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Metabolic Fingerprinting of Biofluids by Infrared Spectroscopy: Modeling and Optimization of Flow Rates for Laminar Fluid Diffusion Interface Sample Preconditioning

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The laminar fluid diffusion interface (LFDI) is a microfluidic tool that manipulates the composition of liquid mixtures by exploiting differences among diffusion coefficients of the dissolved components. One application is the preprocessing of (bio)fluids prior to spectroscopic characterization. For example, in the case of infrared (IR) spectroscopy, the technique can improve sensitivity to low-concentration serum metabolites. The practical benefit is "metabolic fingerprinting" measurements that are more sensitive to low-concentration metabolites than are the counterpart measurements for the original serum sample. Optimal use of the LFDI technique has proven elusive, since the composition of the product of interest is very sensitive to the choice of flow rates for the liquid streams entering and emerging from the LFDI channel. To provide the basis for optimal use, this study had the objective of developing a simulation package that predicts the composition of the LFDI product, given the LFDI structural and operating parameters. To demonstrate the utility of the simulations, composition of the LFDI products predicted for two illustrative sets of trials were compared with experimental data. The flow rates thus derived provided a LFDI product that is relatively rich in serum metabolites, while largely depleted of protein, and very well suited for subsequent IR spectroscopic characterization.

While infrared (IR) spectroscopy has long been recognized as a powerful tool for molecular fingerprinting, the range of applications today extends far beyond what might have been envisaged a generation ago. Today's IR spectrometers and microspectrometers are stable and sensitive enough to usefully characterize complex biological fluids and tissues, serving both as biomedical research tools and potentially as clinical devices.^{1–3} For example, we and others have developed IR-based analytical methods to simultaneously quantify a number of clinically relevant analytes in blood, serum, and

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urine, $^{4-11}$ with parallel efforts on diagnostic test development, $^{12-27}$ including metabolic fingerprinting $^{28-30}$ applications ranging from diabetes $^{18-21}$ to mad cow disease. $^{23-27}$

The spectroscopic methods most commonly associated with emerging metabolomics applications are NMR spectroscopy^{31–40}

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and mass spectrometry (MS).^{41,42} One very attractive feature of NMR spectroscopy is that discrete chemical species generally give rise to discrete spectroscopic patterns that are well-resolved from one another in the spectra of serum and urine. Many of the observed features can therefore be assigned to specific metabolites. The clearest distinguishing features of mass spectrometry as applied to metabolic fingerprinting are the very high sensitivity and broad metabolite coverage. These attractions are counterbalanced by inherent limitations in metabolite quantification (each metabolite requires a separate authentic standard) and by the requirement for fairly elaborate sample preparation and introduction, e.g., by liquid chromatography.

From many perspectives, infrared spectroscopy is the ideal analytical/diagnostic fingerprinting technique. Response is typically linear, the measurement is rapid, and—perhaps most importantly—the cost is low enough and the technique straightforward enough to allow for widespread adoption/implementation of new tests as they emerge. The most significant hindrance to broad adoption of IR spectroscopy in clinical analytical and diagnostic applications is the limited sensitivity. While NMR spectra can reveal features from metabolites in the low micromolar concentration range ($\sim 2-40 \ \mu \text{mol/L}$ at 600 MHz⁴³), detection limits for IR spectroscopy-based serum and urine metabolite assays are typically $\sim 500 \ \mu \text{M}.^{11}$

We have adopted a microfluidic sample preconditioning tool, the "laminar fluid diffusion interface" $^{44-48}$ (LFDI), as a means to

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recover metabolite IR spectroscopic fingerprints that are otherwise below the detection threshold and/or masked by protein absorptions. The defining feature of the LFDI is that it exploits differences among diffusion coefficients to separate high molecular weight from low molecular weight fluid constituents. In the case of serum, the practical benefit is that metabolites (low molecular weight, fast diffusion) may be effectively separated from the relatively abundant proteins (high molecular weight, slow diffusion). The metabolite-rich, protein-depleted LFDI product stream may then be characterized spectroscopically with minimal interference from the otherwise overwhelmingly strong protein absorptions.

