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# **Optimum Phase for Thin Film Synthesis by Fourier Transforms**

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**Abstract**: An optimum phase is developed for rugate reflector design by a simple Fourier Transformation. Surprisingly good solutions are obtained for arbitrary spectral curves by phase shaping alone.

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Thin film synthesis techniques can generate solutions from much more elementary starting designs than conventional refinement. This is an appreciable advantage because the demands on filter performance increase continuously. One of the first practical synthesis approaches, proposed several decades ago but still of interest in particular for rugate filters, establishes an analytical relationship between a refractive index profile n(x) and its transmittance  $T(\sigma)$  through a Fourier transform [1,2]:

$$\ln\left(\frac{n(x)}{n_0}\right) \xleftarrow{FT}{\pi} \frac{i}{\pi} \frac{\widetilde{Q}(T,\sigma)}{\sigma} = \frac{i}{\pi} \frac{Q(T) \exp[i\phi(\sigma)]}{\sigma}$$
(1)

In this equation x is twice the centered optical thickness (see the figures),  $n_0$  is a constant, T the transmittance and  $\sigma = 1/\lambda$  the wavenumber or inverse wavelength. Losses and dispersion are ignored in the original theory but there are indirect ways of introducing them in the calculations.

The complex function  $\tilde{Q}(T, \sigma)$  in Eq.(1) is known as the Q-function. Unfortunately the analytical forms of the Q-magnitude Q(T) proposed in the literature lose their accuracy as the reflectance R=1-T increases. Q is approximately equal to  $R^{1/2}$  when R is small. The Q-phase  $\phi(\sigma)$  is usually unknown and has to be generated in the synthesis process. Additional errors are often introduced, for example when n(x) is forced to fit within prescribed thickness and refractive index limits.

Many efforts have been made to improve the Q-function, either by numerical iterations or analytically [3-7]. Most of the efforts concentrated on the magnitude Q(T). Much less has been said on the phase except in rare situations where it is specified, or to recognize that it has a profound effect on the shape of the refractive index profile [8, 9]. Multiple filter solutions of essentially the same reflectance in the region of interest but different phases are frequently possible, from which the most suitable for fabrication can be selected.

This work concentrates on the phase  $\phi(\sigma)$ . An interesting phase first applied to thin films by Druessel and recently implemented by Cheng for the design and fabrication of complex rugate filters is known as the SWIFT phase [7,10]:

$$\frac{\phi(\sigma)}{2\pi} = \frac{x_1 - x_0}{\int\limits_0^\infty \left|\frac{Q(\nu)}{\nu}\right|^2 d\nu} \int\limits_0^\sigma \int\limits_0^\eta \left|\frac{Q(\nu)}{\nu}\right|^2 d\nu d\eta + x_0 \sigma$$
(2)

In this equation,  $x_0$  and  $x_1$  are thickness limits defining a region where the refractive index modulation is uniformly distributed. The slope  $d\phi/d\sigma$  is gradually adjusted so that different spectral regions are mapped to non-overlapping regions of the system in order to avoid the build up of excessive refractive index amplitude [tilting the phase shifts n(x) along the x axis]. This approach is excellent for chirped wide-band reflectors. It does not work as well for narrow bands because it is more difficult to avoid the overlap of refractive index contributions arising from different spectral regions.

Arbitrary reflectance bands are easily handled when the SWIFT phase (or any other phase) is optimized. This is an interesting exercise. In this work the optimization is performed with an upgraded version of the approach described in Ref.[6]. The new version has analytical gradients of the type:

$$\frac{\partial M}{\partial \phi_k} = \sum_i \frac{\partial M}{\partial n_i} \frac{\partial n_i}{\partial \phi_k} \qquad i, k = 1, 2, \dots$$
(3)

where *M* is a standard merit function characterizing the reflectance error (desired – calculated).  $n_i = n(x_i)$  and  $\phi_k = \phi(\sigma_k)$  are points on the *x* and  $\sigma$  grids used in the calculations. The derivative  $\partial n/\partial \phi$  is obtained from Eq.(1) and  $\partial M/\partial n$  is the same as in Ref.[11]. A Quasi-Newton algorithm minimizes the merit value by varying the phase. The magnitude of the Q-function can be adjusted in a similar way. Analytical gradients and the way they are calculated make a significant difference in terms of accuracy and computation speed. The results of the phase optimization are surprisingly good and shed new light on the Fourier Transform Method in thin films.

