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### Design heat transmission coefficients

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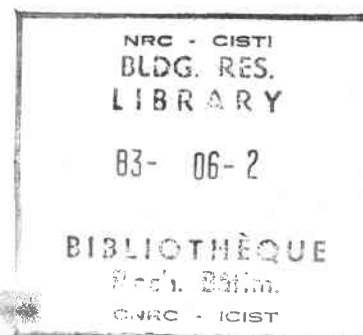
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# DESIGN HEAT TRANSMISSION COEFFICIENTS

CHAPTER 22, ASHRAE HANDBOOK 1977  
FUNDAMENTALS VOLUME

ANALYZED



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## PREFACE

There is a continuing requirement in the work of architects, engineers, and others concerned with heating, ventilating, and air-conditioning of buildings for tabulated information on the heat transmission coefficients of building materials and building sections. The ASHRAE Handbook 1977 Fundamentals Volume is the most authoritative and the most widely used reference source in this connection. The Division is indebted to the Society for permission to reproduce Chapter 22 in full for the assistance and convenience of Canadians requiring such information.

Chapter 22 is based upon the best information available and is kept up to date through frequent revisions. It is applicable to Canadian as well as to United States conditions and it is recommended for use in the estimation of heating and cooling loads and in other heat transfer problems in buildings. Any reservations to be observed in its use are given in the text and in the footnotes to the various tables. It is impossible to guarantee that the values given will apply to a particular product. They are considered to be the most representative values that can be established for use in design. For conductivity of a particular product the user may obtain the value supplied by the manufacturer or secure the results of unbiased tests.

As this ASHRAE Chapter is frequently revised, successive printings as a DBR paper can be based on the most recent version. Chapter 9 of the 1960 ASHRAE Guide and Data Book (as it was then called) was first used to replace a DBR compilation issued in 1951 as DBR Technical Paper No. 7. It in turn was replaced by the 1963 revision which was issued as Technical Paper 168 in view of the change in Chapter title and replaced again by the 1965 version. This present reprint, from the 1977 Fundamentals Handbook, is the most up-to-date information on this subject.

Ottawa  
November 1978

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Director  
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# DESIGN HEAT TRANSMISSION COEFFICIENTS

*Heat Transfer Definitions and Symbols; Surface Conductance; Calculating Overall Coefficients; Overall Coefficients and Their Practical Use; Insulating Constructions; Adjustment for Framing; Curtain Walls; Ventilated Attics; Foundation Coefficients; Glass and Door Coefficients; Wind Effects; Heat Loss Due to Infiltration; Calculating Surface Temperatures; Conductivity of Industrial Insulations; Bare Surface Heat Losses; Heat Flow Calculations; Buried Pipe Lines; Thermal Characteristics and Response Factors for Floors, Walls, and Roofs*

**T**HE design of a heating, refrigerating, or air-conditioning system, including selection of building insulation, sizing of piping and ducts, or evaluation of thermal performance of system parts is based on the principles of heat transfer given in Chapter 2. The equations most widely used to estimate heat transfer loads chargeable to the various parts will usually determine the heat transfer rate under steady state conditions. For a given part under standard conditions, this rate is a specific value,  $U$ , the *overall coefficient of heat transmission* or thermal transmittance.

This chapter is concerned with the concepts and procedures for determining such coefficients, and includes a brief discussion of factors that may affect the values of these coefficients and performance of thermal insulations. Coefficients may be determined by testing, or computed from known values of thermal conductance of the various components. Procedures for calculating coefficients are illustrated by examples and, because it is impracticable to test all combinations of materials, tables of computed design values for the more common constructions are given.

Units in this chapter are in the customary (i.e., U.S., English, and cgs) systems. In the following definitions of heat transfer, the customary unit, followed by the SI unit, is given. Note that although the SI unit of temperature is the kelvin (K), the degree Celsius (formerly centigrade) is properly used with SI units. The temperature interval one degree Celsius equals one kelvin exactly. Factors for converting to SI are given in Table 18 and in Chapter 35.

## HEAT TRANSFER DEFINITIONS AND SYMBOLS

$q$  = *thermal transmission* or rate of heat flow; the quantity of heat flowing due to all mechanisms in unit time under the conditions prevailing at that time; in Btu/hr or (W).

*Note:* Mechanisms relate to modes of heat transfer by solid conduction, mass transfer, gas conduction, convection, and radiation. These may occur separately or in combination, partially or totally depending upon specific circumstances.

$k$  or  $\lambda$  = *thermal conductivity*; the thermal transmission, by conduction only, in unit time through unit area of an infinite slab in a direction perpendicular to the surface, when unit difference in temperature is established between the surfaces; in (Btu · in.)/(hr · ft<sup>2</sup> · F) or W/(m · K).

*Note 1:* A body is considered homogeneous when the above property is found by measurement to be independent of sample dimensions.

*Note 2:* The property must be identified with a specific mean temperature, which varies with temperature; and a direction and orientation of thermal transmission, since some bodies are not isotropic with respect to the property.

*Note 3:* For many thermal insulation materials, thermal transmission occurs by a combination of modes of heat transfer. The measured property should be referred to as an effective or apparent thermal conductivity for the specific test conditions (sample thickness and orientation, environment, environmental pressure, and temperature difference).

The preparation of this chapter is assigned to TC 4.4, Insulation and Moisture Barriers.

$r$  or  $w$  = *thermal resistivity*; the reciprocal of thermal conductivity; (hr · ft<sup>2</sup> · F)/(Btu · in.) or (m · K)/W.

$C$  = *thermal conductance*; the thermal transmission in unit time through unit area of a particular body or assembly having defined surfaces, when unit average temperature difference is established between the surfaces; Btu/(hr · ft<sup>2</sup> · F) or W/(m<sup>2</sup> · K).

*Note 1:* The average temperature of a surface is one that adequately approximates that obtained by integrating the temperature over the body.

*Note 2:* When the two defined surfaces of a mass-type thermal insulation are not of equal areas, as in the case of thermal transmission in a radial direction (see Chapter 2, Table 2), or are not of uniform separation (thickness), an appropriate average area and average thickness must be given.

*Note 3:* When heat transfer is by conduction alone, the average thermal conductivity is the product of the thermal conductance per unit area and the thickness. The average thermal resistivity is the reciprocal of the average thermal conductivity. When conduction is supplemented by any or all of the other modes of heat transfer, the *apparent or effective thermal conductivity* is obtained by multiplying the thermal conductance by the thickness. The apparent or effective resistivity is the reciprocal of the apparent or effective thermal conductivity.

*Note 4:* Where there is air passage through the body, the effective thermal conductance (resistance) must include details of the pressure difference across the body. For a body which is transparent to light, the effective thermal conductance (resistance) may include fenestration, but the optical properties or shading coefficient of the body must be given.

*Note 5:* The thermal conductance of some bodies is related to their thickness. In such cases, the apparent thermal conductivity is a function of thickness. For this reason, it is preferable to express results as effective thermal conductances (resistances) rather than effective thermal conductivities (resistivities).

*Note 6:* "Total" and "areal" thermal conductance are often used as synonyms for thermal conductance.

*Note 7:* Values of thermal conductance (referred to as *conductances*) and their inverses (*resistances*) of the more common building materials are tabulated later in this chapter.

$R$  = *thermal resistance*; the reciprocal of thermal conductance; (hr · ft<sup>2</sup> · F)/Btu or (m<sup>2</sup> · K)/W.

$U$  = *thermal transmittance*; the thermal transmission in unit time through unit area of a particular body or assembly, including its boundary films, divided by the difference between the environmental temperatures on either side of the body or assembly; Btu/(hr · ft<sup>2</sup> · F) or W/(m<sup>2</sup> · K).

*Note 1:* This is often referred to as the *overall coefficient of heat transfer*.

*Note 2:* In practice, the fluid is air, the boundary film is thin, and the average temperature of the fluid is that obtained by averaging over a finite region of the fluid near this film.

$h$  = *film or surface conductance*; the thermal transmission in unit time to or from unit area of a surface in contact with its surroundings for unit difference between the temperature of the surface and the environmental fluid temperature; Btu/(hr · ft<sup>2</sup> · F) or W/(m<sup>2</sup> · K).

*Note 1:* The surroundings must involve air or other fluids for radiation and convection to take place.

Note 2: Subscripts  $i$  and  $o$  are often used to denote inside and outside surface conductances, respectively.

$\epsilon$  = *emittance*; the ratio of the radiant flux emitted by a specimen to that emitted by a blackbody at the same temperature.

Note: The combined effect of the surface emittances of boundary surfaces of an air space where the boundaries are assumed to be parallel and of large dimensions, as compared to the distance between them, is often referred to as *effective emittance* ( $E$ ). Values for a range of air spaces and conditions are tabulated later in this chapter.

$\rho$  = *surface reflectance*; the ratio of the radiant flux reflected by an opaque surface to that falling upon it; dimensionless.

## SURFACE CONDUCTANCE

The convection part of surface conductance is affected by air movement. Fig. 1 shows results of tests<sup>1</sup> made on 12-in. square samples of different materials at a mean temperature of 20 F for wind velocities up to 40 mph. These conductances include the radiation portion of the coefficient which, for the test conditions, was about 0.7 Btu/(hr · ft<sup>2</sup> · F). More recent tests<sup>2</sup> on smooth surfaces show surface length also significantly affects the convection part of conductance; the average value decreases as surface length increases. Moreover, observations<sup>3</sup> of the magnitude of low temperature radiant energy received from outdoor surroundings show that only under certain conditions may the outdoors be treated as a blackbody radiating at air temperature.

## CALCULATING OVERALL COEFFICIENTS

Using the principles of heat transfer in Chapter 2, it is possible to calculate overall coefficients with the resistance method. The total resistance to heat flow through a flat ceiling, floor, or wall (or a curved surface if the curvature is small) is equal numerically to the sum of the resistances in series.

$$R_T = R_1 + R_2 + R_3 + R_4 + \dots + R_n \quad (1)$$

where  $R_1, R_2$ , etc., are the individual resistances of the wall components, and  $R_T$  is total resistance.

For a wall of a single homogeneous material of conductivity  $k$  and thickness  $L$  with surface coefficients  $h_i$  and  $h_o$ :

$$R_T = \frac{1}{h_i} + \frac{L}{k} + \frac{1}{h_o} \quad (2)$$

Then, by definition:

$$U = 1/R_T$$

For a wall with air space construction, consisting of two homogeneous materials of conductivities  $k_1$  and  $k_2$  and thicknesses  $L_1$  and  $L_2$ , respectively, separated by an air space of conductance  $C$ :

$$R_T = \frac{1}{h_i} + \frac{L_1}{k_1} + \frac{1}{C} + \frac{L_2}{k_2} + \frac{1}{h_o} \quad (3)$$

and

$$U = 1/R_T$$

The temperature at any interface can be calculated, since the temperature drop through any component of the wall is proportional to its resistance. Thus, the temperature drop  $\Delta t_1$  through  $R_1$  in Eq 1 is:

$$\Delta t_1 = R_1(t_i - t_o)/R_T \quad (4)$$

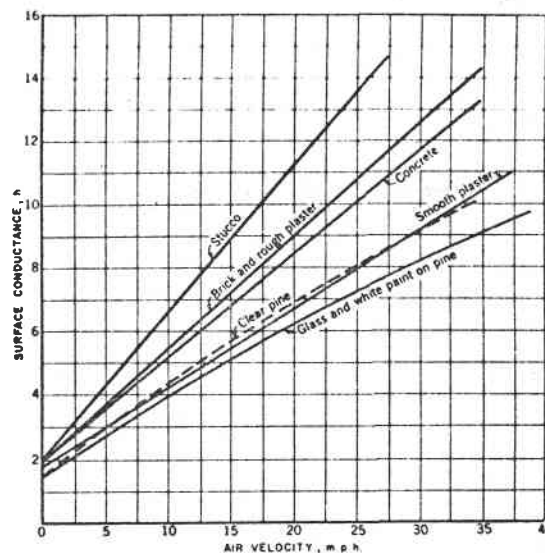


Fig. 1 Surface Conductance for Different 12-in. Square Surfaces as Affected by Air Movement<sup>1</sup>

where  $t_i$  and  $t_o$  are the indoor and outdoor temperatures, respectively.

Hence, the temperature at the interface between  $R_1$  and  $R_2$  is:

$$t_{1-2} = t_i - \Delta t_1 \quad (5)$$

For types of building materials having nonuniform or irregular sections such as hollow clay tile or concrete blocks, it is necessary to use the conductance  $C$  of the section unit as manufactured. The resistance  $R$  of the section  $1/C$  would be used as one of the resistances in an equation similar to Eq 2 and 3.

Note that in order to compute the  $U$ -value of a construction, it is first necessary to know the conductivity and thickness of homogeneous materials, conductance of nonhomogeneous materials (such as concrete blocks), surface conductances of both sides of the construction, and conductances of any air spaces or the thermal resistances of individual elements.

If the conductivities of materials in a wall are highly dependent on temperature, the mean temperature must be known to assign the correct value. In such cases, it is perhaps most convenient to use a trial and error procedure for the calculation of the total resistance,  $R_T$ . First, the mean operating temperature for each layer is estimated and conductivities  $k$  or conductances  $C$  selected. The total resistance  $R_T$  is then calculated as in Eq 3 and then the temperature at each interface is calculated from Eq 4 and 5.

The mean temperature of each component (arithmetic mean of its surface temperatures) can then be used to obtain conductivities  $k$  or conductances  $C$ . For nonlinear relationships, see Chapter 19, Fig. 2. This procedure can then be repeated until the conductivities or conductances have been correctly selected for the resulting mean temperatures. Generally, this can be done in two or three trial calculations.

## Series and Parallel Heat Flow Paths

In many installations, components are arranged so that parallel heat flow paths of different conductances result. If there is no lateral heat flow between paths, each path may be considered to extend from inside to outside, and transmittance of each path may be calculated using Eq 1 or 3. The average transmittance is then:

$$U_{(av)} = a(U_a) + b(U_b) + \dots + n(U_n) \quad (6)$$

where  $a, b, \dots, n$  are respective fractions of a typical basic area composed of several different paths whose transmittances are  $U_a, U_b, \dots, U_n$ .

If heat can flow laterally in any continuous layer so that transverse isothermal planes result, total average resistance  $R_{T(av)}$  will be the sum of the resistances of the layers between such planes, each layer being calculated by the appropriate Eq 1 or a modification of Eq 6, using the resistance values. This is a series combination of layers, of which one (or more) provides parallel paths.

The calculated transmittance, assuming parallel heat flow only, is usually considerably lower than that calculated with the assumption of combined series-parallel heat flow. The actual transmittance will be some value between the two calculated values. In the absence of test values for the combination, an intermediate value should be used; examination of the construction will usually reveal whether a value closer to the higher or lower calculated value should be used. Generally, if the construction contains any highly conducting layer in which lateral conduction is very high compared to transmittance through the wall, a value closer to the series parallel calculation should be used. If, however, there is no layer of high lateral conductance, a value closer to the parallel heat flow calculation should be used, as illustrated in *Example 1*.

**Example 1:** Consider a construction consisting of:

1. Inside surface having film coefficient  $h_i = 2$ .
2. A continuous layer of material of resistance  $R_1 = 1$ .
3. A parallel combination containing two heat flow paths of proportionate areas,  $a = 0.1$ , and  $b = 0.9$ , with resistances  $R_{a2} = 1$  and  $R_{b2} = 8$ .
4. A continuous layer of material of resistance  $R_3 = 0.5$ .
5. Outside surface having film coefficient  $h_o = 4$ .

**Solution:** If parallel heat flow paths are assumed from air to air, the total resistance through area  $a$  will be:

$$\begin{aligned} R_{aT} &= 1/h_i + R_1 + R_{a2} + R_3 + 1/h_o \\ &= 0.5 + 1 + 1 + 0.5 + 0.25 = 3.25 \end{aligned}$$

and

$$U_a = 1/R_{aT} = 1/3.25$$

The resistance and transmittance through area  $b$  will be:

$$\begin{aligned} R_{bT} &= 1/h_i + R_1 + R_{b2} + R_3 + 1/h_o \\ &= 0.5 + 1 + 8 + 0.5 + 0.25 = 10.25 \end{aligned}$$

and

$$U_b = 1/R_{bT} = 1/10.25$$

Then the average calculated transmittances will be:

$$U_{(av)} = a(U_a) + b(U_b) = \frac{0.1}{3.25} + \frac{0.9}{10.25} = 0.119$$

If, however, isothermal planes are assumed to occur at both surfaces of  $R_1$  and of  $R_3$ , the total calculated resistance will be:

$$R_T = 1/h_i + R_1 + \frac{(R_{a2})(R_{b2})}{aR_{b2} + bR_{a2}} + R_3 + 1/h_o$$

$$\frac{(R_{a2})(R_{b2})}{aR_{b2} + bR_{a2}} = \text{combined resistance of } R_{a2} \text{ and } R_{b2} = 4.71$$

$$\text{Then, } R_T = 0.5 + 1 + 4.71 + 0.5 + 0.25 = 6.96$$

$$\text{and } U_{(av)} = 1/6.96 = 0.144$$

If  $R_1$  and  $R_3$  are values for homogeneous materials, a value of about 0.125 might be selected; whereas, if they contain a highly conducting layer, a value of 0.135 might be selected.

When the construction contains one or more paths of small area having a high conductance compared to the conductance of the remaining area, the following method is suggested.

### Heat Flow Through Panels Containing Metal

The transmittance of a panel which includes metal or other highly conductive material extending wholly or partly through insulation should, if possible, be determined by test in the guarded hot box. When a calculation is required, a good approximation can be made by a *Zone Method*. This involves two separate computations—one for a chosen limited portion, *Zone A*, containing the highly conductive element; the other for the remaining portion of simpler construction, called *Zone B*. The two computations are then combined, and the average transmittance per unit of overall area is calculated. The basic laws of heat transfer are applied, by adding area conductances  $C \cdot A$  of *elements in parallel*, and adding area resistances  $R \cdot A$  of *elements in series*.

The surface shape of *Zone A* is determined by the metal element. For a metal beam (Fig. 2 and 3), the *Zone A* surface is a strip of width  $W$ , centered on the beam. For a rod perpendicular to panel surfaces, it is a circle of diameter  $W$ . The value of  $W$  is calculated from Eq 7, which is empirical.

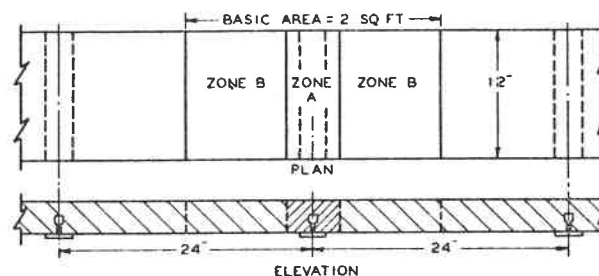
$$W = m + 2d \quad (7)$$

where

$m$  = width or diameter of the metal heat path terminal, inches.

$d$  = distance from panel surface to metal, inches. The value of  $d$  should not be taken less than 0.5 in. (for still air).

In general, the value of  $W$  should be calculated by Eq 7 for



For enlarged section of Zone A, see Fig. 3

Fig. 2 Gypsum Roof Deck on Bulb Tees

		SECT NO	STEEL AREA SQ FT	NON-STEEL AREA SQ FT
ROOFING	1 1/2"	1	0	0.302
		2	0	0.302
GYPSUM CONCRETE	5/8"	3	0.052	0.250
		4	0.010	0.292
STEEL BULB TEE	1"	5	0.167	*
		6	0	0.302
GLASS FIBER INSULATION	1/2"	7	0	0.302
		8	0	0.302

Fig. 3 Enlarged Section of Zone A of Fig. 2

each end of the metal heat path, and the larger value, within the limits of the *basic area*, should be used as illustrated in *Example 2*.

**Example 2:** Calculate transmittance of the roof deck shown in Fig. 2 and 3. Tee-bars on 24-in. centers support glass fiber form boards, gypsum concrete, and built-up roofing. Conductivities of components are: steel 312; gypsum concrete 1.66; glass fiber 0.25. Conductance of built-up roofing is 3.0.

