U1	-11.00bc	-12.010U	0.0272b3 U
STBD P S	rFs	11.07U6	12.0320	12.011	0.0502Ob 0
FitdV	Neg	-0.05020	0.55b55	0.155cb	0.15052 10
P6 ll	Neg	-c.0b21	c.0375c	-0.0c303	1.02210 11

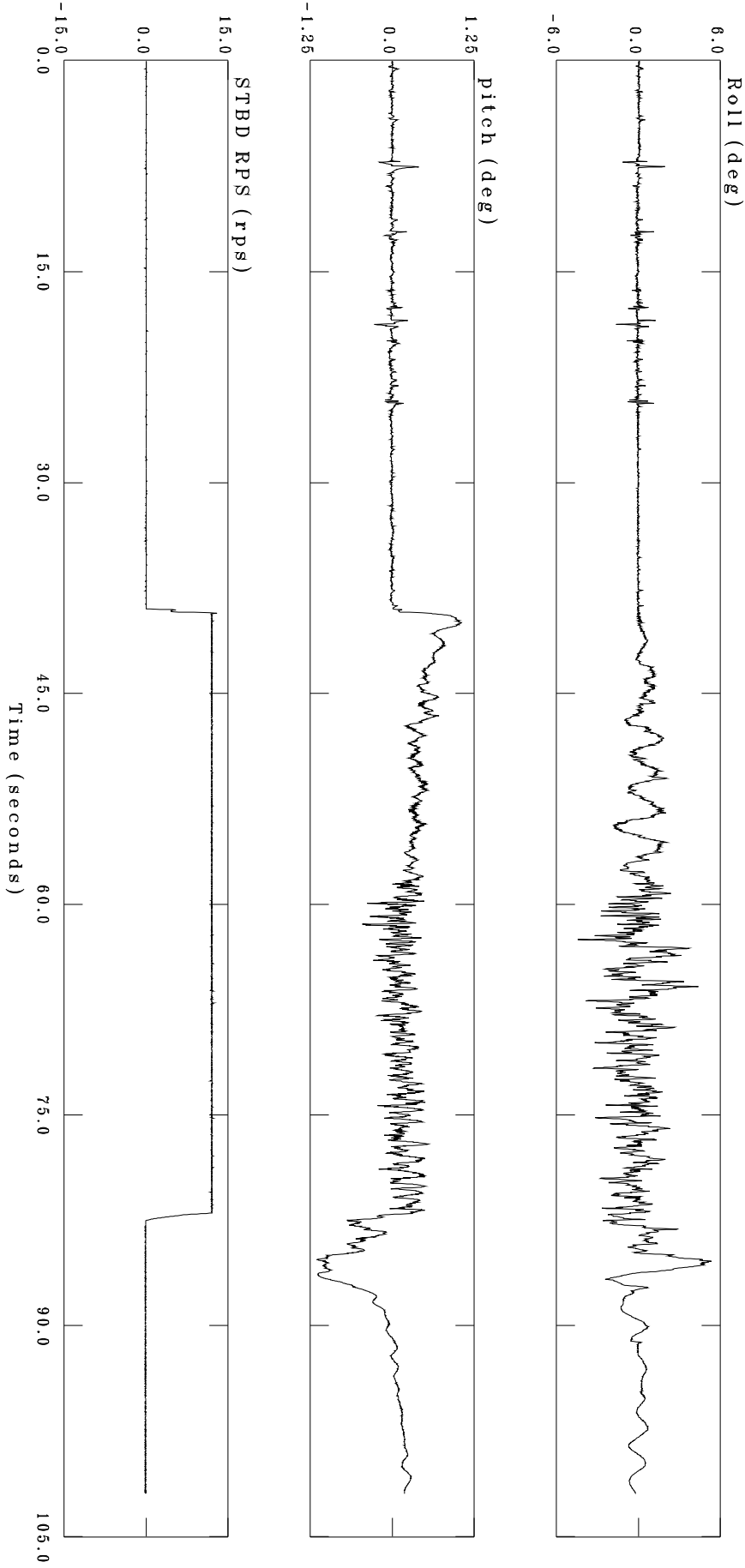
----- A8ter Taring -----

Analysis Date/Time = 17-DEC-2005 13:35:0b
 AcquireN Date/Time = 20-V4I-2001 10:50:10
 PnFdt Hile = C_S2.TAPED
 4dFdt Hile = HP3_S3_12P_S_01b.DAT
 Vgmfer 68 Samples = 1087 R_R
 Segment Start Time = 0.500 segnNs
 Segment EnN Time = 01.000 segnNs