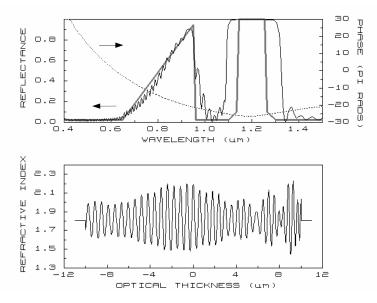


Figure 1: Fourier Transform design generated by the plotted SWIFT phase. Thick grey line: reflectance target. Solid black lines: refractive index profile and its reflectance.

Figure 1 illustrates the design obtained when Q-function [3,4]

$$Q_8 = \ln\left(\sqrt{\frac{1}{\tau}} - \sqrt{\frac{1}{\tau} - 1}\right) \tag{4}$$

and the SWIFT phase represented by a dotted black line are substituted in Eq.(1). The spectral target represented by a thick grey line consists of a linear ramp from 2% to 95% reflectance and a narrow band of 99.9% reflectance. Elsewhere the reflectance should be < 2%. Light is at normal incidence. The refractive index profile represented in the lower part of the figure has an optical thickness of 20 $\mu$ m, essentially what is needed for the narrow reflectance band alone. For simplicity the system is immersed in a medium of average index (1.8). The specified index limits are 1.45 and 2.25.

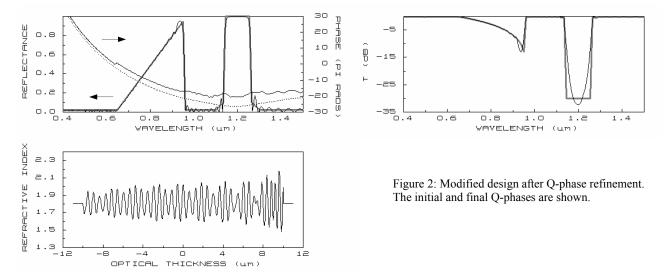
The calculated refractive index modulation is chirped and relatively well distributed in the prescribed thickness and refractive index spaces. The index spread along the thickness axis (and the related SWIFT phase curvature) is adjusted by means of the  $x_1$ - $x_0$  term in Eq.(2). The calculated reflectance is reasonable, especially for wavelengths below 0.95µm, considering the high-reflectance limitations of the Fourier Transform theory and the limitations of the SWIFT phase for narrow reflectance bands. The beats in the index modulation reveal that the contributions from the two reflectance bands overlap, violating the SWIFT phase conditions. Nevertheless this result constitutes a good start for phase refinement.

Figure 2 shows the optimized solution. The reflectance plotted on two different scales is considerably improved. There is also a large change in the Q-phase and the refractive index profile. A Fourier analysis reveals that the index modulation responsible for  $2^{nd}$  reflectance band is essentially a wavelet (apodized sinusoid [12]) spread over the whole available thickness. The index contribution from the triangular band is mostly concentrated on the right hand side of the system in the region of the largest index beats.

The increased Q-phase curvature across the  $2^{nd}$  reflectance band stretches the index profile further by comparison to Fig.(1). It is easily verified that the excess index modulation generated by Q(T) still exists but it is shifted out of the allowed thickness range and is thus not included in the design. Interestingly, the results are quite

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insensitive to the accuracy of Q(T) as long as this function is able to generate enough reflectance. Several other published forms of Q(T) also worked. This phase shaping procedure is remarkably efficient. Introducing Q(T) in the optimization does not improve the solution much. Clearly the optimized Q-phase is not unique and multiple solutions of nearly the same reflectance are possible.



It is interesting to note that related work exists in laser pulse technology [13]. However the height of the pulses does not have to be fitted accurately and the implementation is totally different. To my knowledge the application of this phase-only design approach to thin films is new. This work further stresses the importance of the phase in thin film synthesis by Fourier transforms.

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