**Solution:** The *basic area* is 2 ft<sup>2</sup> (24 in. × 12 in.), with a tee-bar (12 in. long) across the middle. This area is divided into *Zones A* and *B*.

*Zone A* is determined from Eq 7 as follows:

$$\text{Top Side } W = m + 2d = 0.625 + 2 \times 1.5 = 3.625 \text{ in.}$$

$$\text{Bottom Side } W = m + 2d = 2.0 + 2 \times 0.5 = 3.0 \text{ in.}$$

Using the larger value of *W*, the area of *Zone A* is (12 × 3.625) / 144 = 0.302 ft<sup>2</sup>. The area of *Zone B* is 2.0 = 0.302 = 1.698 ft<sup>2</sup>.

To determine area transmittance for *Zone A*, the structure within the zone is divided into five sections parallel to the top and bottom surfaces as shown in Fig. 3. The area conductance *C · A* of each section is calculated by adding the area conductances of its metal and nonmetal paths. Area conductances of the sections are converted to area resistances 1/(*R · A*) and added, to obtain total resistance of *Zone A*.

Section	Area × Conductance	<i>C · A</i>	1/( <i>C · A</i> ) = <i>R/A</i>
Air (outside, 15 mph)	0.302 × 6.0	1.812	0.552
No. 1, Roofing	0.302 × 3.0	0.906	1.104
No. 2, Gypsum concrete	0.302 × 1.66/1.125	0.446	2.242
No. 3, Steel	0.052 × 312.0/0.625	26.0	}0.038
No. 3, Gypsum concrete	0.250 × 1.66/0.625	0.664	
No. 4, Steel	0.0104 × 312/1.00	3.24	}0.302
No. 4, Glass fiber	0.292 × 0.25/1.00	0.073	
No. 5, Steel	0.167 × 312/0.125	416.83	0.002
Air (inside)	0.302 × 1.63	0.492	2.031
Total <i>R/A</i> = 6.271			

Area transmittance of *Zone A* = 1/(*R/A*) = 1/6.271 = 0.159.

For *Zone B*, the unit resistances are added and then converted to area transmittance, as shown in the following table.

Section	Resistance, <i>R</i>	
Air (outside, 15 mph)	1/6.0	= 0.167
Roofing	1/3.0	= 0.333
Gypsum concrete	1.75/1.66	= 1.054
Glass fiber	1.00/0.25	= 4.000
Air (inside)	1/1.63	= 0.613
Total resistance	= 6.167	

Unit transmittance = 1/*R* = 0.162

Area transmittance *U · A*

for *Zone B* = 1.698 × 0.162 = 0.275

for *Zone A* = 0.159

Total area transmittance of *basic area* = 0.434

Transmittance per ft<sup>2</sup> = 0.434/2.0 = 0.217

In tests on similar construction, made by the guarded hot-box method, one laboratory reported a *U*-value of 0.219 Btu/(hr · ft<sup>2</sup> · F), and another laboratory reported a *U*-value of 0.206 Btu/(hr · ft<sup>2</sup> · F).

When the steel is a large proportion of the heat path, as in *Example 2*, detailed calculations of resistance in sections 3, 4, and 5 of *Zone A* are not justified. If only the steel were considered, the final result of *Example 2* would be unchanged.

If the steel path is small, as for a tie rod, detailed calculations for section 3, 4, and 5 are necessary (see Table 4H).

### Caution

A panel with internal metallic structure, bonded on one or both sides to a metal skin or covering, presents special problems of lateral heat flow not covered in the foregoing *Zone Method*.

### Series Heat Flow through Unequal Areas

A construction may be made up of two or more layers (flat or of small curvature) of unequal area, separated by an air space and arranged so that heat flows through the layers in series. The most common such construction is a ceiling and roof combination where the attic space is unheated and unventilated. A combined coefficient based on the most convenient area from air inside to air outside can be calculated from Eq 8.

$$R_T = \frac{1}{U_1} + \frac{1}{n_2 U_2} + \frac{1}{n_3 U_3} + \cdots + \frac{1}{n_p U_p} \quad (8)$$

The combined coefficient *U* is the reciprocal of *R<sub>T</sub>*, or *U* = 1/*R<sub>T</sub>*

where

*U* = combined coefficient to be used with *A<sub>1</sub>*.

*R<sub>T</sub>* = total resistance to all elements in series.

*U<sub>1</sub>, U<sub>2</sub>, ..., U<sub>p</sub>* = coefficient of transmission of *A<sub>1</sub>, A<sub>2</sub>, ..., A<sub>p</sub>*, respectively.

*n<sub>2</sub>, n<sub>3</sub>, ..., n<sub>p</sub>* = area ratios *A<sub>2</sub>/A<sub>1</sub>, A<sub>3</sub>/A<sub>1</sub>, ..., A<sub>p</sub>/A<sub>1</sub>*, respectively.

Note that the overall coefficient should be multiplied by the area *A<sub>1</sub>* to determine the heat loss. Values of *U<sub>1</sub>, U<sub>2</sub>, U<sub>3</sub>, ..., U<sub>p</sub>* should be calculated using Eq 1, 2, or 3; if any layer contains parallel heat flow paths (i.e., windows or dormers on roofs), Eq 6 may be used.

In the calculation, the resistance of the air spaces between layers should be accounted for by assigning one-half of an appropriate air space resistance to each of the layers, rather than the conductance of the surface.

### *U<sub>o</sub>* Concept

In section 4.0 of ASHRAE *Standard 90-75, Energy Conservation in New Building Design*, requirements are stated in terms of *U<sub>o</sub>*, where *U<sub>o</sub>* is the combined thermal transmittance of the respective areas of gross exterior wall, roof/ceiling, and floor assemblies. The *U<sub>o</sub>* equation for a wall is as follows:

$$U_o = \frac{U_{\text{wall}} A_{\text{wall}} + U_{\text{window}} A_{\text{window}} + U_{\text{door}} A_{\text{door}}}{A_o}$$

where

*U<sub>o</sub>* = the average thermal transmittance of the gross wall area, Btu/h · ft<sup>2</sup> · F

*A<sub>o</sub>* = the gross area of exterior walls, ft<sup>2</sup> (m<sup>2</sup>)

*U<sub>wall</sub>* = the thermal transmittance of all elements of the opaque wall area, Btu/h · ft<sup>2</sup> · F

*A<sub>wall</sub>* = opaque wall area, ft<sup>2</sup>

*U<sub>window</sub>* = the thermal transmittance of the window area, Btu/h · ft<sup>2</sup> · F

*A<sub>window</sub>* = window area (including sash) ft<sup>2</sup>

*U<sub>door</sub>* = the thermal transmittance of the door area, Btu/h · ft<sup>2</sup> · F

*A<sub>door</sub>* = door area, ft<sup>2</sup>

NOTE: Where more than one type of wall, window and/or

door is used, the  $U \times A$  term for that exposure shall be expanded into its sub-elements, as:

$$U_{wall_1} A_{wall_1} + U_{wall_2} A_{wall_2}, \text{etc.}$$

### OVERALL COEFFICIENTS AND THEIR PRACTICAL USE

The values in Tables 1, 2, 2C, 3A, and 3B for component elements and materials were selected by ASHRAE Technical Committee 4.4, as representative. They are based on available published data obtained by the guarded hot plate method (ASTM C177), heat flow meter method ASTM C518, or by the guarded hot box method (ASTM C236). Because of variations in commercially available materials of the same type, not all of these selected representative values will be in exact agreement with data for individual products. The value for a particular manufacturer's material can be secured from unbiased tests or from guaranteed manufacturer's data.

The most exact method of determining the heat transmission coefficient for a given combination of building materials assembled as a building section is to test a representative section in a guarded hot box. However, it is not practicable to test all the combinations of interest. Experience has indicated that  $U$ -values for many constructions, when calculated by the methods given in this chapter, using accurate values for component materials, and with corrections for framing member heat loss, are in good agreement with the values determined by guarded hot box measurements, when there are no free air cavities within the construction.

#### Simplified Procedure for Determining $U$ -Values

Tables 4A through 4K illustrate the procedure which enables the engineer to determine and compare values for many types of construction. To determine the  $U$ -value for uninsulated construction, use Tables 4A through 4K. The benefit derived from addition of insulation materials is shown in Tables 5A and 5B. The average  $U$ -value is then determined by Eq 9. Additional summer values for ventilated and nonventilated attics are given in Table 6.

This simplified procedure provides a means of evaluating economic considerations involved in selection of insulating material, as adapted to various building constructions.

Special attention must be given to vapor barriers, outlined in Chapters 19 and 20. Moisture from condensation or other sources reduces the heat flow resistance of insulation.

#### Values Used in Calculation of $U$ -Value Tables

Tables 4A through 4K are based on values given in Tables 1, 2, and 3A. The following conditions have been used to calculate the  $U$ -value by including framing members or other areas of through conduction.

Equilibrium or steady state heat transfer, eliminating effects of heat capacity.

Surrounding surfaces at ambient air temperatures.

Exterior wind velocity of 15 mph for winter (surface  $R = 0.17$ ) and 7.5 mph for summer (surface  $R = 0.25$ ).

Surface emittance of ordinary building materials  $\epsilon = 0.90$ .

Eq 9 is used to correct for the effect of framing members.

$$U_{av} = \frac{S}{100}(U_s) + \left(1 - \frac{S}{100}\right)(U_i) \quad (9)$$

where

$U_{av}$  = average  $U$  value for building section.

$U_i$  =  $U$  value for area between framing members.

$U_s$  =  $U$  value for area backed by framing members.

$S$  = percentage of area backed by framing members.

For those systems with complicated geometry,  $U_{av}$  should be measured by laboratory tests on a large, representative area of the building section including the framing system.

**Example 3:** Parallel heat flow through framing (studs, joists, plates, furring, etc.) and insulated areas is calculated by Eq 9. Consider a frame wall with R-11 insulation, a  $U_i$ -value across the insulated space of 0.069 ( $R = 14.43$ ), and a  $U_s$ -value across the framing of 0.128 ( $R = 7.81$ ). Assuming a 20% framing (typical for 16-in. in o.c. framing including multiple studs, plates, headers, sills, band joists, etc.), the average  $U$ -value of this wall can be calculated.

$$U_i = 0.069; U_s = 0.128; S = 20$$

$$U_{av} = (0.2)(0.128) + (0.8)(0.069) = 0.026 + 0.055 = 0.081$$

For a frame wall with 24-in. o.c. stud space, the framing factor is estimated at 15%. In this case, the average  $U$ -value becomes 0.078. Depending on the care and installation of the insulation,  $U$ -values obtained in practice may be higher than those calculated here.

In construction involving air spaces, the  $U$ -values shown are calculated for areas between framing. See examples in Table 4 if an allowance is to be made for this effect.

To condense the tables, an average resistance value (avg  $R$ ) has been used in some tables for types of materials having approximately the same thermal resistance values. The difference between the average value and the exact value for any given material usually causes no significant change in the resulting  $U$ -value.

*Actual thicknesses of lumber assumed to be as follows:*

Nominal	Actual	Nominal	Actual
1 in. (S-2-S) . . . . .	0.75 in.	3 in. (S-2-S) . . . . .	2.5 in.
1.5 in. (S-2-S) . . . . .	1.25 in.	4 in. (S-2-S) . . . . .	3.5 in.
2 in. (S-2-S) . . . . .	1.5 in.	Finish flooring	
2.5 in. (S-2-S) . . . . .	2 in.	(maple or oak) . . . . .	0.75 in.

Note that the effects of poor workmanship in construction and installation have an increasingly greater percentage effect on heat transmission as the  $U$ -value becomes numerically smaller. Failure to meet design estimates may be caused by lack of attention to exact compliance with specifications. A factor of safety may be employed as a precaution when desirable.

#### Caution

Although the validity of calculating  $U$ -values for all the types of constructions in Tables 4A through 4K, 5A, 5B, 6, and 7 has not been fully demonstrated, calculated values are given because measured values are not available.<sup>4</sup> It is emphasized that the calculated values in Tables 3A, 3B, 4A through 4K, 5, and 6 are given for the convenience of the reader.

In calculating  $U$ -values, exemplary conditions of components and installations are assumed (i.e., that insulating materials are uniformly of the nominal thickness and conductivity, air spaces are of uniform thickness and surface temperatures, effects due to moisture are not involved, and installation details are in accordance with design). Some evidence of departures of measured from calculated values for certain insulated constructions is given in *Building Materials and Structures Report* BMS 151, National Bureau of Standards. To provide a factor of safety to account for departures of constructions from requirements and practices, some may wish to moderately increase the calculated  $U$ -values of the insulated walls, floors, and ceiling sections obtained from Tables 4A through 4K before making adjustments for framing (as indicated in Eq 9). Where reflective air spaces are involved in building construction, and their thermal resistance values constitute a major share of the installed resistance of the insulation, increases of  $U$ -values up to 10% for applications where heat flow is horizontal or upward, and up to 20%



where heat flow is downward, appear reasonable, on the basis of present information. However, to accurately determine thermal resistance values of multiple air spaces, tests on the actual construction should be conducted.<sup>4</sup>

### INSULATED CONSTRUCTIONS—HOW TO USE TABLES 5A AND 5B

In Tables 4A through 4K,  $U$ -values are given for many common types of building wall, floor, and ceiling constructions. For any of these constructions that contain an air space, the tabulated  $U$ -value is based on the assumption that the air space is empty, and its surfaces are of ordinary building materials of high thermal emittance, such as wood, masonry, plaster, or paper. The exception is the example shown in Table 4K where the construction utilizes a reflective air space under winter and summer heat flow conditions. Considerable benefit in reducing the heat transmission coefficient of a construction can be effected by application of thermal insulating materials in the air space.

Table 5A provides a means of determining, without calculation, the  $U$ -value of the between-framing area of various types of construction with added insulation installed in the air space. The left column of Table 5A refers to the  $U$ - or  $R$ -values of designed building sections. The right-hand portion of the table consists of a tabulation of  $U$ -values resulting from the combination of  $U$ - or  $R$ -values shown in the left column with the addition of the  $R$ -values heading each column. In order to use Table 5A, the designer enters the left column with a known  $U$ - or  $R$ -value of a designed building section. Proceeding horizontally across the right-hand portion of the table, he will find  $U$ -values showing improved performance resulting from addition of thermal resistances as shown at the head of each column.

Any and all  $U$ -values are based on a series of assumptions as to nominal characteristics. Common variations in conditions, materials, workmanship, etc., can introduce much greater variations in  $U$ -values than the variations resulting from the assumed mean temperatures and temperature differences described. From this, it is also clear that the use of more than two significant figures in stating a  $U$ -value may assume more precision than can possibly exist.

#### Example of the Use of Table 5A

**Example 4:** Table 4A shows a wood frame construction without insulation and a  $U_f=0.206$  with adjustment for framing. Refer to Table 5A, left-hand column. Enter table at  $U=0.20$ . For improvement of thermal performance of the designed section to  $U=0.07$ , move horizontally to ( $U=0.08$ ) or ( $U=0.06$ ). Read vertically to top of columns, finding that  $R=8$  and  $R=12$  respectively. Interpolating to the desired  $U=0.07$ , it is seen that material having an  $R$ -value of 10 or 11 will satisfy the requirement.

Table 5B is constructed and used similar to Table 5A. However, after having selected the desired  $U$ -value for a roof deck insulation, the values are shown in conductance  $C$  of roof deck insulation. This facilitates specification of materials, since roof deck insulations are available by conductance values ( $C$ ).

### ADJUSTMENT FOR FRAMING

Adjustment for parallel heat flow through framing and insulated areas may be made by using Eq 9. (see Example 3.)

### CURTAIN WALLS

Curtain wall constructions present a combination of metals and insulating materials. Few panels are of true sandwich construction for which the thermal characteristics can be computed by combining the thermal resistances of the several

layers. Many panels have ribs and stiffeners which may create complicated heat flow paths for which it is virtually impossible to calculate the heat transfer coefficients with reliability. Coefficients for the assembled sections must be determined on a representative sample by the guarded hot box method (ASTM C236) for sections which have no free air cavities within the construction.

### VENTILATED ATTICS: SUMMER CONDITIONS (HOW TO USE TABLE 6)

Table 6 is intended to be used with Table 4K (heat flow down), Table 5A, and Eq 9, or when ceiling resistance is known. Its purpose is to determine heat flow resistance of the attic space under varying conditions of ventilating air temperatures and rates, ceiling resistance, roof or sol-air temperatures, and surface emittances.<sup>5</sup> Ventilating air temperature is the outdoor design temperature.

The total resistance,  $R = 1/U$ , obtained by adding the ceiling and attic resistances, can be converted to a  $U$ -value so that the heat gain may be calculated. The applicable temperature difference is that difference between room air and sol-air temperature or between room air and roof temperatures. (See footnote d, Table 6.)

Table 6 may be used for both pitched and flat residential roofs over attic spaces. When there is an attic floor, the ceiling resistance should be that which applies to the complete ceiling-floor construction.

### BASEMENT FLOOR, BASEMENT WALL, AND CONCRETE SLAB FLOOR COEFFICIENTS

The heat transfer through basement walls and floors to the ground depends on: (1) temperature difference between the air within the room and that of the ground; (2) material constituting the wall or floor; and (3) conductivity of the surrounding earth. Conductivity of the earth will vary with local conditions, and is usually unknown. Laboratory tests<sup>6</sup> indicate a heat flow of approximately 2.0 Btu/(hr · ft<sup>2</sup>) through an uninsulated concrete basement floor, with a temperature difference of 20 deg F between basement floor and the air temperature 6 in. above the floors. The  $U$ -value 0.10 is sometimes used for concrete basement floors on the ground. For more detailed procedures, see Ref 7.

For basement walls below grade only, the temperature difference for winter design conditions will be greater than for the floor. Test results indicate a unit area heat loss, at midheight of the basement wall portion below grade, of approximately twice that of the same floor area.

For concrete slab floors laid in contact with the ground at grade level, tests<sup>7</sup> indicate that, for *small floor areas* (equal to that of a house 25 ft square), the heat loss may be calculated as proportional to the length of exposed edge rather than total area. This amounts to 0.81 Btu/(hr)(linear ft of exposed edge) (deg F difference between the indoor air temperature and the average outdoor air temperature). Note that this may be appreciably reduced by insulating under the ground slab and along the edges between the floor and abutting walls. (Also see Chapter 24.) In most calculations, if the perimeter loss is calculated accurately, no other floor loss need be considered.

### GLASS AND DOOR COEFFICIENTS

The  $U$ -values given in Table 8 for flat glass, glass block, and plastic panels were obtained from ASHRAE Research Reports<sup>8</sup> in cases where the panels have been tested. In other instances, values were computed using procedures outlined in Chapter 26. Values in Table 9 for doors were calculated or taken from available published papers. For winter conditions,

an outdoor surface conductance of  $6.0 \text{ Btu}/(\text{hr} \cdot \text{ft}^2 \cdot \text{F})$  was used; for summer conditions,  $4.0 \text{ Btu}/(\text{hr} \cdot \text{ft}^2 \cdot \text{F})$ . The indoor surface conductance was taken as  $1.46 \text{ Btu}/(\text{hr} \cdot \text{ft}^2 \cdot \text{F})$  for vertical surfaces,  $1.63$  for horizontal surfaces with heat flow up, and  $1.08$  for horizontal surfaces with heat flow down. The outdoor surface conductances are for wind velocities of  $15$  and  $7.5 \text{ mph}$ , respectively. Adjustments for other wind velocities may be made using factors in Table 10.

All values are approximate, since some parameters which may have important effects were not considered. For example, in an actual installation, the indoor surface of a glazing panel may be exposed to nearby radiating surfaces, such as radiant-heating panels or exposed windows in adjacent or opposite walls having much higher or lower temperature than the indoor air. Use of the listed  $U$ -value assumes that the surface temperature of surrounding bodies is equal to the ambient air temperature. Air movement across the indoor surface of a panel, such as caused by outlet grilles in the sill, will increase the  $U$ -value.