Descripti6n	Mnit	xin	xah	xean	S D o CVan
IiNe6 Syng	96lts	-0.012b15	0.0157b7	0.0002b737	0.001570b 1
Carriage TaqV Iel6 qity	m/s	0.021U0	1.020U	0.00000	0.10370 2
PdNner Angle	Neg	20.3Uc	30.1c5	20.0c5	0.0730UU 3
*4PT T-PMST	V	c1.0310	b0.3cc	5b.0b2	c.30cc c
STBD T-PMST	V	35.03b	b0.03U	5b.173	b.0073 5
*4PT T4PQME	Vm	2.0700	5.003b	2.0703c	0.0cc07 b
STBD T4PQME	Vm	-c.00U2	-1.053b	-1.003b	0.030703 7
*4PT P S	rFs	-12.37b	-12.0b0	-12.20c	0.0272b3 U
STBD P S	rFs	11.7U5	12.032U	12.010	0.0502Ob 0
FitdV	Neg	-0.0c000	0.5b27b	0.1b1b7	0.15052 10
P6 ll	Neg	-c.02c7	c.01cU	-0.003bU	1.02210 11







Appendix B
Ice sheet summary

NRC - INSTITUTE FOR MARINE DYNAMICS

ARCTIC VESSEL RESEARCH SECTION

ICE MECHANICAL PROPERTIES SUMMARY

Test Name: HEALY16

Project Number: 919

Warm up commenced: 03:25 23-NOV-2001

Time	Warm-up hrs	Loc	hi mm	Sf kPa	Lc cm	E MPa	E/Sf	Lc/hi	K1c N/m	Sf/K1c m-.5	Sc/s kPa	Rhoi Mg/m3
0850	5.41	N	30.8 ± 1.6 n= 3									
		S	29.4 ± 0.4 n= 3									
0900	5.58	40N	30.0	94. ± 2.9								
			30.4	34. (u/d 36%)								
			30.5									
0902	5.61	40S	30.5	85. ± 5.0								
			30.7	43. (u/d 49%)								
1158	8.55	39N	31.1	49. ± 3.5								
			31.3	22. (u/d 45%)								
1201	8.60	39S	31.6	55. ± 4.3								
			31.9	22. (u/d 40%)								
1340	10.25	40	31.1		31.	32.5	1938	10.0				
1350	10.41	41S	31.0	16. ± 1.3								
			30.6	17. (u/d 107%)								
1352	10.45	41N	30.8	33. ± 3.0								
			30.9	15. (u/d 44%)								
1432	11.11	N	31.9 ± 1.1 n= 9									
		S	31.4 ± 1.0 n= 9									
1523	11.96	N	31.6 ± 1.0 n=13									
		S	31.4 ± 0.6 n=13									
1552	12.45	N	31.1 ± 0.6 n=12									
		S	31.1 ± 0.8 n=12									
1612	12.78	43N	30.3	24. ± 2.0								
1616	12.85	43S	30.2	16. ± 2.2								
1618	12.88	43N	30.0									.923
1623	12.96	43S	30.1									.912

Run #	Date	Time	Hours	from Warm-up	Flexural Strength north	Flexural Strength south	mean
TURN CIRC 1	11/23/2001	1414	10.81		33.1	22.9	28.0
TURN CIRC 2	11/23/2001	1507	11.70		28.0	18.2	23.1
TURN CIRC 3	11/23/2001	1539	12.23		25.3	15.9	20.6