Shading devices such as venetian blinds, draperies, and roller shades will reduce the  $U$ -value substantially if they fit tightly to the window jambs, head, and sill, and are made of a nonporous material. As a rough approximation, tight-fitting shading devices may be considered to reduce the  $U$ -value of vertical exterior single glazing by  $25\%$  and of vertical exterior double glazing and glass block by  $15\%$ . These adjustments should not be considered in choosing heating equipment, but may be used for calculating design cooling loads.

For panels not vertical or horizontal, such as sloped glass in some types of skylights, calculation procedures outlined in Chapter 26 should be followed. Since data are presented for only vertical, horizontal, and  $45$ -degree sloped surfaces and air spaces, an orientation which most closely approximates the application condition could be used (see Chapter 26).

### WIND VELOCITY EFFECT ON $U$ -VALUES

Table 7 lists factors which, when multiplied by the room or building volume, will give the estimated heat loss due to infiltration.

### CALCULATING SURFACE TEMPERATURES

In many heating and cooling load calculations, it is necessary to determine the inside surface temperature or the temperature of the surfaces within the structure. The resistances through any two paths of heat flow are proportional to the temperature drops through these paths, and can be expressed as:

$$\frac{R_1}{R_2} = \frac{(t_i - t_x)}{(t_i - t_o)} \quad (10)$$

where

$R_1$  = the resistance from the indoor air to any point in the structure at which the temperature is to be determined.

$R_2$  = the overall resistance of the wall from indoor air to outdoor air.

$t_i$  = indoor air temperature.

$t_x$  = temperature to be determined.

$t_o$  = outdoor air temperature.

**Example 5:** Determine the inside surface temperature for a wall having an overall coefficient of heat transmission  $U = 0.25$ , indoor air temperature  $70 \text{ F}$ , and outdoor air temperature  $-20 \text{ F}$ .

**Solution:**

$$R_1 = 1/h_i = 1/1.46 = 0.685$$

$$R_2 = 1/U = 1/0.25 = 4.00$$

Then, by Eq 10:

$$\frac{0.685}{4.000} = \frac{70 - t_x}{70 - (-20)}$$

$$t_x = 54.6 \text{ F}$$

**Example 6:** Determine the temperature of the bottom of a 4-in. insulated concrete roof slab to which has been glued 0.5-in. acoustical tile ( $C = 0.80$ ) as the interior finish. The roof-ceiling overall coefficient of heat transmission,  $U$ , is  $0.14$  for heat flow up. The indoor air temperature is assumed to be  $70 \text{ F}$ , and the outdoor air temperature,  $-20 \text{ F}$ .

**Solution:**

$$R_1 = (1/h_i) + (1/C) = (1/1.63) + (1/0.80) = 1.863$$

$$R_2 = (1/U) = (1/0.14) = 7.143$$

Then, by Eq 10:

$$\frac{1.863}{7.143} = \frac{70 - t_x}{70 - (-20)}$$

$$t_x = 46.5 \text{ F}$$

The concrete surface temperature is of interest since reference to a psychrometric chart or table will show that moisture condensation can occur on this surface under the above conditions ( $46.5 \text{ F}$ ) if the relative humidity in the room exceeds about  $44\%$ . Additional roof insulation should be considered above the slab to avoid condensation at this point if higher relative humidities in the room are anticipated.

The same procedure can be used for determining the temperature at any point within the structure.

A chart for determining inside wall surface temperature is given in Fig. 8, Chapter 8, 1976 ASHRAE HANDBOOK & Product Directory.

### CONDUCTIVITY OF INDUSTRIAL INSULATIONS

The conductivities of various materials used as industrial insulations are given in Table 3B. They are given as functions of the mean temperatures of the arithmetic mean of the inner and outer surface temperature of the insulations.

### BARE SURFACE HEAT LOSSES—FLAT SURFACES AND PIPE

Heat losses from horizontal bare steel pipes, based on tests at Mellon Institute and calculated from the fundamental radiation and convection equations (Chapter 2), are given in Table 11. This table also gives the heat losses or surface conductances for flat, vertical, and horizontal surfaces for surface temperatures up to  $1080 \text{ F}$  with the surrounding air at  $80 \text{ F}$ . The surface per linear ft of pipe is given in the second column of Table 11.

Heat losses from tarnished copper pipe and tube<sup>9</sup> are given in Table 12. The surface per linear ft of tube is given in Table 13. Table 1, Section A, also gives surface conductances for flat surfaces of different emittances and orientations in contact with still air. Table 14 gives area, in  $\text{ft}^2$ , of flanges and fittings for various standard pipe sizes. These tables can be used in estimating the amount of insulation required.

Example 7 shows how the annual heat loss from uncovered pipe may be computed from the data in Table 11.

**Example 7:** Compute total annual heat loss from  $165 \text{ ft}$  of

2-in. bare pipe in service 4000 hr/yr. The pipe is carrying steam at 10 psi pressure and is exposed to an average air temperature of 80 F.

**Solution:** The pipe temperature is taken as the steam temperature, which is 239.4 F, obtained by interpolation from Steam Tables. The temperature difference between the pipe and air =  $239.4 - 80 = 159.4$  F. By interpolation in Table 11 between temperature differences of 150 and 200 F, heat loss from a 2-in. pipe at a temperature difference of 159.4 F is found to be 2.615 Btu/(hr · ft<sup>2</sup> · F). Total annual heat loss from the entire line =  $2.615 \times 159.4 \times 0.622$  (linear ft factor)  $\times 165$  (linear ft)  $\times 4000$  (hr) = 171,100 MB (MB = 1000 Btu).

### HEAT FLOW CALCULATIONS

In calculating heat flow, Eq 11 and 12 are generally used. Eq 11 is used for flat surfaces (Fig. 4), and Eq 12 is used for cylindrical surfaces (Fig. 5).

$$q_s = \frac{t_o - t_a}{(L_1/k_1) + (L_2/k_2) + R_s} \quad (11)$$

$$q_s = \frac{t_o - t_a}{[r_s \log_e(r_1/r_o)]/k_1 + [r_s \log_e(r_s/r_1)]/k_2 + R_s} \quad (12)$$

where

$q_s$  = rate of heat transfer per square foot of outer surface of insulation, Btu per (hour) (square foot).

$k$  = thermal conductivity of insulation at mean temperature, Btu per (hour) (square foot) (degree Fahrenheit per inch thickness).

$L$  = thickness of insulation, inches.

$t_a$  = temperature of ambient air, Fahrenheit.

$t_o$  = temperature of inner surface of insulation, Fahrenheit.

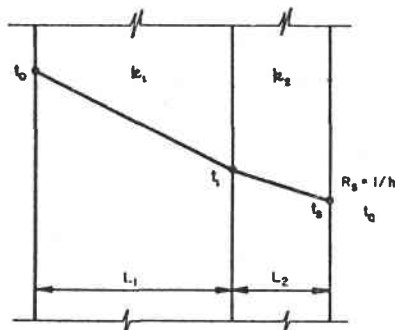


Fig. 4 Heat Flow through Flat Surfaces

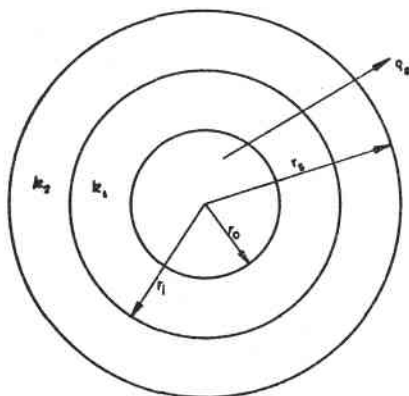


Fig. 5 Heat Flow through Cylindrical Surfaces

$t_s$  = temperature of outer surface of insulation, Fahrenheit.

$r_o$  = inner radius of insulation, inches.

$r_1, r_2, \dots$  = outer radius of intermediate layers of insulation, inches.

$R_s$  = surface resistance =  $1/h$  = (hour) (square foot) (degree Fahrenheit) per Btu.

$h$  = surface conductance coefficient, Btu per (hour) (square foot) (degree Fahrenheit).

$\log_e$  = natural or Napierian logarithm.

To calculate heat flow per ft<sup>2</sup> of pipe surface, use:

$$q_o = q_s (r_s/r_o) \quad (13)$$

where

$q_o$  = rate of heat transfer per square foot of pipe surface, Btu per (hour) (square foot).

For steady state conditions, heat flow through each successive material is the same. However, the temperature drop through each material is proportional to its thermal resistance. The terms which appear in the denominators of Eq 11 and 12 represent the resistances to heat flow.

The heat transferred is inversely proportional to the sum of the resistances ( $R_1 + R_2 + \dots + R_s$ ) of the system. The various temperature drops in the system are proportional to the resistances.

The assumptions used for calculations of heat loss are usually:

$t_o$  = temperature at inner surface of insulation equal to the temperature of fluid in the pipe or container.

$t_a$  = still air ambient temperature = 80 Fahrenheit.

$r_o$  = inner radius of insulation = outside radius of iron pipe.

$r_s$  = outer radius of insulation =  $r_o + L$ .

**Example 8:** Compute heat loss from a boiler wall if the interior insulation surface temperature is 1100 F and ambient still air temperature is 80 F. The wall is insulated with 4.5 in. of mineral fiber block and 0.5 in. of mineral fiber insulating and finishing cement.

**Solution:** Assume that mean temperature of the mineral fiber block is 700 F, mean temperature of the insulating cement is 200 F, and  $R_s = 0.60$ .

From Table 3B,  $k_1 = 0.62$  and  $k_2 = 0.80$ . Then:

$$q_s = \frac{1100 - 80}{(4.5/0.62) + (0.5/0.80) + 0.60} = \frac{1020}{8.483} = 120.2 \text{ Btu/(hr} \cdot \text{ft}^2)$$

As a check, from Fig. 6, at 120.2 Btu/(hr · ft<sup>2</sup>),  $R_s = 0.56$ . The mean temperature of the mineral fiber block is:

$$1100 - (3.63/8.44) (1020) = 1100 - 439 = 661 \text{ F}$$

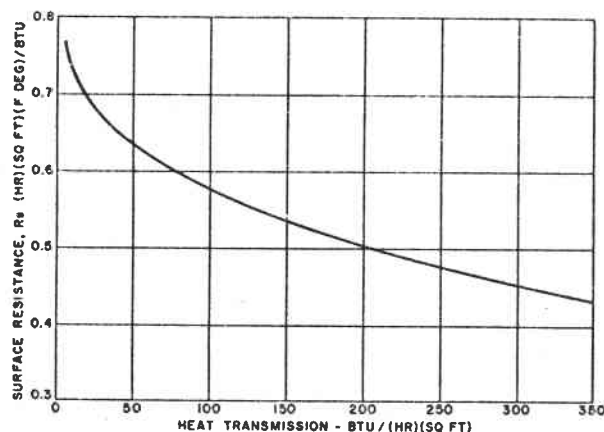
The mean temperature of the insulating cement is:

$$1100 - (7.57/8.44) (1020) = 1100 - 915 = 185 \text{ F}$$

From Table 3B, at 661 F,  $k_1 = 0.60$ , and at 185 F,  $k_2 = 0.79$ . Recalculating  $q_s$  with these adjusted values:

$$q_s = \frac{1020}{(4.5/0.60) + (0.5/0.79) + 0.56} = \frac{1020}{8.69} = 117.4 \text{ Btu/(hr} \cdot \text{ft}^2)$$

From Fig. 6, at 117.4 Btu/(hr · ft<sup>2</sup>),  $R_s = 0.56$ .



(Surface Emittance 0.85 to 0.90 in still Air)

**Fig. 6 Heat Transmission vs Surface Resistance for Flat and Cylindrical Surfaces**

The mean temperature of the mineral fiber block is:

$$1100 - (3.75/8.69) (1020) = 1100 - 440 = 660 \text{ F}$$

The mean temperature of the insulating cement is:

$$1100 - (7.81/8.69) (1020) = 1100 - 917 = 183 \text{ F}$$

From Table 3B, at 661 F,  $k_1 = 0.60$ , and at 183 F,  $k_2 = 0.79$ .

Since  $R_s$ ,  $k_1$ , and  $k_2$  do not change at these values,  $q_s = 117.4$  Btu/(hr · ft<sup>2</sup>).

**Example 9:** Compute heat loss per ft<sup>2</sup> of outer surface of insulation if pipe temperature is 1200 F and ambient still air temperature is 80 F. The pipe is nominal 6-in. iron pipe, insulated with a nominal 3 in. of diatomaceous silica as the inner layer and a nominal 2 in. of calcium silicate as the outer layer.

**Solution:** From Table 15,  $r_o = 3.31$  in. A nominal 3-in. thick diatomaceous silica insulation to fit a nominal 6-in. iron pipe is 3.02 in. thick. A nominal 2-in. thick calcium silicate insulation to fit over the 3.02-in. diatomaceous silica is 2.08 in. thick. Therefore,  $r_i = 6.33$  in.;  $r_s = 8.41$  in.

Assume that the mean temperature of the diatomaceous silica is 600 F, the mean temperature of the calcium silicate is 250 F, and  $R_s = 0.50$ .

From Table 3B,  $k_1 = 0.66$  and  $k_2 = 0.42$ :

$$q_s = \frac{1200 - 80}{\left[ \frac{8.41 \log_e(6.33/3.31)}{0.66} + \frac{8.41 \log_e(8.41/6.33)}{0.40} \right] + 0.50} = \frac{1120}{(5.45/0.66) + (2.39/0.40) + 0.50} = 76.0 \text{ Btu/(hr · ft}^2\text{)}$$

From Fig. 6, at 76.0 Btu/(hr · ft<sup>2</sup>),  $R_s = 0.60$ .

The mean temperature of the diatomaceous silica is:

$$1200 - (4.13/14.83) (1120) = 1200 - 312 = 888 \text{ F}$$

The mean temperature of the calcium silicate is:

$$1200 - (11.24/14.83) (1120) = 1200 - 849 = 351 \text{ F}$$

From Table 3B,  $k_1 = 0.72$  and  $k_2 = 0.46$ . Recalculating:

$$q_s = \frac{1120}{(5.45/0.72) + (2.39/0.46) + 0.60} = 83.8 \text{ Btu/(hr · ft}^2\text{)}$$

From Fig. 6, at 83.8 Btu/(hr · ft<sup>2</sup>),  $R_s = 0.59$ .

Mean temperature of the diatomaceous silica is:

$$1200 - (3.78/13.36) (1120) = 1200 - 317 = 883 \text{ F}$$

Mean temperature of the calcium silicate is:

$$1200 - (10.17/13.36) (1120) = 1200 - 853 = 347 \text{ F}$$

From Table 3B,  $k_1 = 0.72$  and  $k_2 = 0.46$ . Recalculating:

$$q_2 = \frac{1120}{(5.45/0.72) + (2.39/0.46) + 0.59} = 83.8 \text{ Btu/(hr · ft}^2\text{)}$$

Since  $R_s$ ,  $k_1$ , and  $k_2$  will not change at 83.6°C Btu/(hr · ft<sup>2</sup>), this is the final  $q_s$ .

The heat flow per square foot of the inner surface of the insulation will be:

$$q_o = q_s(r_o/r_i) = 83.8(8.41/3.31) = 213 \text{ Btu/(hr · ft}^2\text{)}$$

### HEAT FLOW CALCULATIONS INVOLVING BURIED PIPE LINES

In calculating heat flow from or to buried pipe lines, it is necessary to make an assumption as to the thermal properties of the earth. Because most soil or earth contains moisture, it is technically incorrect to report thermal conductivity. Table 17 gives the *apparent* thermal conductivity values of various soils. These values may be used as a guide when making heat flow calculations involving buried lines. See Ref. 10 for discussion of thermal properties of soil. Ref. 11 gives methods for calculating the heat flow that takes place between one or more buried cylinders and the surroundings.

### THERMAL CHARACTERISTICS AND RESPONSE FACTORS FOR FLOORS, WALLS, AND ROOFS

Current methods for estimating the heat transferred through floors, walls, and roofs of buildings are largely based on a steady state or steady periodic heat flow concept (Equivalent Temperature Difference Concept). The engineering application of these concepts is not complicated and has served well for many years in the process of design and selection of heating and cooling equipment for buildings. However, competitive practices of the building industry sometimes require more than the selection or design of a single heating or cooling system. Consultants are requested to present a detailed comparison of alternative heating and cooling systems for a given building, including initial costs as well as short- and long-term operating and maintenance costs. The degree of sophistication required for costs may make it necessary to calculate the heating and cooling load for estimating energy requirements in hourly increments for a year's time for given buildings at known geographic locations. Because of the number of calculations involved, computer processing becomes necessary. The hour-by-hour heating and cooling load calculations, when based upon a steady heat flow or steady periodic heat flow concept, do not account for the heat storage effects of the building structure, especially with regard to net heat gain to the air-conditioned spaces.

A heat transfer calculation to better account for randomly fluctuating hourly outdoor climatic conditions and indoor energy use schedules, such as lighting, is necessary. A technique called the *response factor method* evaluates the heat conducted through multilayer building elements under transient (nonsteady and nonsteady periodic) exposure conditions. According to this method, the heat flux (Btu/(hr · ft<sup>2</sup>)) at a given time  $t$  at the outer as well as the inner surfaces of building elements exposed to the outdoors (expressed  $q_{o,t}$  and  $q_{i,t}$  respectively) can be calculated as follows:

$$q_{o,t} = \sum_{j=0}^{\infty} T_{o,t-j} X_j - \sum_{j=0}^{\infty} T_{i,t-j} Y_j \quad (14a)$$

$$q_{i,t} = \sum_{j=0}^{\infty} T_{o,t-j} Y_j - \sum_{j=0}^{\infty} T_{i,t-j} Z_j \quad (14b)$$

In these expressions,  $T_{o,t-j}$  and  $T_{i,t-j}$  are outdoor and indoor temperatures [F] (or outside surface and inside surface temperatures depending upon the heat conduction system) at time  $t-j$  hr. The response factors are three sets of numbers expressed as  $X_j$ ,  $Y_j$ , and  $Z_j$  (for  $j = 1, 2, \infty$ ) in above equations and have units of Btu/(hr · ft<sup>2</sup> · F), the same as the unit for overall heat transfer coefficient  $U$ . Application of the response factor relations to a steady state heat conduction situation where

$$q_{o,t} = q_{i,t} = U(T_o - T_i)$$

$$T_o = T_{o,t} \text{ for all } t$$

$$T_i = T_{i,t} \text{ for all } t,$$

would result in:

$$\sum_{j=0}^{\infty} X_j = \sum_{j=0}^{\infty} Y_j = \sum_{j=0}^{\infty} Z_j = U \quad (15)$$

### Wall Response Factors

The tabulation at the end of this section illustrates response factors *calculated* for a typical wall. In this particular wall, the response factors for  $j > 28$  can be obtained by a geometric progression using the common ratio  $R$  such that:

$$(X_{j+1}/X_j) = (Y_{j+1}/Y_j) = (Z_{j+1}/Z_j) = R$$

In typical wall heat transfer calculations, the summation terms in Eq 14A and 14B may be truncated at  $j = 48$ . In other words, if the value of heat flux at time  $t$  is needed, it is necessary to have the hourly temperature history covering the previous 48-hr period as well as the values of  $X_j$ ,  $Y_j$ , and  $Z_j$  for  $j = 0, 2, \dots, 47$ . By making use of the hourly heat flux history in addition to the temperature history, the maximum number of  $j$  could be decreased considerably. This aspect is discussed in detail in Chapter 2. The temperature and heat flux data need not be steady or steady periodic at all.

Unlike the overall heat transfer coefficient, or  $U$ -value, calculation of the response factor requires complex mathematical treatment. Computer programs are available at both the National Research Council of Canada and the National Bureau of Standards to calculate response factors from known data, such as the number of composite layers, and for each layer, the thermal conductivity, thermal diffusivity, and thickness. (In the case of an air cavity or air space, only the thermal resistance value is required.) The NBS program can also be used to calculate response factors for constructions of cylindrical and spherical shape.

As is the case when applying  $U$ -values, many building elements are so constructed that parallel heat paths of different thermal characteristics result. If there is appreciable lateral heat transfer between paths, for example, when metal skins are used, theoretical calculation of response factors is not yet possible. For such constructions, experimental determination of transient heat transfer characteristics is necessary to determine the response factors. ASHRAE currently is sponsoring experimental research (RP-102).

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Tabulation of Illustrative Wall Response Factors

Thickness l l (ft)	Thermal Conduc- tivity k (ft Btu/(hr · ft <sup>2</sup> · F)	Density ρ (lb/ft <sup>3</sup> )	Specific Heat c (ft Btu/(lb · F))	Resistance of Air Layer Res (l) (hr · ft <sup>2</sup> · F) /Btu	Wall Composition
1				0.3333	Outside surface
2	0.3333	0.77	125	0.22	4-in. face brick
3				0.842	0.75-in. air space
4	0.1667	0.025	5.7	0.3	2-in. insulation
5	0.0313	0.24	78	0.26	0.375-in. gypsum bd
6	0.042	0.27	90	0.2	0.50-in. plaster
7				0.833	Inside surface

Overall heat transfer coefficient  $U = 0.1060$  Btu/(hr · ft<sup>2</sup> · F)

i	X	Y	Z
0	1.9828631184	0.0000694414	0.7658454069
1	-0.5332548902	0.0032610373	-0.3626101180
2	-0.2897180964	0.0108381158	-0.1594774346
3	-0.2226418777	0.0143821960	-0.0722106733
4	-0.1751782415	0.0141359305	-0.0330527494
5	-0.1381393441	0.0124128118	-0.0153907015
6	-0.1089916981	0.0103599746	-0.0073676305
7	-0.0860172059	0.0084293880	-0.0036792673
8	-0.0678956034	0.0067667191	-0.0019496245
9	-0.0535962455	0.0053921814	-0.0011124022
10	-0.0423104538	0.0042793546	-0.0006875056
11	-0.0334020144	0.0033884423	-0.0004575496
12	-0.0263696421	0.0026795634	-0.0003231437
13	-0.0208180261	0.0021174509	-0.0002380978
14	-0.0164352751	0.0016725725	-0.0001803688
15	-0.0129752460	0.0013208578	-0.0001389992
16	-0.0102436541	0.0010429664	-0.0001082184
17	-0.0080871331	0.0008234788	-0.0000847576
18	-0.0063846118	0.0006501542	-0.0000666111
19	-0.0050405105	0.0005132985	-0.0000524525
20	-0.0039793727	0.0004052451	-0.0000413496
21	-0.0031416279	0.0003199354	-0.0000326175
22	-0.0024802469	0.0002525834	-0.0000257387
23	-0.0019581009	0.0001994098	-0.0000203148
24	-0.0015458781	0.0001574300	-0.0000160357
25	-0.0012204372	0.0001242877	-0.0000126587
26	-0.0009635087	0.0000981225	-0.0000099933
27	-0.0007606692	0.0000774656	-0.0000078893
28	-0.0006005318	0.0000611574	-0.0000062283

$$\text{Common ratio for } \frac{X_{j+1}}{X_j} = \frac{Y_{j+1}}{Y_j} = \frac{Z_{j+1}}{Z_j} = R \text{ for } j > 28.$$

$$R = 0.78947824)^4.$$

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**Table 1 Surface Conductances and Resistances for Air**

All conductance values expressed in Btu/(hr·ft<sup>2</sup>·F).

A surface cannot take credit for both an air space resistance value and a surface resistance value. No credit for an air space value can be taken for any surface facing an air space of less than 0.5 in.

SECTION A. Surface Conductances and Resistances <sup>a,b,d</sup>							SECTION B. Reflectivity and Emittance Values of Various Surfaces <sup>c</sup> and Effective Emittances of Air Spaces					
Position of Surface	Direction of Heat Flow	Surface Emittance						Surface	Reflectivity in Percent	Average Emittance $\epsilon$	Effective Emittance $E$ of Air Space	
		Non-reflective $\epsilon = 0.90$	Reflective $\epsilon = 0.20$		Reflective $\epsilon = 0.05$		One surface emittance $\epsilon$ ; the other 0.90				Both surfaces emittances $\epsilon$	
			$h_1$	R	$h_1$	R						
STILL AIR												
Horizontal . . . . .	Upward	1.63	0.61	0.91	1.10	0.76	1.32	Aluminum foil, bright . . . . .	92 to 97	0.05	0.05	0.03
Sloping—45 deg . . . . .	Upward	1.60	0.62	0.88	1.14	0.73	1.37	Aluminum sheet . . . . .	80 to 95	0.12	0.12	0.06
Vertical . . . . .	Horizontal	1.46	0.68	0.74	1.35	0.59	1.70	Aluminum coated paper, polished . . . . .	75 to 84	0.20	0.20	0.11
Sloping—45 deg . . . . .	Downward	1.32	0.76	0.60	1.67	0.45	2.22	Steel, galvanized, bright. . .	70 to 80	0.25	0.24	0.15
Horizontal . . . . .	Downward	1.08	0.92	0.37	2.70	0.22	4.55	Aluminum paint . . . . .	30 to 70	0.50	0.47	0.35
MOVING AIR												
(Any Position)		$h_0$	R	$h_0$	R	$h_0$	R	Building materials: wood, paper, masonry, nonmetallic paints . . . . .	5 to 15	0.90	0.82	0.82
15-mph Wind . . . . .	Any	6.00	0.17					Regular glass . . . . .	5 to 15	0.84	0.77	0.72
(for winter)												
7.5-mph Wind . . . . .	Any	4.00	0.25									
(for summer)												

<sup>a</sup>For ventilated attics or spaces above ceilings under summer conditions (heat flow down) see Table 6.

<sup>b</sup>Conductances are for surfaces of the stated emittance facing virtual blackbody surroundings at the same temperature as the ambient air. Values are based on a surface-air temperature difference of 10 deg F and for surface temperature of 70 F.

<sup>c</sup>See also Chapter 2, Table 4.

<sup>d</sup>See Fig. 1 for additional data.



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Position of Air Space	Direction of Heat Flow	Air Space		0.5-in. Air Space <sup>d</sup>					0.75-in. Air Space <sup>d</sup>				
		Mean Temp., <sup>b</sup> (F)	Temp Diff., <sup>b</sup> (deg F)	Value of $E^{b,c}$					Value of $E^{b,c}$				
				0.03	0.05	0.2	0.5	0.82	0.03	0.05	0.2	0.5	0.82
Horiz.	Up	90	10	2.13	2.03	1.51	0.99	0.73	2.34	2.22	1.61	1.04	0.75
		50	30	1.62	1.57	1.29	0.96	0.75	1.71	1.66	1.35	0.99	0.77
		50	10	2.13	2.05	1.60	1.11	0.84	2.30	2.21	1.70	1.16	0.87
		0	20	1.73	1.70	1.45	1.12	0.91	1.83	1.79	1.52	1.16	0.93
		0	10	2.10	2.04	1.70	1.27	1.00	2.23	2.16	1.78	1.31	1.02
		-50	20	1.69	1.66	1.49	1.23	1.04	1.77	1.74	1.55	1.27	1.07
		-50	10	2.04	2.00	1.75	1.40	1.16	2.16	2.11	1.84	1.46	1.20
45° Slope	Up	90	10	2.44	2.31	1.65	1.06	0.76	2.96	2.78	1.88	1.15	0.81
		50	30	2.06	1.98	1.56	1.10	0.83	1.99	1.92	1.52	1.08	0.82
		50	10	2.55	2.44	1.83	1.22	0.90	2.90	2.75	2.00	1.29	0.94
		0	20	2.20	2.14	1.76	1.30	1.02	2.13	2.07	1.72	1.28	1.00
		0	10	2.63	2.54	2.03	1.44	1.10	2.72	2.62	2.08	1.47	1.12
		-50	20	2.08	2.04	1.78	1.42	1.17	2.05	2.01	1.76	1.41	1.16
		-50	10	2.62	2.56	2.17	1.66	1.33	2.53	2.47	2.10	1.62	1.30
Vertical	Horiz.	90	10	2.47	2.34	1.67	1.06	0.77	3.50	3.24	2.08	1.22	0.84
		50	30	2.57	2.46	1.84	1.23	0.90	2.91	2.77	2.01	1.30	0.94
		50	10	2.66	2.54	1.88	1.24	0.91	3.70	3.46	2.35	1.43	1.01
		0	20	2.82	2.72	2.14	1.50	1.13	3.14	3.02	2.32	1.58	1.18
		0	10	2.93	2.82	2.20	1.53	1.15	3.77	3.59	2.64	1.73	1.26
		-50	20	2.90	2.82	2.35	1.76	1.39	2.90	2.83	2.36	1.77	1.39
		-50	10	3.20	3.10	2.54	1.87	1.46	3.72	3.60	2.87	2.04	1.56
45° Slope	Down	90	10	2.48	2.34	1.67	1.06	0.77	3.53	3.27	2.10	1.22	0.84
		50	30	2.64	2.52	1.87	1.24	0.91	3.43	3.23	2.24	1.39	0.99
		50	10	2.67	2.55	1.89	1.25	0.92	3.81	3.57	2.40	1.45	1.02
		0	20	2.91	2.80	2.19	1.52	1.15	3.75	3.57	2.63	1.72	1.26
		0	10	2.94	2.83	2.21	1.53	1.15	4.12	3.91	2.81	1.80	1.30
		-50	20	3.16	3.07	2.52	1.86	1.45	3.78	3.65	2.90	2.05	1.57
		-50	10	3.26	3.16	2.58	1.89	1.47	4.35	4.18	3.22	2.21	

Table 2 Thermal Resistances of Plane<sup>a</sup> Air Spaces<sup>d,e\*</sup>

Position of Air Space	Direction of Heat Flow	Air Space		1.5-in. Air Space <sup>d</sup>					3.5-in. Air Space <sup>d</sup>				
		Mean Temp. <sup>b</sup> (F)	Temp Diff. <sup>b</sup> (deg F)	Value of $E^{b,c}$					Value of $E^{b,c}$				
				0.03	0.05	0.2	0.5	0.82	0.03	0.05	0.2	0.5	0.82
Horiz	Up	90	10	2.55	2.41	1.71	1.08	0.77	2.84	2.66	1.83	1.13	0.80
		50	30	1.87	1.81	1.45	1.04	0.80	2.09	2.01	1.58	1.10	0.84
		50	10	2.50	2.40	1.81	1.21	0.89	2.80	2.66	1.95	1.28	0.93
		0	20	2.01	1.95	1.63	1.23	0.97	2.25	2.18	1.79	1.32	1.03
		0	10	2.43	2.35	1.90	1.38	1.06	2.71	2.62	2.07	1.47	1.12
		-50	20	1.94	1.91	1.68	1.36	1.13	2.19	2.14	1.86	1.47	1.20
		-50	10	2.37	2.31	1.99	1.55	1.26	2.65	2.58	2.18	1.67	1.33
45° Slope	Up	90	10	2.92	2.73	1.86	1.14	0.80	3.18	2.96	1.97	1.18	0.82
		50	30	2.14	2.06	1.61	1.12	0.84	2.26	2.17	1.67	1.15	0.86
		50	10	2.88	2.74	1.99	1.29	0.94	3.12	2.95	2.10	1.34	0.96
		0	20	2.30	2.23	1.82	1.34	1.04	2.42	2.35	1.90	1.38	1.06
		0	10	2.79	2.69	2.12	1.49	1.13	2.98	2.87	2.23	1.54	1.16
		-50	20	2.22	2.17	1.88	1.49	1.21	2.34	2.29	1.97	1.54	1.25
		-50	10	2.71	2.64	2.23	1.69	1.35	2.87	2.79	2.33	1.75	1.39
Vertical	Horiz.	90	10	3.99	3.66	2.25	1.27	0.87	3.69	3.40	2.15	1.24	0.85
		50	30	2.58	2.46	1.84	1.23	0.90	2.67	2.55	1.89	1.25	0.91
		50	10	3.79	3.55	2.39	1.45	1.02	3.63	3.40	2.32	1.42	1.01
		0	20	2.76	2.66	2.10	1.48	1.12	2.88	2.78	2.17	1.51	1.14
		0	10	3.51	3.35	2.51	1.67	1.23	3.49	3.33	2.50	1.67	1.23
		-50	20	2.64	2.58	2.18	1.66	1.33	2.82	2.75	2.30	1.73	1.37
		-50	10	3.31	3.21	2.62	1.91	1.48	3.40	3.30	2.67	1.94	1.50
45° Slope	Down	90	10	5.07	4.55	2.56	1.36	0.91	4.81	4.33	2.49	1.34	0.90
		50	30	3.58	3.36	2.31	1.42	1.00	3.51	3.30	2.28	1.40	1.00
		50	10	5.10	4.66	2.85	1.60	1.09	4.74	4.36	2.73	1.57	1.08
		0	20	3.85	3.66	2.68	1.74	1.27	3.81	3.63	2.66	1.74	1.27
		0	10	4.92	4.62	3.16	1.94	1.37	4.59	4.32	3.02	1.88	1.34
		-50	20	3.62	3.50	2.80	2.01	1.54	3.77	3.64	2.90	2.05	1.57
		-50	10	4.67	4.47	3.40	2.29	1.70	4.50	4.32	3.31	2.25	1.68
Horiz.	Down	90	10	6.09	5.35	2.79	1.43	0.94	10.07	8.19	3.41	1.57	1.00
		50	30	6.27	5.63	3.18	1.70	1.14	9.60	8.17	3.86	1.88	1.22
		50	10	6.61	5.90	3.27	1.73	1.15	11.15	9.27	4.09	1.93	1.24
		0	20	7.03	6.43	3.91	2.19	1.49	10.90	9.52	4.87	2.47	1.62
		0	10	7.31	6.66	4.00	2.22	1.51	11.97	10.32	5.08	2.52	1.64
		-50	20	7.73	7.20	4.77	2.85	1.99	11.64	10.49	6.02	3.25	2.18
		-50	10	8.09	7.52	4.91	2.89	2.01	12.98	11.56	6.36	3.34	2.22

<sup>a</sup>See Chapter 20, section on Factors Affecting Heat Transfer across Air Spaces.

<sup>b</sup>Interpolation is permissible for other values of mean temperature, temperature differences, and effective emittance  $E$ . Interpolation and moderate extrapolation for air spaces greater than 3.5 in. are also permissible.

<sup>c</sup>Effective emittance of the space  $E$  is given by  $1/E = 1/e_1 + 1/e_2 - 1$ , where  $e_1$  and  $e_2$  are the emittances of the surfaces of the air space (See section B of Table 1.)

<sup>d</sup>Credit for an air space resistance value cannot be taken more than once and only for the boundary conditions established.

<sup>e</sup>Resistances of horizontal spaces with heat flow downward are substantially independent of temperature difference.

<sup>f</sup>Thermal resistance values were determined from the relation  $R = 1/C$ , where  $C = h_c + Eh_r$ ,  $h_c$  is the conduction-convection coefficient,  $Eh_r$  is the radiation coefficient  $\approx 0.00686 E [(460 + t_m)/100]^3$ , and  $t_m$  is the mean temperature of the air space. For interpretation from Table 2 to air space thicknesses less than 0.5 in. (as in insulating window glass), assume  $h_c = 0.795 (1 + 0.0016)$  and compute  $R$ -values from the above relations for an air space thickness of 0.2 in.

\*Based on National Bureau of Standards data presented in Housing Research Paper No. 32, Housing and Home Finance Agency 1954, U. S. Government Printing Office, Washington 20402.

Table 3A Thermal Properties of Typical Building and Insulating Materials—(Design Values)<sup>a</sup>

(For Industrial Insulation Design Values, see Table 3B). These constants are expressed in Btu per (hour) (square foot) (degree Fahrenheit temperature difference). Conductivities ( $k$ ) are per inch thickness, and conductances ( $C$ ) are for thickness or construction stated, not per inch thickness. All values are for a mean temperature of 75 F, except as noted by an asterisk (\*) which have been reported at 45 F. The SI units for Resistance (last two columns) were calculated by taking the values from the two Resistance columns under Customary Unit, and multiplying by the factor  $1/k$  (r/in.) and  $1/C$  (R) for the appropriate conversion factor in Table 18.

Description	Customary Unit					SI Unit		
	Density (lb/ft <sup>3</sup> )	Conduc- tivity ( <i>k</i> )	Conduc- tance ( <i>C</i> )	Resistance <sup>b</sup> ( <i>R</i> )		Specific Heat, Btu/(lb) (deg F)	Resistance <sup>b</sup> ( <i>R</i> )	
				Per inch thickness (1/ <i>k</i> )	For thick- ness listed (1/ <i>C</i> )		(m · K) W	(m <sup>2</sup> · K) W
<b>BUILDING BOARD</b>								
<b>Boards, Panels, Subflooring, Sheathing</b>								
<b>Woodboard Panel Products</b>								
Asbestos-cement board	120	4.0	—	0.25	—	0.24	1.73	
Asbestos-cement board . . . . . 0.125 in.	120	—	33.00	—	0.03			0.005
Asbestos-cement board . . . . . 0.25 in.	120	—	16.50	—	0.06			0.01
Gypsum or plaster board . . . . . 0.375 in.	50	—	3.10	—	0.32	0.26		0.06
Gypsum or plaster board . . . . . 0.5 in.	50	—	2.22	—	0.45			0.08
Gypsum or plaster board . . . . . 0.625 in.	50	—	1.78	—	0.56			0.10
Plywood (Douglas Fir) . . . . .	34	0.80	—	1.25	—	0.29	8.66	
Plywood (Douglas Fir) . . . . . 0.25 in.	34	—	3.20	—	0.31			0.05
Plywood (Douglas Fir) . . . . . 0.375 in.	34	—	2.13	—	0.47			0.08
Plywood (Douglas Fir) . . . . . 0.5 in.	34	—	1.60	—	0.62			0.11
Plywood (Douglas Fir) . . . . . 0.625 in.	34	—	1.29	—	0.77			0.19



Table 3A Thermal Properties of Typical Building and Insulating Materials—(Design Values)<sup>a</sup>