NRC - INSTITUTE FOR MARINE DYNAMICS

ARCTIC VESSEL RESEARCH SECTION

ICE MECHANICAL PROPERTIES SUMMARY

Test Name: HEALY17

Project Number: 919

Warm up commenced: 00:03 27-NOV-2001

Time	Warm-up hrs	Loc	hi mm	Sf kPa	Lc cm	E MPa	E/Sf	Lc/hi	K1c N/m	Sf/K1c m-.5	Sc/s kPa	Rhoi Mg/m3
0819	8.27	N	42.2 ± 1.1 n= 3									
		S	41.3 ± 1.3 n= 3									
0841	8.63	40S	41.7		52.	104.7	2156	12.4				
0855	8.87	39N	41.9	49. ± 2.3								
			42.2	31. (u/d 63%)								
0857	8.90	39S	42.6	47. ± 2.6								
			42.4	34. (u/d 72%)								
1009	10.10	38N	42.5	47. ± 0.5								
			42.5	25. (u/d 52%)								
1011	10.13	38S	42.8	45. ± 1.7								
			42.7	33. (u/d 72%)								
1015	10.20	38S	42.7									.851
1050	10.78	N	41.8 ± 0.8 n=12									
		S	41.8 ± 0.8 n=12									
1055	10.87	40N	42.9	41. ± 5.8								
			42.4	14. (u/d 33%)								
1059	10.93	40S	42.9	21. ± 3.3								
			43.3	17. (u/d 80%)								
1200	11.95	N	42.0 ± 1.2 n= 9									
		S	42.0 ± 1.2 n= 9									
1213	12.17	36S	41.7									.880
1338	13.58	41N	42.0	29. ± 3.0								
			42.3	16. (u/d 54%)								
1340	13.62	41S	43.1	29. ± 1.0								
			42.3	16. (u/d 53%)								
1455	14.87	45N	42.8	23. ± 3.3								
			42.0	16. (u/d 69%)								

1457	14.90	45S	43.3	23. ± 4.4
			43.2	19. (u/d 81%)

1541	15.63	N	42.3 ± 0.5	n=13
		S	42.6 ± 0.3	n=13

1558	15.92	62S	41.8		.868
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Run #	Date	Time	Hours from Warm-up	Flexural Strength		
				north	south	mean
TURN CIRC 1	11/27/2001	0935	9.53	47.9	39.0	43.5
TURN CIRC 2	11/27/2001	1145	11.70	36.1	31.2	33.7
TURN CIRC 3	11/27/2001	1520	15.28	22.6	21.7	22.1

NRC - INSTITUTE FOR MARINE DYNAMICS

ARCTIC VESSEL RESEARCH SECTION

ICE MECHANICAL PROPERTIES SUMMARY

Test Name: HEALY18

Project Number: 919

Warm up commenced: 21:46 28-NOV-2001

Time	Warm-up hrs	Loc	hi mm	Sf kPa	Lc cm	E MPa	E/Sf	Lc/hi	K1c N/m	Sf/K1c m ^{-1.5}	Sc/s kPa	Rhoi Mg/m ³
0835	10.81	N	41.9 ± 1.2	n= 3								
		S	40.1 ± 0.1	n= 3								
0843	10.95	40S	41.8		46.	65.6	1256	11.1				
0858	11.20	40N	41.7	51. ± 2.2								
			41.3	30. (u/d 60%)								
0904	11.30	40S	40.4	50. ± 2.6								
			40.2	34. (u/d 67%)								
1030	12.73	39N	41.6	46. ± 3.4								
			41.6	24. (u/d 53%)								
1033	12.78	39S	41.0	53. ± 1.4								
			40.7	17. (u/d 32%)								
1114	13.46	38N	41.7	42. ± 1.8								
			42.0	29. (u/d 69%)								
1118	13.53	38S	41.1	49. ± 4.0								
			40.9	17. (u/d 34%)								
1225	14.65	37N	41.2	33. ± 2.7								
			41.3	21. (u/d 64%)								
1230	14.73	37S	40.7	34. ± 2.3								
			41.0	22. (u/d 64%)								
1314	15.46	N	40.7 ± 0.9	n=12								
		S	40.8 ± 0.9	n=12								
1331	15.75	24N	39.5									.861
1406	16.33	N	41.4 ± 0.8	n=12								
		S	41.3 ± 0.6	n=12								
1421	16.58	48N	41.2									.875
1434	16.80	36N	40.9	28. ± 1.2								

1439	16.88	36S	40.6	27. ± 1.3	
			40.5	16. (u/d 61%)	
1520	17.56	N	41.1 ± 0.6	n=11	
		S	41.3 ± 1.0	n=11	
1535	17.81	60S	41.1		.868

Appendix C

Turning circle diameter analysis

The turning diameter was estimated from the measured channel profile, i.e., a set of x, y pairs that are supposed to reside on a circular arc, but with some noise. For a set of measured x and y coordinate pairs, the equation for the circle to these points is:

$$(x - x_c)^2 + (y - y_c)^2 = R^2 \quad \text{C1}$$

where x_c, y_c and R are the x and y coordinates and the radius of the circle, respectively.

Figures C1 to C8 show the channel profile for each test runs respectively.