Description	Customary Unit					SI Unit		
	Density (lb/ft <sup>3</sup> )	Conduc- tivity (k)	Conduc- tance (C)	Resistance <sup>b</sup> (R)		Specific Heat, Btu/(lb) (deg F)	Resistance <sup>b</sup> (R)	
				Per inch thickness (1/k)	For thick- ness listed (1/C)		(m·K) W	(m <sup>2</sup> ·K) W
Plywood or wood panels. . . . . 0.75 in.	34	—	1.07	—	0.93	0.29		0.16
Vegetable Fiber Board								
Sheathing, regular density. . . . . 0.5 in.	18	—	0.76	—	1.32	0.31		0.23
. . . . . 0.78125 in.	18	—	0.49	—	2.06			0.36
Sheathing intermediate density . . . . . 0.5 in.	22	—	0.82	—	1.22	0.31		0.21
Nail-base sheathing. . . . . 0.5 in.	25	—	0.88	—	1.14	0.31		0.20
Shingle backer. . . . . 0.375 in.	18	—	1.06	—	0.94	0.31		0.17
Shingle backer . . . . . 0.3125 in.	18	—	1.28	—	0.78			0.14
Sound deadening board . . . . . 0.5 in.	15	—	0.74	—	1.35	0.30		0.24
Tile and lay-in panels, plain or acoustic . . . . .	18	0.40	—	2.50	—	0.14	17.33	
. . . . . 0.5 in.	18	—	0.80	—	1.25			0.22
. . . . . 0.75 in.	18	—	0.53	—	1.89			0.33
Laminated paperboard . . . . .	30	0.50	—	2.00	—	0.33	13.86	
Homogeneous board from recycled paper . . . . .	30	0.50	—	2.00	—	0.28	13.86	
Hardboard								
Medium density . . . . .	50	0.73	—	1.37	—	0.31	9.49	
High density, service temp. service underlay . . . . .	55	0.82	—	1.22	—	0.32	8.46	
High density, std. tempered . . . . .	63	1.00	—	1.00	—	0.32	6.93	
Particleboard								
Low density . . . . .	37	0.54	—	1.85	—	0.31	12.82	
Medium density . . . . .	50	0.94	—	1.06	—	0.31	7.35	
High density . . . . .	62.5	1.18	—	0.85	—	0.31	5.89	
Underlayment . . . . . 0.625 in.	40	—	1.22	—	0.82	0.29		0.14
Wood subfloor. . . . . 0.75 in.		—	1.06	—	0.94	0.33		0.17
<b>BUILDING MEMBRANE</b>								
Vapor—permeable felt. . . . .	—	—	16.70	—	0.06			0.01
Vapor—seal, 2 layers of mopped 15-lb felt . . . . .	—	—	8.35	—	0.12			0.02
Vapor—seal, plastic film . . . . .	—	—	—	—	Negl.			
<b>FINISH FLOORING MATERIALS</b>								
Carpet and fibrous pad . . . . .	—	—	0.48	—	2.08	0.34		0.37
Carpet and rubber pad . . . . .	—	—	0.81	—	1.23	0.33		0.22
Cork tile . . . . . 0.125 in.	—	—	3.60	—	0.28	0.48		0.05
Terrazzo . . . . . 1 in.	—	—	12.50	—	0.08	0.19		0.01
Tile—asphalt, linoleum, vinyl, rubber vinyl asbestos . . . . .	—	—	20.00	—	0.05	0.30		0.01
ceramic . . . . .						0.24		
. . . . .						0.19		
Wood, hardwood finish . . . . . 0.75 in.			1.47		0.68			0.12
<b>INSULATING MATERIALS</b>								
<b>BLANKET AND BATT</b>								
Mineral Fiber, fibrous form processed from rock, slag, or glass								
approx. <sup>c</sup> 2–2.75 in. . . . .	0.3–2.0	—	0.143	—	7 <sup>d</sup>	0.17–0.23		1.23
approx. <sup>c</sup> 3–3.5 in. . . . .	0.3–2.0	—	0.091	—	11 <sup>d</sup>			1.94
approx. <sup>c</sup> 5.50–6.5 . . . . .	0.3–2.0	—	0.053	—	19 <sup>d</sup>			3.35
approx. <sup>c</sup> 6–7 in. . . . .	0.3–2.0	—	0.045	—	22 <sup>d</sup>			3.87
approx. <sup>d</sup> 8.5 in. . . . .	0.3–2.0	—	0.033	—	30 <sup>d</sup>			5.28
<b>BOARD AND SLABS</b>								
Cellular glass . . . . .	8.5	0.38	—	2.63	—	0.24	18.23	
Glass fiber, organic bonded . . . . .	4–9	0.25	—	4.00	—	0.23	27.72	
Expanded rubber (rigid). . . . .	4.5	0.22	—	4.55	—	0.40	31.53	
Expanded polystyrene extruded Cut cell surface. . . . .	1.8	0.25	—	4.00	—	0.29	27.72	
Expanded polystyrene extruded Smooth skin surface . . . . .	2.2	0.20	—	5.00	—	0.29	34.65	
Expanded polystyrene extruded Smooth skin surface . . . . .	3.5	0.19	—	5.26	—		36.45	
Expanded polystyrene, molded beads. . . . .	1.0	0.28	—	3.57	—	0.29	24.74	
Expanded polyurethane <sup>f</sup> (R-11 exp.) . . . . .	1.5	0.16	—	6.25	—	0.38	43.82	
(Thickness 1 in. or greater) . . . . .	2.5							

Table 3A Thermal Properties of Typical Building and Insulating Materials—(Design Values)<sup>a</sup>

Description	Density (lb/ft <sup>3</sup> )	Conduc- tivity (k)	Conduc- tance (C)	Customary Unit		Specific Heat, Btu/(lb) (deg F)	SI Unit	
				Resistance <sup>b</sup> (R)			Resistance <sup>b</sup> (R)	
				Per inch thickness (1/k)	For thick- ness listed (1/C)		(m · K) W	(m <sup>2</sup> · K) W
Mineral fiber with resin binder . . . . .	15	0.29	—	3.45	—	0.17	23.91	
Mineral fiberboard, wet felted								
Core or roof insulation . . . . .	16-17	0.34	—	2.94	—		20.38	
Acoustical tile . . . . .	18	0.35	—	2.86	—	0.19	19.82	
Acoustical tile . . . . .	21	0.37	—	2.70	—		18.71	
Mineral fiberboard, wet molded								
Acoustical tiles . . . . .	23	0.42	—	2.38	—	0.14	16.49	
Wood or cane fiberboard								
Acoustical tiles . . . . . 0.5 in.	—	—	0.80	—	1.25	0.31		0.22
Acoustical tiles . . . . . 0.75 in.	—	—	0.53	—	1.89			0.33
Interior finish (plank, tile) . . . . .	15	0.35	—	2.86	—	0.32	19.82	
Wood shredded (cemented in preformed slabs) . . . . .	22	0.60	—	1.67	—	0.31	11.57	
<b>LOOSE FILL</b>								
Cellulosic insulation (milled paper or wood pulp) . . . . .	2.3-3.2	0.27-0.32	—	3.13-3.70	—	0.33	21.69-25.64	
Sawdust or shavings . . . . .	8.0-15.0	0.45	—	2.22	—	0.33	15.39	
Wood fiber, softwoods . . . . .	2.0-3.5	0.30	—	3.33	—	0.33	23.08	
Perlite, expanded . . . . .	5.0-8.0	0.37	—	2.70	—	0.26	18.71	
Mineral fiber (rock, slag or glass)								
approx. c 3.75-5 in. . . . .	0.6-2.0	—	—		11	0.17		1.94
approx. c 6.5-8.75 in. . . . .	0.6-2.0	—	—		19			3.35
approx. c 7.5-10 in. . . . .	0.6-2.0	—	—		22			3.87
approx. c 10.25-13.75 in. . . . .	0.6-2.0	—	—		30			5.28
Vermiculite, exfoliated . . . . .	7.0-8.2	0.47	—	2.13	—	3.20	14.76	
	4.0-6.0	0.44	—	2.27	—		15.73	
<b>ROOF INSULATION<sup>b</sup></b>								
Preformed, for use above deck								
Different roof insulations are available in different thicknesses to provide the design C values listed. <sup>h</sup> Consult individual manufacturers for actual thickness of their material. . . . .			0.72 to 0.12		1.39 to 8.33		— —	0.24 to 1.47
<b>MASONRY MATERIALS</b>								
<b>CONCRETES</b>								
Cement mortar . . . . .	116	5.0	—	0.20	—		1.39	
Gypsum-fiber concrete 87.5% gypsum, 12.5% wood chips . . . . .	51	1.66	—	0.60	—	0.21	4.16	
Lightweight aggregates including ex- panded shale, clay or slate; expanded slags; cinders; pumice; vermiculite; also cellular concretes . . . . .	120 100 80 60 40 30 20	5.2 3.6 2.5 1.7 1.15 0.90 0.70	— — — — — — —	0.19 0.28 0.40 0.59 0.86 1.11 1.43	— — — — — — —		1.32 1.94 2.77 4.09 5.96 7.69 9.91	
Perlite, expanded . . . . .	40 30 20	0.93 0.71 0.50	— — —	1.08 1.41 2.00	— — —	0.32	7.48 9.77 13.86	
Sand and gravel or stone aggregate (oven dried) . . . . .	140	9.0	—	0.11	—	0.22	0.76	
Sand and gravel or stone aggregate (not dried) . . . . .	140	12.0	—	0.08	—		0.55	
Stucco . . . . .	116	5.0	—	0.20	—		1.39	
<b>MASONRY UNITS</b>								
Brick, common <sup>i</sup> . . . . .	120	5.0	—	0.20	—	0.19	1.39	
Brick, face <sup>i</sup> . . . . .	130	9.0	—	0.11	—		0.76	
Clay tile, hollow:								
1 cell deep . . . . . 3 in.	—	—	1.25	—	0.80	0.21		0.14
1 cell deep . . . . . 4 in.	—	—	0.90	—	1.11			0.20
2 cells deep . . . . . 6 in.	—	—	0.66	—	1.52			0.27
2 cells deep . . . . . 8 in.	—	—	0.54	—	1.85			0.33
2 cells deep . . . . . 10 in.	—	—	0.45	—	2.22			0.39
3 cells deep . . . . . 12 in.	—	—	0.40	—	2.50			0.44

### Description

Description	Density (lb/ft <sup>3</sup> )	Conduc- tivity (k)	Conduc- tance (C)	Customary Unit		Specific Heat, Btu/(lb) (deg F)	SI Unit	
				Resistance <sup>b</sup> (R)			Resistance <sup>b</sup> (R)	
				Per inch thickness (1/k)	For thick- ness listed (1/C)		(m · K) W	(m <sup>2</sup> · K) W
Concrete blocks, three oval core: Sand and gravel aggregate . . . . . 4 in.	—	—	1.40	—	0.71	0.22		0.13

Table 3A Thermal Properties of Typical Building and Insulating Materials—(Design Values)\*

Description	Customary Unit						SI Unit	
	Density (lb/ft <sup>3</sup> )	Conduc- tivity (k)	Conduc- tance (C)	Resistance <sup>b</sup> (R)		Specific Heat, Btu/(lb) (deg F)	Resistance <sup>b</sup> (R)	
				Per inch thickness (1/k)	For thick- ness listed (1/C)		(m·K) W	(m <sup>2</sup> ·K) W
Aluminum or Steel <sup>m</sup> , over sheathing								
Hollow-backed . . . . .	—	—	1.61	—	0.61	0.29		0.11
Insulating-board backed nominal								
0.375 in. . . . .	—	—	0.55	—	1.82	0.32		0.32
Insulating-board backed nominal								
0.375 in., foil backed . . . . .	—	—	0.34	—	2.96			0.52
Architectural glass . . . . .	—	—	10.00	—	0.10	0.20		0.02
<b>WOODS</b>								
Maple, oak, and similar hardwoods . . . . .	45	1.10	—	0.91	—	0.30	6.31	
Fir, pine, and similar softwoods . . . . .	32	0.80	—	1.25	—	0.33	8.66	
Fir, pine, and similar softwoods . . . . . 0.75 in.	32	—	1.06	—	0.94	0.33		0.17
. . . . . 1.5 in.	—	—	0.53	—	1.89			0.33
. . . . . 2.5 in.	—	—	0.32	—	3.12			0.60
. . . . . 3.5 in.	—	—	0.23	—	4.35			0.75

## Notes for Table 3A

\*Representative values for dry materials were selected by ASHRAE TC4.4, Insulation and Moisture Barriers. They are intended as design (not specification) values for materials in normal use. For properties of a particular product, use the value supplied by the manufacturer or by unbiased tests.

<sup>b</sup>Resistance values are the reciprocals of C before rounding off C to two decimal places.

<sup>c</sup>Also see Insulating Materials, Board.

<sup>d</sup>Does not include paper backing and facing, if any. Where insulation forms a boundary (reflective or otherwise) of an air space, see Tables 1 and 2 for the insulating value of air space for the appropriate effective emittance and temperature conditions of the space.

<sup>e</sup>Conductivity varies with fiber diameter. (See Chapter 20, Thermal Conductivity section, and Fig. 1.) Insulation is produced by different densities; therefore, there is a wide variation in thickness for the same R-value among manufacturers. No effort should be made to relate any specific R-value to any specific thickness. Commercial thicknesses generally available range from 2 to 8.5.

<sup>f</sup>Values are for aged board stock. For change in conductivity with age of expanded urethane, see Chapter 19, Factors Affecting Thermal Conductivity.

<sup>g</sup>Insulating values of acoustical tile vary, depending on density of the board and on type, size, and depth of perforations.

<sup>h</sup>The U. S. Department of Commerce, *Simplified Practice Recommendation for Thermal Conductance Factors for Preformed Above-Deck Roof Insulation*, No. R 257-55, recognizes the specification of roof insulation on the basis of the C-values shown. Roof insulation is made in thicknesses to meet these values.

<sup>i</sup>Face brick and common brick do not always have these specific densities. When density is different from that shown, there will be a change in thermal conductivity.

<sup>j</sup>Data on rectangular core concrete blocks differ from the above data on oval core blocks, due to core configuration, different mean temperatures, and possibly differences in unit weights. Weight data on the oval core blocks tested are not available.

<sup>k</sup>Weights of units approximately 7.625 in. high and 15.75 in. long. These weights are given as a means of describing the blocks tested, but conductance values are all for 1 ft<sup>2</sup> of area.

<sup>l</sup>Vermiculite, perlite, or mineral wool insulation. Where insulation is used, vapor barriers or other precautions must be considered to keep insulation dry.

<sup>m</sup>Values for metal siding applied over flat surfaces vary widely, depending on amount of ventilation of air space beneath the siding; whether air space is reflective or nonreflective; and on thickness, type, and application of insulating backing-board used. Values given are averages for use as design guides, and were obtained from several guarded hotbox tests (ASTM C236) or calibrated hotbox (BSS 77) on hollow-backed types and types made using backing-boards of wood fiber, foamed plastic, and glass fiber. Departures of  $\pm 50\%$  or more from the values given may occur.

Table 3B Thermal Conductivity (k) of Industrial Insulation (Design Values)\* (For Mean Temperatures Indicated)

Expressed in Btu per (hour)(square foot)(degree Fahrenheit temperature difference per in.)

Expressed in Btu per (hour)(square foot)(degree Fahrenheit temperature difference per inch)																	
Form	Material Composition	Accepted Max Temp for Use, $F^{\circ}$	Typical Density (lb/ft <sup>3</sup> )	Typical Conductivity $k$ at Mean Temp $F^{\circ}$													
				-100	-75	-50	-25	0	25	50	75	100	200	300	500	700	900
<b>BLANKETS &amp; FELTS</b>																	
<b>MINERAL FIBER</b>																	
(Rock, slag or glass)																	
Blanket, metal reinforced		1200	6-12										0.26	0.32	0.39	0.54	
		1000	2.5-6										0.24	0.31	0.40	0.61	
Mineral fiber, glass		350	0.65 0.75 1.0 1.5 2.0 3.0				0.25	0.26	0.28	0.30	0.33	0.36	0.53				
Blanket, flexible, fine-fiber							0.24	0.25	0.27	0.29	0.32	0.34	0.48				
organic bonded							0.23	0.24	0.25	0.27	0.29	0.32	0.43				
							0.21	0.22	0.23	0.25	0.27	0.28	0.37				
							0.20	0.21	0.22	0.23	0.25	0.26	0.33				
							0.19	0.20	0.21	0.22	0.23	0.24	0.31				
Blanket, flexible, textile-fiber		350	0.65 0.75 1.0 1.5 3.0				0.27	0.28	0.29	0.30	0.31	0.32	0.50	0.68			
organic bonded							0.26	0.27	0.28	0.29	0.31	0.32	0.48	0.66			
							0.24	0.25	0.26	0.27	0.29	0.31	0.45	0.60			
							0.22	0.23	0.24	0.25	0.27	0.29	0.39	0.51			
							0.20	0.21	0.22	0.23	0.24	0.25	0.32	0.41			
Felt, semirigid organic bonded		400	3-8						0.24	0.25	0.26	0.27	0.35	0.44			
		850	3	0.16	0.17	0.18	0.19	0.20	0.21	0.22	0.23	0.24	0.35	0.55			
Laminated & felted		1200	7.5											0.35	0.45	0.60	
Without binder																	
<b>VEGETABLE &amp; ANIMAL FIBER</b>																	
Hair Felt or Hair Felt plus Jute		180	10						0.26	0.28	0.29	0.30					

**Table 3B Thermal Conductivity (*k*) of Industrial Insulation (Design Values)\* (For Mean Temperatures Indicated)**

Expressed in Btu per (hour)(square foot)(degree Fahrenheit temperature difference per in.)

Form	Material Composition	Accepted Max Temp for Use, F*	Typical Density (lb/ft <sup>3</sup> )	Typical Conductivity <i>k</i> at Mean Temp <i>F</i>													
				-100	-75	-50	-25	0	25	50	75	100	200	300	500	700	900
<b>BLOCKS, BOARDS &amp; PIPE INSULATION</b>																	
<b>ASBESTOS</b>																	
	Laminated asbestos paper	700	30									0.40	0.45	0.50	0.60		
	Corrugated & laminated asbestos Paper																
	4-ply	300	11-13								0.54	0.57	0.68				
	6-ply	300	15-17								0.49	0.51	0.59				
	8-ply	300	18-20								0.47	0.49	0.57				
<b>MOLDED AMOSITE &amp; BINDER</b>																	
	85% MAGNESIA	1500	15-18								0.32	0.37	0.42	0.52	0.62	0.72	
<b>CALCIUM SILICATE</b>																	
		600	11-12								0.35	0.38	0.42				
		1200	11-13								0.38	0.41	0.44	0.52	0.62	0.72	
		1800	12-15											0.63	0.74	0.95	
<b>CELLULAR GLASS</b>																	
	DIATOMACEOUS SILICA	800	8.5			0.32	0.33	0.35	0.36	0.38	0.40	0.42	0.48	0.55			
		1600	21-22												0.64	0.68	0.72
		1900	23-25												0.70	0.75	0.80
<b>MINERAL FIBER</b>																	
	Glass,																
	Organic bonded, block and boards	400	3-10	0.16	0.17	0.18	0.19	0.20	0.22	0.24	0.25	0.26	0.33	0.40			
	Nonpinking binder	1000	3-10									0.26	0.31	0.38	0.52		
	Pipe insulation, slag or glass	350	3-4					0.20	0.21	0.22	0.23	0.24	0.29				
		500	3-10					0.20	0.22	0.24	0.25	0.26	0.33	0.40			
	Inorganic bonded-block	1000	10-15									0.33	0.38	0.45	0.55		
		1800	15-24									0.32	0.37	0.42	0.52	0.62	0.74
	Pipe insulation slag or glass	1000	10-15									0.33	0.38	0.45	0.55		
<b>MINERAL FIBER</b>																	
	Resin binder		15			0.23	0.24	0.25	0.26	0.28	0.29						
<b>RIGID POLYSTYRENE</b>																	
	Extruded, Refrigerant 12 exp	170	3.5	0.16	0.16	0.15	0.16	0.16	0.17	0.18	0.19	0.20					
	Extruded, Refrigerant 12 exp	170	2.2	0.16	0.16	0.17	0.16	0.17	0.18	0.19	0.20						
	Extruded	170	1.8	0.17	0.18	0.19	0.20	0.21	0.23	0.24	0.25	0.27					
	Molded beads	170	1	0.18	0.20	0.21	0.23	0.24	0.25	0.26	0.28						
<b>POLYURETHANE**</b>																	
	Refrigerant 11 exp	210	1.5-2.5	0.16	0.17	0.18	0.18	0.18	0.17	0.16	0.16	0.17					
<b>RUBBER, Rigid Foamed</b>																	
	VEGETABLE & ANIMAL FIBER	150	4.5						0.20	0.21	0.22	0.23					
	Wool felt (pipe insulation)	180	20						0.28	0.30	0.31	0.33					
<b>INSULATING CEMENTS</b>																	
<b>MINERAL FIBER</b>																	
	(Rock, slag, or glass)																
	With colloidal clay binder	1800	24-30									0.49	0.55	0.61	0.73	0.85	
	With hydraulic setting binder	1200	30-40									0.75	0.80	0.85	0.95		
<b>LOOSE FILL</b>																	
	Cellulose insulation (milled pulverized paper or wood pulp)		2.5-3							0.26	0.27	0.29					
	Mineral fiber, slag, rock or glass		2-5			0.19	0.21	0.23	0.25	0.26	0.28	0.31					
	Perlite (expanded)		5-8	0.25	0.27	0.29	0.30	0.32	0.34	0.35	0.37	0.39					
	Silica aerogel		7-6			0.13	0.14	0.15	0.15	0.16	0.17	0.18					
	Vermiculite (expanded)		7-8.2			0.39	0.40	0.42	0.44	0.45	0.47	0.49					
			4-6			0.34	0.35	0.38	0.40	0.42	0.44	0.46					

\*Representative values for dry materials as selected by ASHRAE TC 4.4, Insulation and Moisture Barriers. They are intended as design (not specification) values for materials of building construction for normal use. For thermal resistance of a particular product, use the value supplied by the manufacturer or by unbiased tests.

\*\*These temperatures are generally accepted as maximum. When operating temperature approaches these limits follow the manufacturer's recommendations.

\*\*Values are for aged board stock. For change in conductivity with age of refrigerant-blown expanded urethane see section on Thermal Conductivity, Chapter 19.

Note: Some polyurethane foams are formed by means which produce a stable product (with respect to *k*), but most are blown with refrigerant and will change with time.

**Table 4A Coefficients of Transmission (*U*) of Frame Walls\***

These coefficients are expressed in Btu per (hour) (square foot) (degree Fahrenheit) difference in temperature between the air on the two sides, and are based on an outside wind velocity of 15 mph

Replace Air Space with 3.5-in. R-11 Blanket Insulation (New Item 4)

Construction	Resistance ( <i>R</i> )			
	Between Framing	At Framing	Between Framing	At Framing
1. Outside surface (15 mph wind)	0.17	0.17	0.17	0.17
2. Siding, wood, 0.5 in. × 8 in. lapped (average)	0.81	0.81	0.81	0.81
3. Sheathing, 0.5-in. asphalt impregnated	1.32	1.32	1.32	1.32
4. Nonreflective air space, 3.5 in. (50 F mean; 10 deg F temperature difference)	1.01	—	11.00	—
5. Nominal 2-in. × 4-in. wood stud	—	4.38	—	4.38
6. Gypsum wallboard, 0.5 in.	0.45	0.45	0.45	0.45
7. Inside surface (still air)	0.68	0.68	0.68	0.68
Total Thermal Resistance ( <i>R</i> )	$R_i=4.44$	$R_s=7.81$	$R_i=14.43$	$R_s=7.81$

Construction No. 1:  $U_i = 1/4.44 = 0.225$ ;  $U_s = 1/7.81 = 0.128$ . With 20% framing (typical of 2-in. × 4-in. studs @ 16-in. o.c.),  $U_{av} = 0.8(0.225) + 0.2(0.128) = 0.206$  (See Eq 9)

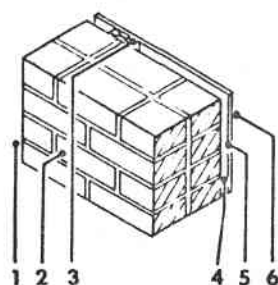
Construction No. 2:  $U_i = 1/14.43 = 0.069$ ;  $U_s = 0.128$ . With framing unchanged,  $U_{av} = 0.8(0.069) + 0.2(0.128) = 0.081$

\*See text section Calculating Overall Coefficients for basis of calculations.

**Table 4B Coefficients of Transmission (*U*) of Solid Masonry Walls<sup>a</sup>**

Coefficients are expressed in Btu per (hour) (square foot) (degree Fahrenheit difference in temperature between the air on the two sides), and are based on an outside wind velocity of 15 mph

Replace Furring Strips and Air Space with 1-in. Extruded Polystyrene (New Item 4)

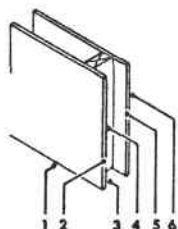


Construction	Resistance ( <i>R</i> )		2
	Between Furring	At Furring	
1. Outside surface (15 mph wind)	0.17	0.17	0.17
2. Common brick, 8 in.	1.60	1.60	1.60
3. Nominal 1-in. x 3-in. vertical furring	—	0.94	—
4. Nonreflective air space, 0.75 in. (50 F mean; 10 deg F temperature difference)	1.01	—	5.00
5. Gypsum wallboard, 0.5 in.	0.45	0.45	0.45
6. Inside surface (still air)	0.68	0.68	0.68
Total Thermal Resistance ( <i>R</i> )	$R_i = 3.91$	$R_s = 3.84$	$R_t = 7.90 = R_s$

Construction No. 1:  $U_i = 1/3.91 = 0.256$ ;  $U_s = 1/3.84 = 0.260$ . With 20% framing (typical of 1-in. x 3-in. vertical furring on masonry @ 16-in. o.c.)  $U_{av} = 0.8(0.256) + 0.2(0.260) = 0.257$ Construction No. 2:  $U_i = U_s = U_{av} = 1/7.90 = 0.127$ <sup>a</sup>See text section Calculating Overall Coefficients for basis of calculations.**Table 4C Coefficients of Transmission (*U*) of Frame Partitions or Interior Walls<sup>a</sup>**

Coefficients are expressed in Btu per (hour) (square foot) (degree Fahrenheit difference in temperature between the air on the two sides), and are based on still air (no wind) conditions on both sides

Replace Air Space with 3.5-in. R-11 Blanket Insulation (New Item 3)

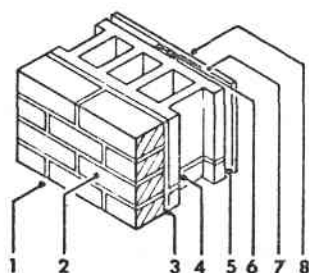


Construction	Resistance ( <i>R</i> )			
	Between Framing	At Framing	Between Framing	At Framing
1. Inside surface (still air)	0.68	0.68	0.68	0.68
2. Gypsum wallboard, 0.5 in.	0.45	0.45	0.45	0.45
3. Nonreflective air space, 3.5 in. (50 F mean; 10 deg F temperature difference)	1.01	—	11.00	—
4. Nominal 2-in. x 4-in. wood stud	—	4.38	—	4.38
5. Gypsum wallboard, 0.5 in.	0.45	0.45	0.45	0.45
6. Inside surface (still air)	0.68	0.68	0.68	0.68
Total Thermal Resistance ( <i>R</i> )	$R_i = 3.27$	$R_s = 6.64$	$R_t = 13.26$	$R_s = 6.64$

Construction No. 1:  $U_i = 1/3.27 = 0.306$ ;  $U_s = 1/6.64 = 0.151$ . With 10% framing (typical of 2-in. x 4-in. studs @ 24-in. o.c.),  $U_{av} = 0.9(0.306) + 0.1(0.151) = 0.290$ Construction No. 2:  $U_i = 1/13.26 = 0.075$ ,  $U_s = 1/6.64 = 0.151$ . With framing unchanged,  $U_{av} = 0.9(0.075) + 0.1(0.151) = 0.083$ <sup>a</sup>See text section Calculating Overall Coefficients for basis of calculations.**Table 4D Coefficients of Transmission (*U*) of Masonry Walls<sup>a</sup>**

Coefficients are expressed in Btu per (hour) (square foot) (degree Fahrenheit difference in temperature between the air on the two sides), and are based on an outside wind velocity of 15 mph

Replace Cinder Aggregate Block with 6-in. Light-weight Aggregate Block with Cores Filled (New Item 4)



Construction	Resistance ( <i>R</i> )			
	Between Furring	At Furring	Between Furring	At Furring
1. Outside surface (15 mph wind)	0.17	0.17	0.17	0.17
2. Face brick, 4 in.	0.44	0.44	0.44	0.44
3. Cement mortar, 0.5 in.	0.10	0.10	0.10	0.10
4. Concrete block, cinder aggregate, 8 in.	1.72	1.72	2.99	2.99
5. Reflective air space, 0.75 in. (50 F mean; 30 deg F temperature difference)	2.77	—	2.77	—
6. Nominal 1-in. x 3-in. vertical furring	—	0.94	—	0.94
7. Gypsum wallboard, 0.5 in., foil backed	0.45	0.45	0.45	0.45
8. Inside surface (still air)	0.68	0.68	0.68	0.68
Total Thermal Resistance ( <i>R</i> )	$R_i = 6.33$	$R_s = 4.50$	$R_t = 7.60$	$R_s = 5.77$

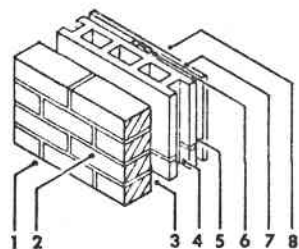
Construction No. 1:  $U_i = 1/6.33 = 0.158$ ;  $U_s = 1/4.50 = 0.222$ . With 20% framing (typical of 1-in. x 3-in. vertical furring on masonry @ 16-in. o.c.),  $U_{av} = 0.8(0.158) + 0.2(0.222) = 0.171$ Construction No. 2:  $U_i = 1/7.60 = 0.132$ ,  $U_s = 1/5.77 = 0.173$ . With framing unchanged,  $U_{av} = 0.8(0.132) + 0.2(0.173) = 0.140$ <sup>a</sup>See text section Calculating Overall Coefficients for basis of calculations.



**Table 4E Coefficients of Transmission (*U*) of Masonry Cavity Walls<sup>a</sup>**

<sup>a</sup> Coefficients are expressed in Btu per (hour) (square foot) (degree Fahrenheit difference in temperature between the air on the two sides), and are based on an outside wind velocity of 15 mph

Replace Furring Strips and Gypsum Wallboard with 0.625-in. Plaster (Sand Aggregate) Applied Directly to Concrete Block-Fill 2.5-in. Air Space with Vermiculite Insulation (New Items 3 and 7).



Construction	Resistance ( <i>R</i> )		2
	Between Furring	At Furring	
1. Outside surface (15 mph wind)	0.17	0.17	0.17
2. Common brick, 8 in.	0.80	0.80	0.80
3. Nonreflective air space, 2.5 in. (30 F mean; 10 deg F temperature difference)	1.10*	1.10*	5.32**
4. Concrete block, stone aggregate, 4 in.	0.71	0.71	0.71
5. Nonreflective air space 0.75 in. (50 F mean; 10 deg F temperature difference)	1.01	—	—
6. Nominal 1-in. x 3-in. vertical furring	—	0.94	—
7. Gypsum wallboard, 0.5 in.	0.45	0.45	0.11
8. Inside surface (still air)	0.68	0.68	0.68
Total Thermal Resistance ( <i>R</i> ) . . . . .	<i>R<sub>i</sub></i> = 4.92	<i>R<sub>s</sub></i> = 4.85	<i>R<sub>i</sub></i> = <i>R<sub>s</sub></i> = 7.79

Construction No. 1:  $U_i = 1/4.92 = 0.203$ ;  $U_s = 1/4.85 = 0.206$ . With 20% framing (typical of 1-in. x 3-in. vertical furring on masonry @ 16-in. o.c.),  $U_{av} = 0.8(0.203) + 0.2(0.206) = 0.204$

Construction No. 2:  $U_i = U_s = U_{av} = 1.79 = 0.128$

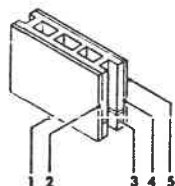
<sup>a</sup> See text section Calculating Overall Coefficients for basis of calculations.

\* Interpolated value from Table 2.

\*\* Calculated value from Table 3.

**Table 4F Coefficients of Transmission (*U*) of Masonry Partitions<sup>a</sup>**

Coefficients are expressed in Btu per (hour) (square foot) (degree Fahrenheit difference in temperature between the air on the two sides), and are based on still air (no wind) conditions on both sides



Construction	1	2
	1	2
1. Inside surface (still air)	0.68	0.68
2. Plaster, lightweight aggregate, 0.625 in.	0.39	0.39
3. Concrete block, cinder aggregate, 4 in.	1.11	1.67
4. Plaster, lightweight aggregate, 0.625 in.	0.39	0.39
5. Inside surface (still air)	0.68	0.68
Total Thermal Resistance ( <i>R</i> ) . . . . .	3.25	3.81

Construction No. 1:  $U = 1/3.25 = 0.308$

Construction No. 2:  $U = 1/3.81 = 0.262$

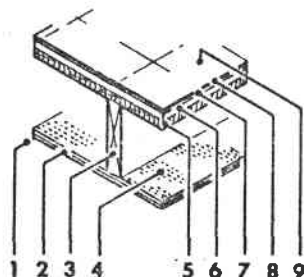
<sup>a</sup> See text section Calculating Overall Coefficients for basis of calculations.

**Table 4G Coefficients of Transmission (*U*) of Frame Construction Ceilings and Floors<sup>a</sup>**

Coefficients are expressed in Btu per (hour) (square foot) (degree Fahrenheit difference between the air on the two sides), and are based on still air (no wind) on both sides

Assume Unheated Attic Space above Heated Room with Heat Flow Up—Remove Tile, Felt, Plywood, Sub-floor and Air Space—Replace with R-19 Blanket Insulation (New Item 4)

Heated Room Below  
Unheated Space



Construction (Heat Flow Up)	Resistance ( <i>R</i> )		2	
	Between Floor Joists	At Floor Joist	Between Floor Joists	At Floor Joists
1. Bottom surface (still air)	0.61	0.61	0.61	0.61
2. Metal lath and lightweight aggregate, plaster, 0.75 in.	0.47	0.47	0.47	0.47
3. Nominal 2-in. x 8-in. floor joist	—	9.06	—	9.06
4. Nonreflective airspace, 7.25-in.	0.93*	—	19.00	—
5. Wood subfloor, 0.75 in.	0.94	0.94	—	—
6. Plywood, 0.625 in.	0.78	0.78	—	—
7. Felt building membrane	0.06	0.06	—	—
8. Resilient tile	0.05	0.05	—	—
9. Top surface (still air)	0.61	0.61	0.61	0.61
Total Thermal Resistance ( <i>R</i> ) . . . . .	<i>R<sub>i</sub></i> = 4.45	<i>R<sub>s</sub></i> = 12.58	<i>R<sub>i</sub></i> = 20.69	<i>R<sub>s</sub></i> = 10.75

Construction No. 1:  $U_i = 1/4.45 = 0.225$ ;  $U_s = 1/12.58 = 0.079$ . With 10% framing (typical of 2-in. joists @ 16-in. o.c.),  $U_{av} = 0.9(0.225) + 0.1(0.079) = 0.210$

Construction No. 2:  $U_i = 1/20.69 = 0.048$ ;  $U_s = 1/10.75 = 0.093$ . With framing unchanged,  $U_{av} = 0.9(0.048) + 0.1(0.093) = 0.053$

<sup>a</sup> See text section Calculating Overall Coefficients for basis of calculations.

\* Use largest air space (3.5 in.) value shown in Table 2.

**Table 4H Coefficients of Transmission (*U*) of Flat Masonry Roofs with Built-up Roofing, with and without Suspended Ceilings<sup>a,b</sup> (Winter Conditions, Upward Flow)**

These Coefficients are expressed in Btu per (hour) (square foot) (degree Fahrenheit difference in temperature between the air on the two sides), and are based upon an outside wind velocity of 15 mph

Add Rigid Roof Deck Insulation, $C = 0.24$ ( $R = 1/C$ ) (New Item 7)			
Construction (Heat Flow Up)		1	2
1. Inside surface (still air)		0.61	0.61
1. Metal lath and lightweight aggregate plaster, 0.75 in.		0.47	0.47
3. Nonreflective air space, greater than 3.5 in. (50 F mean; 10 deg F temperature difference)		0.93*	0.93*
4. Metal ceiling suspension system with metal hanger rods		0**	0**
5. Corrugated metal deck		0	0
6. Concrete slab, lightweight aggregate, 2 in.		2.22	2.22
7. Rigid roof deck insulation (none)		—	4.17
8. Built-up roofing, 0.375 in.		0.33	0.33
9. Outside surface (15 mph wind)		0.17	0.17
Total Thermal Resistance ( <i>R</i> )		4.73	8.90

Construction No. 1:  $U_{av} = 1/4.73 = 0.211$

Construction No. 2:  $U_{av} = 1/8.90 = 0.112$

<sup>a</sup>See text section Calculating Overall Coefficients for basis of calculations.

<sup>b</sup>To adjust *U* values for the effect of added insulation between framing members, see Table 5 or 6.

\*Use largest air space (3.5 in.) value shown in Table 2.

\*\*Area of hanger rods is negligible in relation to ceiling area.

**Table 4I Coefficients of Transmission (*U*) of Wood Construction Flat Roofs and Ceilings<sup>a</sup> (Winter Conditions, Upward Flow)**

Coefficients are expressed in Btu per (hour) (square foot) (degree Fahrenheit difference in temperature between the air on the two sides), and are based upon an outside wind velocity of 15 mph

Replace Roof Deck Insulation and 7.25-in. Air Space with 6-in. R-19 Blanket Insulation and 1.25-in. Air Space (New Items 5 and 7)

Construction (Heat Flow Up)	1		2	
	Resistance ( <i>R</i> )			
	Between Joists	At Joists	Between Joists	At Joists
1. Inside surface (still air)	0.61	0.61	0.61	0.61
2. Acoustical tile, fiberboard, glued, 0.5 in.	1.25	1.25	1.25	1.25
3. Gypsum wallboard, 0.5 in.	0.45	0.45	0.45	0.45
4. Nominal 2-in. × 8-in. ceiling joists	—	9.06	—	9.06
5. Nonreflective air space, 7.25 in. (50 F mean; 10 deg F temperature difference)	0.93*	—	1.05**	—
6. Plywood deck, 0.625 in.	0.78	0.78	0.78	0.78
7. Rigid roof deck insulation, $c = 0.72$ , ( $R = 1/C$ )	1.39	1.39	19.00	—
8. Built-up roof	0.33	0.33	0.33	0.33
9. Outside surface (15 mph wind)	0.17	0.17	0.17	0.17
Total Thermal Resistance ( <i>R</i> )	$R_i = 5.91$	$R_s = 14.04$	$R_i = 23.64$	$R_s = 12.65$

Construction No. 1  $U_i = 1/5.91 = 0.169$ ;  $U_s = 1/14.04 = 0.071$ . With 10% framing (typical of 2-in. joists @ 16-in. o.c.),  $U_{av} = 0.9(0.169) + 0.1(0.071) = 0.159$

Construction No. 2  $U_i = 1/23.64 = 0.042$ ;  $U_s = 1/12.65 = 0.079$ . With framing unchanged,  $U_{av} = 0.9(0.042) + 0.1(0.079) = 0.046$

<sup>a</sup>See text section Calculating Overall Coefficients for basis of calculations.

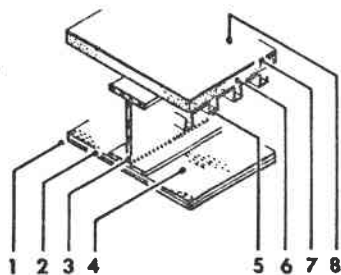
\*Use largest air space (3.5 in.) value shown in Table 2.

\*\*Interpolated value (0 F mean; 10 deg F temperature difference).



**Table 4J Coefficients of Transmission (*U*) of Metal Construction Flat Roofs and Ceilings\***  
(Winter Conditions, Upward Flow)

Coefficients are expressed in Btu per (hour) (square foot) (degree Fahrenheit difference in temperature between the air on the two sides), and are based on upon outside wind velocity of 15 mph



Replace Rigid Roof Deck Insulation ( $C = 0.24$ ) and Sand Aggregate Plaster with Rigid Roof Deck Insulation,  $C = 0.36$  and Lightweight Aggregate Plaster (New Items 2 and 6)

Construction (Heat Flow Up)	1	2
1. Inside surface (still air)	0.61	0.61
2. Metal lath and sand aggregate plaster, 0.75 in	0.13	0.47
3. Structural beam	0.00*	0.00*
4. Nonreflective air space (50 F mean; 10 deg F temperature difference)	0.93**	0.93**
5. Metal deck	0.00*	0.00*
6. Rigid roof deck insulation, $C = 0.24$ ( $R = 1/c$ )	4.17	2.78
7. Built-up roofing, 0.375 in.	0.33	0.33
8. Outside surface (15 mph wind)	0.17	0.17
Total Thermal Resistance ( <i>R</i> )	6.34	5.29

Construction No. 1:  $U = 1/6.34 = 0.158$

Construction No. 2:  $U = 1/5.29 = 0.189$

\* See text section Calculating Overall Coefficients for basis of calculations.

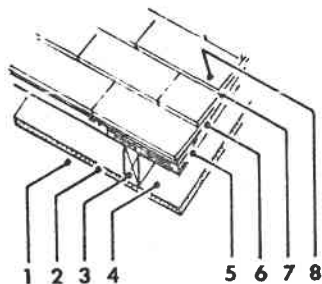
If structural beams and metal deck are to be considered, the technique shown in Examples 1 and 2, and Fig. 3 may be used to estimate total *R*. Full scale testing of a suitable portion of the construction is, however, preferable.

\*\* Use largest air space (3.5 in.) value shown in Table 2.

**Table 4K Coefficients of Transmission (*U*) of Pitched Roofs<sup>a,b</sup>**

Coefficients are expressed in Btu per (hour) (square foot) (degree Fahrenheit difference in temperature between the air on the two sides), and are based on an outside wind velocity of 15 mph for heat flow upward and 7.5 mph for heat flow downward

Find  $U_{av}$  for same Construction 2 with Heat Flow Down (Summer Conditions)



Construction 1 (Heat Flow Up) (Reflective Air Space)	1		2	
	Between Rafters	At Rafters	Between Rafters	At Rafters
1. Inside surface (still air)	0.62	0.62	0.76	0.76
2. Gypsum wallboard 0.5 in., foil backed	0.45	0.45	0.45	0.45
3. Nominal 2-in. x 4-in. ceiling rafter	—	4.38	—	4.38
4. 45 deg slope reflective air space, 3.5 in. (50 F mean, 30 deg F temperature difference)	2.17	—	4.33	—
5. Plywood sheathing, 0.625 in.	0.78	0.78	0.78	0.78
6. Felt building membrane	0.06	0.06	0.06	0.06
7. Asphalt shingle roofing	0.44	0.44	0.44	0.44
8. Outside surface (15 mph wind)	0.17	0.17	0.25**	0.25**
Total Thermal Resistance ( <i>R</i> )	$R_t = 4.69$	$R_s = 6.90$	$R_t = 7.07$	$R_s = 7.12$

Construction No. 1:  $U_t = 1/4.69 = 0.213$ ;  $U_s = 1/6.90 = 0.145$ . With 10% framing (typical of 2-in. rafters @ 16-in. o.c.),  $U_{av} = 0.9 (0.213) + 0.1 (0.145) = 0.206$

Construction No. 2:  $U_t = 1/7.07 = 0.141$ ;  $U_s = 1/7.12 = 0.140$ . With framing unchanged,  $U_{av} = 0.9 (0.141) + 0.1 (0.140) = 0.141$

Find  $U_{av}$  for same Construction 2 with Heat Flow Down (Summer Conditions)

Construction 1 (Heat Flow Up) (Non-Reflective Air Space)	3		4	
	Between Rafters	At Rafters	Between Rafters	At Rafters
1. Inside surface (still air)	0.62	0.62	0.76	0.76
2. Gypsum wallboard, 0.5 in.	0.45	0.45	0.45	0.45
3. Nominal 2-in. x 4-in. ceiling rafter	—	4.38	—	4.38
4. 45 deg slope, nonreflective air space, 3.5 in. (50 F mean; 10 deg F temperature difference)	0.96	—	0.90*	—
5. Plywood sheathing, 0.625 in.	0.78	0.78	0.78	0.78
6. Felt building membrane	0.06	0.06	0.06	0.06
7. Asphalt shingle roofing	0.44	0.44	0.44	0.44
8. Outside surface (15-mph wind)	0.17	0.17	0.25**	0.25**
Total Thermal Resistance ( <i>R</i> )	$R_t = 3.48$	$R_s = 6.90$	$R_t = 3.64$	$R_s = 7.12$

Construction No. 3:  $U_t = 1/3.48 = 0.287$ ;  $U_s = 1/6.90 = 0.145$ . With 10% framing typical of 2-in. rafters @ 16-in. o.c.),  $U_{av} = 0.9 (0.287) + 0.1 (0.145) = 0.273$

Construction No. 4:  $U_t = 1/3.64 = 0.275$ ;  $U_s = 1/7.12 = 0.140$ . With framing unchanged,  $U_{av} = 0.9 (0.275) + 0.1 (0.140) = 0.262$

\* See text section Calculating Overall Coefficients for basis of calculations.

<sup>b</sup> Pitch of roof—45 deg.

\* Air space value at 90 F mean, 10 F dif. temperature difference.

\*\* 7.5-mph wind.

**Table 5A Determination of  $U$ -Value Resulting from Addition of Insulation to the Total Area<sup>a</sup> of any Given Building Section**

Given Building Section Property <sup>a,b</sup>	Added $R^{c,d,e}$							
	$R = 4$		$R = 6$		$R = 8$		$R = 12$	
	$U$	$R$	$U$	$R$	$U$	$R$	$U$	$R$
1.00	1.00	0.20	0.14	0.11	0.08	0.06	0.05	0.04
0.90	1.11	0.20	0.14	0.11	0.08	0.06	0.05	0.04
0.80	1.25	0.19	0.14	0.11	0.08	0.06	0.05	0.04
0.70	1.43	0.18	0.13	0.11	0.07	0.06	0.05	0.04
0.60	1.67	0.18	0.13	0.10	0.07	0.06	0.05	0.04
0.50	2.00	0.17	0.13	0.10	0.07	0.06	0.05	0.04
0.40	2.50	0.15	0.12	0.10	0.07	0.05	0.04	0.04
0.30	3.33	0.14	0.11	0.09	0.07	0.05	0.04	0.04
0.20	5.00	0.11	0.09	0.08	0.06	0.05	0.04	0.03
0.10	10.00	0.07	0.06	0.06	0.05	0.04	0.03	0.03
0.08	12.50	0.06	0.05	0.05	0.04	0.04	0.03	0.03

<sup>a</sup>For  $U$ - or  $R$ -values not shown in the table, interpolate as necessary.

<sup>b</sup>Enter column 1 with  $U$  or  $R$  of the design building section.

<sup>c</sup>Under appropriate column heading for added  $R$ , find  $U$ -value of resulting design section.

<sup>d</sup>If the insulation occupies previously considered air space, an adjustment must be made in the given building section  $R$ -value.

<sup>e</sup>If insulation is applied between framing members, use Eq 9 to determine average  $U$ -value.

**Table 5B Determination of  $U$ -Value Resulting from Addition of Insulation to Uninsulated Roof Deck**

$U$ -Value of Roof without Roof-Deck Insulation <sup>a</sup>	Conductance $C$ of Roof-Deck Insulation					
	0.12	0.15	0.19	0.24	0.36	0.72
	$U$	$U$	$U$	$U$	$U$	$U$
0.10	0.05	0.06	0.07	0.07	0.08	0.09
0.15	0.07	0.08	0.08	0.09	0.11	0.12
0.20	0.08	0.09	0.10	0.11	0.13	0.16
0.25	0.08	0.09	0.11	0.12	0.15	0.19
0.30	0.09	0.10	0.12	0.13	0.16	0.21
0.35	0.09	0.11	0.12	0.14	0.18	0.24
0.40	0.09	0.11	0.13	0.15	0.19	0.26
0.50	0.10	0.12	0.14	0.16	0.21	0.30
0.60	0.10	0.12	0.14	0.17	0.23	0.33
0.70	0.10	0.12	0.15	0.18	0.24	0.35

<sup>a</sup>Interpolation or mild extrapolation may be used.

**Table 6 Effective Resistance of Ventilated Attics<sup>a</sup>—(Summer Condition)<sup>5</sup>**  
**PART A. NONREFLECTIVE SURFACES**

Ventilation Air Temp., F		Sol-Air <sup>d</sup> Temp., F		PARTIAL NONREFLECTIVE SURFACES									
				No Ventilation		Natural Ventilation		Power Ventilation <sup>e</sup>					
				Ventilation Rate, cfm/ft <sup>2</sup>									
				0		0.1 <sup>b</sup>		0.5		1.0		1.5	
				1/U Ceiling Resistance, R <sup>c</sup>									
				10	20	10	20	10	20	10	20	10	20
80	120	1.9	1.9	2.8	3.4	6.3	9.3	9.6	16	11	20		
	140	1.9	1.9	2.8	3.5	6.5	10	9.8	17	12	21		
	160	1.9	1.9	2.8	3.6	6.7	11	10	18	13	22		
90	120	1.9	1.9	2.5	2.8	4.6	6.7	6.1	10	6.9	13		
	140	1.9	1.9	2.6	3.1	5.2	7.9	7.6	12	8.6	15		
	160	1.9	1.9	2.7	3.4	5.8	9.0	8.5	14	10	17		
100	120	1.9	1.9	2.2	2.3	3.3	4.4	4.0	6.0	4.1	6.9		
	140	1.9	1.9	2.4	2.7	4.2	6.1	5.8	8.7	6.5	10		
	160	1.9	1.9	2.6	3.2	5.0	7.6	7.2	11	8.3	13		

**PART B. REFLECTIVE SURFACES<sup>f</sup>**

80	120	6.5	6.5	8.1	8.8	13	17	17	25	19	30
	140	6.5	6.5	8.2	9.0	14	18	18	26	20	31
	160	6.5	6.5	8.3	9.2	15	18	19	27	21	32
90	120	6.5	6.5	7.5	8.0	10	13	12	17	13	19
	140	6.5	6.5	7.7	8.3	12	15	14	20	16	22
	160	6.5	6.5	7.9	8.6	13	16	16	22	18	25
100	120	6.5	6.5	7.0	7.4	8.0	10	8.5	12	8.8	12
	140	6.5	6.5	7.3	7.8	10	12	11	15	12	16
	160	6.5	6.5	7.6	8.2	11	14	13	18	15	20

<sup>a</sup>The term *effective resistance* is used when there is attic ventilation. A value for no ventilation is also included. The effective resistance of the attic may be added to the resistance ( $1/U$ ) of the ceiling (Table 4G) to obtain the effective resistance of the combination based on sol-air (Chapter 28) and room temperature. These values apply to wood frame construction with a roof deck and roofing having a conductance of 1.0 Btu/(hr · ft<sup>2</sup> · F).

<sup>b</sup>When attic ventilation meets the requirements of Table 3 in Chapter 21, 0.1 cfm/ft<sup>2</sup> may be assumed as the natural summer ventilation rate for design purposes.

<sup>c</sup>Resistance is one (hr · ft<sup>2</sup> · F)/Btu. Determine ceiling resistance from Tables 4G and 5A, and adjust for framing by Eq 9. Do not add the effect of a reflective surface facing the attic to the ceiling resistance from Table 4G, as it is accounted for in Table 6, Part B.

<sup>d</sup>Roof surface temperature rather than sol-air temperature (see Chapter 28) may be used if 0.25 is subtracted from the attic resistance shown.

<sup>e</sup>Based on air discharging outward from attic.

<sup>f</sup>Surfaces with effective emittance  $E$  of 0.05 between ceiling joists facing the attic space.

**Table 7 Estimated Heat Lost from Building by Infiltration<sup>13</sup>**

The tabulated factors, when multiplied by room or building volume ( $\text{ft}^3$ ), will result in estimated heat loss (Btu/hr) due to infiltration and does not include the heat needed to warm ventilating air

Room or Building Type	No. of Walls with Windows	Temp. Difference, deg F				Room or Building Type	No. of Walls with Windows	Temp. Difference, deg F			
		25	50	75	100			25	50	75	100
A	None	0.23	0.45	0.68	0.90	B	Any	1.35	2.70	4.05	5.40
	1	0.34	0.68	1.02	1.36	C	Any	0.90-1.35	1.80-2.70	2.70-4.05	3.60-5.40
	2	0.68	1.35	2.02	2.70	D	Any	0.45-0.68	0.90-1.35	1.35-2.02	1.80-2.70
	3 or 4	0.90	1.80	2.70	3.60	E	Any	0.68-1.35	1.35-2.70	2.03-4.05	2.70-5.40

**A =** Offices, apartments, hotels, multistory buildings in general.

**B =** Entrance halls or vestibules.

**C = Industrial buildings.**

D = Houses, all types, all rooms except vestibules.

**E** = Public or institutional buildings.

**Table 8 Coefficients of Transmission ( $U$ ) of Windows, Skylights, and Light Transmitting Partitions**

These values are for heat transfer from air to air, Btu/(hr · ft<sup>2</sup> · F). To calculate total heat gain including solar transmission, see Chapter 28.

<b>PART A—VERTICAL PANELS (EXTERIOR WINDOWS, SLIDING PATIO DOORS, AND PARTITIONS)— FLAT GLASS, GLASS BLOCK, AND PLASTIC SHEET</b>				<b>PART B—HORIZONTAL PANELS (SKYLIGHTS)— FLAT GLASS, GLASS BLOCK, AND PLASTIC DOMES</b>			
Description	Exterior <sup>a</sup>		Interior	Description	Exterior <sup>a</sup>		Interior <sup>f</sup>
	Winter	Summer			Winter <sup>i</sup>	Summer <sup>j</sup>	
<b>Flat Glass<sup>b</sup></b>				<b>Flat Glass<sup>c</sup></b>			
single glass	1.10	1.04	0.73	single glass	1.23	0.83	0.96
<b>insulating glass—double<sup>c</sup></b>				<b>insulating glass—double<sup>c</sup></b>			
0.1875-in. air space <sup>d</sup>	0.62	0.65	0.51	0.1875-in. air space <sup>d</sup>	0.70	0.57	0.62
0.25-in. air space <sup>d</sup>	0.58	0.61	0.49	0.25-in. air space <sup>d</sup>	0.65	0.54	0.59
0.5-in. air space <sup>e</sup>	0.49	0.56	0.46	0.5-in. air space <sup>e</sup>	0.59	0.49	0.56
0.5-in. air space, low emittance coating <sup>f</sup>				0.5-in. air space, low emittance coating <sup>f</sup>			
e = 0.20	0.32	0.38	0.32	e = 0.20	0.48	0.36	0.39
e = 0.40	0.38	0.45	0.38	e = 0.40	0.52	0.42	0.45
e = 0.60	0.43	0.51	0.42	e = 0.60	0.56	0.46	0.50
<b>insulating glass—triple<sup>c</sup></b>				<b>Glass Block<sup>h</sup></b>			
0.25-in. air spaces <sup>d</sup>	0.39	0.44	0.38	11 × 11 × 3 in. thick with cavity divider	0.53	0.35	0.44
0.5-in. air spaces <sup>g</sup>	0.31	0.39	0.30	12 × 12 × 4 in. thick with cavity divider	0.51	0.34	0.42
<b>storm windows</b>							
1-in. to 4-in. air spaced <sup>d</sup>	0.50	0.50	0.44				
<b>Plastic Sheet</b>				<b>Plastic Domes<sup>k</sup></b>			
single glazed				single-walled	1.15	0.80	—
0.125-in. thick	1.06	0.98	—	double-walled	0.70	0.46	—
0.25-in. thick	0.96	0.89	—				
0.5-in. thick	0.81	0.76	—				
<b>insulating unit—double<sup>c</sup></b>				<b>PART C—ADJUSTMENT FACTORS FOR VARIOUS WINDOW AND SLIDING PATIO DOOR TYPES (MULTIPLY U VALUES IN PARTS A AND B BY THESE FACTORS)</b>			
0.25-in. air space <sup>d</sup>	0.55	0.56	—				
0.5-in. air space <sup>e</sup>	0.43	0.45	—				
<b>Glass Block<sup>h</sup></b>							
6 × 6 × 4 in. thick	0.60	0.57	0.46	Description	Single Glass	Double or Triple Glass	Storm Windows
8 × 8 × 4 in. thick	0.56	0.54	0.44	Windows			
—with cavity divider	0.48	0.46	0.38	All Glass <sup>l</sup>	1.00	1.00	1.00
12 × 12 × 4 in. thick	0.52	0.50	0.41	Wood Sash—80% Glass	0.90	0.95	0.90
—with cavity divider	0.44	0.42	0.36	Wood Sash—60% Glass	0.80	0.85	0.80
12 × 12 × 2 in. thick	0.60	0.57	0.46	Metal Sash—80% Glass	1.00	1.20 <sup>m</sup>	1.20 <sup>m</sup>
				<b>Sliding Patio Doors</b>			
				Wood Frame	0.95	1.00	—
				Metal Frame	1.00	1.10 <sup>m</sup>	—

<sup>a</sup>See Part C for adjustment for various window and sliding patio door types.

<sup>b</sup>Emittance of uncooled glass surface = 0.84.

<sup>c</sup>Double and triple refer to the number of lights of glass.

<sup>d</sup>0.125-in. glass.

°0.25-in. glass.

<sup>f</sup>Coating on either glass surface facing air space; all other glass surfaces uncoated.

<sup>8</sup>Window design: 0.25-in. glass—0.125-in. glass—0.25-in. glass.

<sup>h</sup> Dimensions are nominal.<sup>i</sup>For heat flow up.<sup>j</sup>For heat flow down.

<sup>k</sup>Based on area of opening, not total surface area.

<sup>1</sup>Refers to windows with negligible opaque area.

<sup>m</sup> Values will be less than these when metal sash and frame incorporate thermal breaks. In some thermal break designs, *U*-values will be equal to or less than those for the glass. Window manufacturers should be consulted for specific data.

Table 9 Coefficients of Transmission ( $U$ ) for Slab Doors

Btu per (hr · ft <sup>2</sup> · F)				
Thickness <sup>a</sup>	Winter		Summer	
	Solid Wood, No Storm Door	Storm Door <sup>b</sup>		No Storm Door
		Wood	Metal	
1-in.	0.64	0.30	0.39	0.61
1.25-in.	0.55	0.28	0.34	0.53
1.5-in.	0.49	0.27	0.33	0.47
2-in.	0.43	0.24	0.29	0.42
Steel Door <sup>14</sup>				
1.75 in.				
A <sup>c</sup>	0.59	—	—	0.58
B <sup>d</sup>	0.19	—	—	0.18
C <sup>e</sup>	0.47	—	—	0.46

<sup>a</sup>Nominal thickness.<sup>b</sup>Values for wood storm doors are for approximately 50% glass; for metal storm door values apply for any percent of glass.<sup>c</sup>A = Mineral fiber core (2 lb/ft<sup>3</sup>).<sup>d</sup>B = Solid urethane foam core with thermal break.<sup>e</sup>C = Solid polystyrene core with thermal break.Table 10 Conversion Table for Wall Coefficient  $U$  for Various Wind Velocities

$U$ for 15 mph <sup>a</sup>	$U$ for 0 to 30 mph Wind Velocities						$U$ for 15 mph <sup>a</sup>	$U$ for 0 to 30 mph Wind Velocities					
	0	5	10	20	25	30		0	5	10	20	25	30
0.050	0.049	0.050	0.050	0.050	0.050	0.050	0.290	0.257	0.278	0.286	0.293	0.295	0.296
0.060	0.059	0.059	0.060	0.060	0.060	0.060	0.310	0.273	0.296	0.305	0.313	0.315	0.317
0.070	0.068	0.069	0.070	0.070	0.070	0.070	0.330	0.288	0.314	0.324	0.333	0.336	0.338
0.080	0.078	0.079	0.080	0.080	0.080	0.080	0.350	0.303	0.332	0.344	0.354	0.357	0.359
0.090	0.087	0.089	0.090	0.090	0.091	0.091	0.370	0.318	0.350	0.363	0.375	0.378	0.380
0.100	0.096	0.099	0.100	0.100	0.101	0.101	0.390	0.333	0.368	0.382	0.395	0.399	0.401
0.110	0.105	0.108	0.109	0.110	0.111	0.111	0.410	0.347	0.385	0.402	0.416	0.420	0.422
0.130	0.123	0.127	0.129	0.131	0.131	0.131	0.430	0.362	0.403	0.421	0.436	0.441	0.444
0.150	0.141	0.147	0.149	0.151	0.151	0.152	0.450	0.376	0.420	0.439	0.457	0.462	0.465
0.170	0.158	0.166	0.169	0.171	0.172	0.172	0.500	0.410	0.464	0.487	0.509	0.514	0.518
0.190	0.175	0.184	0.188	0.191	0.192	0.193	0.600	0.474	0.548	0.581	0.612	0.620	0.626
0.210	0.192	0.203	0.208	0.212	0.213	0.213	0.700	0.535	0.631	0.675	0.716	0.728	0.736
0.230	0.209	0.222	0.227	0.232	0.233	0.234	0.800	0.592	0.711	0.766	0.821	0.836	0.847
0.250	0.226	0.241	0.247	0.252	0.253	0.254	0.900	0.645	0.789	0.858	0.927	0.946	0.960
0.270	0.241	0.259	0.266	0.273	0.274	0.275	1.000	0.695	0.865	0.949	1.034	1.058	1.075

<sup>a</sup> $U$  in first column is from previous tables or as calculated for 15 mph wind velocity.

**Table 11 Heat Losses from Horizontal Bare Steel Pipes and Flat Surfaces<sup>a</sup>**

In Btu per (Square foot of pipe surface)(hour)(degree Fahrenheit temperature difference between pipe and air)

Pipe Size (in.)	Linear Foot Factor <sup>b</sup>	Temperature Difference Degree Fahrenheit between Pipe Surface and Surrounding Air (Air at 80 F)																			
		50	100	150	200	250	300	350	400	450	500	550	600	650	700	750	800	850	900	950	1000
0.5	0.220	2.12	2.48	2.80	3.10	3.42	3.74	4.07	4.47	4.86	5.28	5.72	6.19	6.69	7.22	7.79	8.39	9.03	9.70	10.42	11.18
0.75	0.275	2.08	2.43	2.74	3.04	3.35	3.67	4.00	4.40	4.79	5.21	5.65	6.12	6.61	7.15	7.71	8.31	8.95	9.62	10.34	11.09
1	0.344	2.04	2.38	2.69	2.99	3.30	3.61	3.94	4.33	4.72	5.14	5.58	6.05	6.54	7.07	7.64	8.23	8.87	9.55	10.26	11.02
1.25	0.435	2.00	2.34	2.64	2.93	3.24	3.55	3.88	4.27	4.66	5.07	5.51	5.97	6.47	7.00	7.56	8.16	8.79	9.47	10.18	10.94
1.5	0.497	1.98	2.31	2.61	2.90	3.20	3.52	3.84	4.23	4.62	5.03	5.47	5.93	6.43	6.96	7.52	8.12	8.75	9.43	10.14	10.89
2	0.622	1.95	2.27	2.56	2.85	3.15	3.46	3.78	4.17	4.56	4.97	5.41	5.87	6.37	6.89	7.45	8.05	8.68	9.36	10.07	10.82
2.5	0.753	1.92	2.23	2.52	2.81	3.11	3.42	3.74	4.12	4.51	4.92	5.36	5.82	6.31	6.84	7.40	7.99	8.62	9.30	10.01	10.77
3	0.916	1.89	2.20	2.49	2.77	3.07	3.37	3.69	4.08	4.46	4.87	5.31	5.77	6.26	6.79	7.35	7.94	8.57	9.25	9.96	10.71
3.5	1.047	1.87	2.18	2.46	2.74	3.04	3.34	3.66	4.05	4.43	4.84	5.27	5.73	6.23	6.75	7.31	7.91	8.54	9.21	9.92	10.67
4	1.178	1.85	2.16	2.44	2.72	3.01	3.32	3.64	4.02	4.40	4.81	5.25	5.71	6.20	6.72	7.28	7.87	8.51	9.18	9.89	10.64
4.5	1.309	1.84	2.14	2.42	2.70	2.99	3.30	3.61	4.00	4.38	4.79	5.22	5.68	6.17	6.69	7.25	7.85	8.48	9.15	9.86	10.61
5	1.456	1.83	2.13	2.40	2.68	2.97	3.28	3.59	3.97	4.35	4.76	5.20	5.65	6.15	6.68	7.23	7.82	8.45	9.12	9.83	10.58
6	1.734	1.80	2.10	2.37	2.65	2.94	3.24	3.55	3.94	4.32	4.72	5.16	5.61	6.10	6.63	7.19	7.78	8.41	9.08	9.79	10.54
7	1.996	1.79	2.08	2.35	2.63	2.91	3.21	3.53	3.91	4.29	4.69	5.13	5.58	6.07	6.60	7.15	7.75	8.38	9.05	9.76	10.51
8	2.258	1.77	2.06	2.33	2.60	2.89	3.19	3.50	3.88	4.26	4.67	5.10	5.56	6.05	6.57	7.12	7.72	8.35	9.02	9.73	10.48
9	2.520	1.76	2.05	2.31	2.59	2.87	3.17	3.48	3.86	4.24	4.65	5.08	5.53	6.02	6.54	7.10	7.69	8.32	8.99	9.70	10.45
10	2.814	1.75	2.03	2.30	2.57	2.85	3.15	3.46	3.84	4.22	4.62	5.05	5.51	6.00	6.52	7.08	7.67	8.30	8.97	9.68	10.43
12	3.338	1.73	2.01	2.27	2.54	2.83	3.12	3.43	3.81	4.19	4.59	5.02	5.48	5.96	6.48	7.04	7.63	8.26	8.93	9.64	10.39
14	3.665	1.72	2.00	2.26	2.53	2.81	3.11	3.41	3.79	4.17	4.57	5.00	5.46	5.94	6.47	7.02	7.61	8.24	8.91	9.62	10.37
16	4.189	1.70	1.98	2.24	2.51	2.79	3.08	3.39	3.77	4.14	4.55	4.98	5.43	5.92	6.44	6.99	7.59	8.21	8.88	9.59	10.34
18	4.717	1.69	1.96	2.22	2.49	2.77	3.07	3.37	3.75	4.12	4.53	4.96	5.41	5.90	6.42	6.97	7.56	8.19	8.86	9.57	10.32
20	5.236	1.68	1.95	2.21	2.47	2.75	3.05	3.36	3.73	4.11	4.51	4.94	5.39	5.88	6.40	6.95	7.54	8.17	8.84	9.55	10.29
24	6.283	1.66	1.93	2.19	2.45	2.73	3.02	3.33	3.70	4.07	4.48	4.90	5.36	5.84	6.36	6.92	7.51	8.14	8.80	9.51	10.26
Vertical Surface		1.84	2.14	2.42	2.70	3.00	3.30	3.62	4.00	4.38	4.79	5.22	5.68	6.17	6.70	7.26	7.85	8.48	9.15	9.86	10.62
Horizontal Surface Facing Upward		2.03	2.37	2.67	2.97	3.28	3.59	3.92	4.31	4.70	5.12	5.56	6.02	6.52	7.05	7.61	8.21	8.85	9.52	10.24	10.99
Horizontal Surface Facing Downward		1.61	1.86	2.11	2.36	2.64	2.93	3.23	3.60	3.97	4.37	4.80	5.25	5.73	6.25	6.80	7.39	8.02	8.69	9.39	10.14

<sup>a</sup>Values are for Flat Surfaces 4 ft<sup>2</sup> or more in area.<sup>b</sup>To secure losses per linear ft, multiply ft<sup>2</sup> losses in table by this factor. Losses per ft<sup>2</sup> of pipe surface for pipes larger than 24 in. can be considered the same as losses for 24-in. pipe.**Table 12 Heat Losses from Bare Tarnished Copper Tubes<sup>a</sup>**

Nominal Diameter of Tube (in.)	Temperature of Tube, F							
	120	150	180	210	240	270	300	330
	Temperature Difference, Tube to Air, Deg F							
	50	80	110	140	170	200	230	260
Heat Loss per Linear Foot of Tube, Btu/hr								
0.25	8	14	21	29	37	46	56	66
0.375	10	18	28	37	48	60	72	85
0.5	13	22	33	45	59	72	88	104
0.625	15	26	39	53	68	85	102	121
0.75	17	30	45	61	79	97	117	139
1	21	37	55	75	97	120	146	173
1.25	25	45	66	90	117	145	175	207
1.5	29	52	77	105	135	167	203	241
2	37	66	97	132	171	212	257	305
2.5	44	78	117	160	206	255	310	367
3	51	92	136	186	240	297	360	428
3.5	59	104	156	212	274	340	412	490
4	66	118	174	238	307	381	462	550
5	80	142	212	288	373	464	561	669
6	93	166	246	336	432	541	656	776
8	120	215	317	435	562	699	848	1010
10	146	260	387	527	681	848	1031	1227
12	172	304	447	621	802	999	1214	1446

<sup>a</sup>Extracted from Ref 9. Used by permission.**Table 13 External Surface per Linear Foot of Copper Tubing**

Outside diameter 0.125 in. greater than nominal size

Tube Size (in.)	Surface Area (ft <sup>2</sup> )	Tube Size (in.)	Surface Area (ft <sup>2</sup> )	Tube Size (in.)	Surface Area (ft <sup>2</sup> )
0.5	0.164	2	0.556	5	1.342
0.75	0.229	2.5	0.687	6	1.604
1	0.295	3	0.818	8	2.128
1.25	0.360	3.5	0.949	...	....
1.5	0.426	4	1.080	...	....

Table 14 Area of Flanged Fittings, Square Feet<sup>a</sup>

Nominal Pipe Size (in.)	Flanged Coupling		90 Deg Ell		Long Radius Ell		Tee		Cross	
	Standard	Extra Heavy	Standard	Extra Heavy	Standard	Extra Heavy	Standard	Extra Heavy	Standard	Extra Heavy
1	0.320	0.438	0.795	1.015	0.892	1.083	1.235	1.575	1.622	2.07
1.25	0.383	0.510	0.957	1.098	1.084	1.340	1.481	1.925	1.943	2.53
1.5	0.477	0.727	1.174	1.332	1.337	1.874	1.815	2.68	2.38	3.54
2	0.672	0.848	1.65	2.01	1.84	2.16	2.54	3.09	3.32	4.06
2.5	0.841	1.107	2.09	2.57	2.32	2.76	3.21	4.05	4.19	5.17
3	0.945	1.484	2.38	3.49	2.68	3.74	3.66	5.33	4.77	6.95
3.5	1.122	1.644	2.98	3.96	3.28	4.28	4.48	6.04	5.83	7.89
4	1.344	1.914	3.53	4.64	3.96	4.99	5.41	7.07	7.03	9.24
4.5	1.474	2.04	3.95	5.02	4.43	5.46	6.07	7.72	7.87	10.07
5	1.622	2.18	4.44	5.47	5.00	6.02	6.81	8.52	8.82	10.97
6	1.82	2.78	5.13	6.99	5.99	7.76	7.84	10.64	10.08	13.75
8	2.41	3.77	6.98	9.76	8.56	11.09	10.55	14.74	13.44	18.97
10	3.43	5.20	10.18	13.58	12.35	15.60	15.41	20.41	19.58	26.26
12	4.41	6.71	13.08	17.73	16.35	18.76	19.67	26.65	24.87	34.11

<sup>a</sup>Including areas of accompanying flanges bolted to the fitting.Table 15 Approximate Wall Thickness (L) of Insulation for Pipes<sup>15</sup>

Pipe			Insulation, Nominal Thickness							
Nominal Size	Outer Diameter		in.	1	1.5	2	2.5	3	3.5	4
			mm	25	38	51	64	76	89	102
in.	in. mm		Approximate Wall Thickness							
			in. mm	in. mm	in. mm	in. mm	in. mm	in. mm	in. mm	in. mm
0.5	0.84	21	1.01 26	1.57 40	2.07 53	2.88 73	3.38 86	3.88 99	4.38 111	
0.75	1.05	27	0.90 23	1.46 37	1.96 50	2.78 71	3.28 83	3.78 96	4.28 109	
1	1.32	33	1.08 27	1.58 40	2.12 54	2.64 67	3.14 80	3.64 92	4.14 105	
1.25	1.66	42	0.91 23	1.66 42	1.94 49	2.47 63	2.97 75	3.47 88	3.97 101	
1.5	1.90	48	1.04 26	1.54 39	2.35 60	2.85 72	3.35 85	3.85 98	4.42 112	
2	2.38	60	1.04 26	1.58 40	2.10 53	2.60 66	3.10 79	3.60 91	4.17 106	
2.5	2.88	73	1.04 26	1.86 47	2.36 60	2.86 73	3.36 85	3.92 100	4.42 112	
3	3.50	89	1.02 26	1.54 39	2.04 52	2.54 65	3.04 77	3.61 92	4.11 104	
3.5	4.00	102	1.30 33	1.80 46	2.30 58	2.80 71	3.36 85	3.86 98	4.36 111	
4	4.50	114	1.04 26	1.54 39	2.04 52	2.54 65	3.11 79	3.61 92	4.11 104	
4.5	5.00	127	1.30 33	1.80 46	2.30 58	2.86 73	3.36 85	3.86 98	4.48 114	
5	5.56	141	0.99 25	1.49 38	1.99 51	2.56 65	3.06 78	3.56 90	4.18 106	
6	6.62	168	0.96 24	1.46 37	2.02 51	2.52 64	3.02 77	3.65 93	4.15 105	
7	7.62	194	—	1.52 39	2.02 51	2.52 64	3.15 80	3.65 93	4.15 105	
8	8.62	219	—	1.52 39	2.02 51	2.65 67	3.15 80	3.65 93	4.15 105	
9	9.62	244	—	1.52 39	2.15 55	2.65 67	3.15 80	3.65 93	4.15 105	
10	10.75	273	—	1.58 40	2.08 53	2.58 66	3.08 78	3.58 91	4.08 104	
11	11.75	298	—	1.58 40	2.08 53	2.58 66	3.08 78	3.58 91	4.08 104	
12	12.75	324	—	1.58 40	2.08 53	2.58 66	3.08 78	3.58 91	4.08 104	
14 <sup>a</sup>	14.00	356	—	1.46 37	1.96 50	2.46 62	2.96 75	3.46 88	3.96 101	

<sup>a</sup>Larger sizes through 36 in., same as for 14 in.Table 16 Approximate Wall Thickness of Insulation for Tubes<sup>15</sup>

Tube			Insulation, Nominal Thickness							
Nominal Size	Outer Diameter		in.	1	1.5	2	2.5	3	3.5	4
			mm	25	38	51	64	76	89	102
in.	in. mm		Approximate Wall Thickness							
			in. mm	in. mm	in. mm	in. mm	in. mm	in. mm	in. mm	in. mm
0.375	0.50	13	0.93 24	1.49 38	1.99 51	2.52 64	3.05 77	—	—	—
0.5	0.62	16	1.12 28	1.43 36	1.93 49	2.46 62	2.99 76	—	—	—
0.75	0.88	22	1.00 25	1.56 40	2.06 52	2.86 73	3.36 85	3.87 98	4.37 111	
1	1.12	28	0.87 22	1.43 36	1.93 49	2.74 70	3.24 82	3.74 95	4.24 108	
1.25	1.38	35	1.06 27	1.56 40	2.08 53	2.62 67	3.12 79	3.62 92	4.12 105	
1.5	1.62	41	0.93 24	1.43 36	1.96 50	2.49 63	2.99 76	3.49 89	3.99 101	
2	2.12	54	0.92 23	1.42 36	2.23 57	2.73 69	3.23 82	3.73 95	4.30 109	
2.5	2.62	67	0.92 23	1.45 37	1.98 50	2.48 63	2.98 76	3.48 88	4.04 103	
3	3.12	79	0.92 23	1.73 44	2.23 57	2.73 69	3.23 82	3.80 97	4.30 109	
3.5	3.62	92	0.95 24	1.48 38	1.98 50	2.48 63	2.98 76	3.54 90	4.04 103	
4	4.12	105	1.23 31	1.73 44	2.23 57	2.73 69	3.30 84	3.80 97	4.30 109	
5	5.12	130	1.23 31	1.73 44	2.23 57	2.80 71	3.30 84	3.80 97	4.42 112	
6	6.12	155	1.21 31	1.71 43	2.28 58	2.78 71	3.28 83	3.90 99	4.40 112	

Table 17 Apparent Thermal Conductivity ( $k$ ) Values of Soils in Approximate Order of Decreasing Values\*

Soil Designation	Mean Temperature -40±										
	Mechanical Analysis % by Weight				Moisture Content, %						
	Gravel	Sand	Silt	Clay							
					4		10		20		
					Dry Density, lb/ft <sup>3</sup>						
Over 2.0 mm	0.5 to 2.00 mm	0.005 to 0.05 mm	Under 0.005 mm	100	110	120	90	110	90	100	
Fine Crushed Quartz .....	0.0	100.0	0.0	0.0	12.0	16.0					
Crushed Quartz .....	15.5	79.0		5.5	11.5	16.0	22.0				
Graded Ottawa Sand .....	0.0	99.9		0.1	10.0	14.0					
Fairbanks Sand .....	27.5	70.0		2.5	8.5±	10.5	13.5		15.0		
Lowell Sand .....	0.0	100.0	0.0	0.0	8.5	11.0			13.5		
Chena River Gravel .....	80.0	19.4		0.6		9.0±	13.0				
Crushed Feldspar .....	25.5	70.3		4.2	6.0	7.5	9.5				
Crushed Granite .....	16.2	77.0		6.8	5.5	7.5	10.0				
Dakota Sandy Loam .....	10.9	57.9	21.2	10.0		6.5	9.5		13±		
Crushed Trap Rock .....	27.0	63.0		10.0	5.0	6.0	7.0				
Ramsey Sandy Loam .....	0.4	53.6	27.5	18.5	4.5	6.5			10.0		
Northway Fine Sand .....	0.0	97.0	3.0	0.0	4.5	5.5			8.5		
Northway Sand .....	3.0	97.0	0.0	0.0	4.5	6.0			7.5±		
Healy Clay .....	0.0	1.9	20.1	78.0	4.0±			5.5	9.0±	8.0	10.0
Fairbanks Silt Loam .....	0.0	7.6	80.9	11.5				5.0	9.0±	7.5	10.0
Fairbanks Silty Clay Loam .....	0.0	9.2	63.8	27.0				5.0	9.0±	7.5	9.5
Northway Silt Loam .....	1.0	21.0	64.4	13.6				4.0±	7.0±	6.0±	7.0±

\* $k$  = Btu per (square foot)(hour)(Fahrenheit degree per inch).

Table 18 Conversion Factors to SI Metric Units

(See Chapter 31 for a more complete list of factors.)

Physical Quantity	Symbol	To Convert from	To	Multiply by
Length	$x$	in. ft	m m	2.540 000* E-02 3.048 000* E-01
Area		in. <sup>2</sup> ft <sup>2</sup>	m <sup>2</sup> m <sup>2</sup>	6.451 600* E-04 9.290 304* E-02
Volume		in. <sup>3</sup> ft <sup>3</sup>	m <sup>3</sup> m <sup>3</sup>	1.638 706 E-05 2.831 685 E-02
Temperature		F F	°C K	$t_C = (t_F - 32)/1.8$ $t_K = (t_F + 459.67)/1.8$
Pressure		in. Hg (60 F)	Pa	3.376 85 E + 03
Mass		lb	kg	4.535 924 E - 01
Mass/unit area	$M$	lb/ft <sup>2</sup>	kg/m <sup>2</sup>	4.882 428 E + 00
Moisture content rate		lb/(ft <sup>2</sup> )(week)	kg/(m <sup>2</sup> ·s)	8.072 793 E - 06
Density	$P$	lb/ft <sup>3</sup>	kg/m <sup>3</sup>	1.601 846 E + 01
Thermal conductivity	$k$	(Btu·in.)/(hr·ft <sup>2</sup> ·F)	W/(m·K)	1.442 279 E - 01
Thermal conductance	$C$	Btu/(hr·ft <sup>2</sup> ·F)	W/(m <sup>2</sup> ·K)	5.678 263 E + 00
U-value	$U$	Btu/(hr·ft <sup>2</sup> ·F)	W/(m <sup>2</sup> ·K)	5.678 263 E + 00
Thermal resistance	$R$	(hr·ft <sup>2</sup> ·F)/Btu	(m <sup>2</sup> ·K)/W	1.761 102 E - 01
Thermal resistivity	$r$ /in.	(hr·ft <sup>2</sup> ·F)/(Btu·in.)	(m·K)/W	6.933 471 E + 00
Heat flow	$q$	Btu/(hr·ft <sup>2</sup> )	W/m <sup>2</sup>	3.154 591 E + 00
Water vapor permeability (23°C)	$\mu$	$\frac{\text{grain}}{(\text{hr})(\text{ft}^2)(\text{in. Hg/in.})}$	kg/(Pa·s·m)	1.459 29 E - 12
permeance (23°C)	$p, P$	$\frac{\text{grain}}{(\text{hr})(\text{ft}^2)(\text{in. Hg})}$	kg/(Pa·s·m <sup>2</sup> )	5.745 25 E - 11

\*Exact factor.