Proof-of-concept studies have hinted at the potential benefits of LFDI preconditioning in the IR spectroscopic characterization of both serum and urine samples.^{49–51} Although the initial experiments were encouraging, it was not clear that the experimental parameters (flow rates) were optimal for this new application. The more recent experiments were guided by model predictions; however, that model was limited by the assumptions underlying its development, in particular by the assumption of plug flow (constant velocity at all points in the microchannel crosssection).⁵¹ The velocity profile is more accurately described as parabolic,⁴⁴ with zero velocity at the channel walls and maximum velocity at the channel center, and this has important implications for accurate modeling.

Our present goal is to realize the full potential of the LFDI technique as a means to expand the range of IR spectroscopybased analytical and clinical diagnostic methods. To that end, the aims of this study were (i) to develop the capability to model the fluid flow and molecular diffusion processes that underlie the LFDI separation technique, (ii) to thereby estimate the composition expected of the LFDI product for various choices of experimental parameters (flow rates), and (iii) to compare the model-predicted LFDI product composition to experimental values. The practical objective motivating this work is to ultimately provide an integrated LFDI-IR metabolic fingerprinting platform with the sensitivity rivaling that of NMR spectroscopic measurements.

MATERIALS AND METHODS

Laminar Fluid Diffusion Interface. The laminar fluid diffusion interface lies between two fluid streams—one the sample and the other the receiver fluid—flowing in parallel within a microchannel, with flow rates chosen to ensure laminar flow. While laminar flow ensures no turbulent mixing of the two streams, there is diffusion across the interface between them.

Figure 1 illustrates the essential features of the LFDI microchannel and its use. Because the sample and receiver fluid (typically water) flow in parallel, concentration gradients develop within the receiver stream. The different diffusion rates for slow vs intermediate vs fast diffusers leads to the different concentration profiles. The essential feature of this process is that the receiver

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Figure 1. Schematic depiction of the laminar fluid diffusion channel. Upper panel A shows the "idealized" interface; the sample and receiver fluid streams, of height X_s and X_r , respectively, flow in contact while diffusion occurs across the interface. At the channel exit, the concentration gradients differ for species with low (dark gray shading), intermediate (medium gray), and high (light gray) diffusion constants. Metabolite-rich, protein-depleted product is aspirated from the upper portion of the channel exit, with the precise location of the diffusion barrier X_b determined by the aspiration flow rate. The actual LFDI card (lower panel B) has the sample/receiver and product/waste channels separated by a divider of thickness 127 μ m (5 mil); in practice, the sample stream and diffusion barrier heights are governed solely by the (relative) flow rates Q_s , Q_r , and Q_p . See also Table 1.

Table 1. LFDI (Channel Dimensions	and Operating	Parameters
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parameter	description	parameter	description
$h = 330 \ \mu m$	LFDI channel height	$Q_{ m p}$	product aspiration flow rate (μ L/sec)
w = 4.45 mm	LFDI channel width	X_{s}	height of sample stream (μm)
h/w = 0.074	LFDI channel aspect ratio	$X_{ m r}$	height of receiver fluid stream (um)
L = 22.2 mm	LFDI channel length	$X_{ m p}$	height of aspired product stream (µm)
$V = 32.6 \ \mu L$	LFDI channel volume	$t_{\rm res} = V/(Q_{\rm s} + Q_{\rm r})$	channel residence time (sec)
$Q_{\rm s}$	sample flow rate $(\mu L/s)$	$X_{\rm b} = h - X_{\rm s} - X_{\rm p}$	diffusion barrier height (μm)
Q.	receiver fluid flow rate $(\mu L/s)$	F	

fluid is enriched in low molecular weight species (metabolites) as the sample is depleted of them. The metabolite-rich LFDI "product" is harvested by effectively splitting the emerging stream and collecting only the fluid that emerges above the diffusion barrier X_b . In an "idealized" arrangement, the sample and receiver might be envisaged as streams separated by an infinitely thin knife edge (at a height X_s) until they enter the LFDI channel; similarly, the product aspiration channel would be separated from the waste channel by a knife edge coincident with the diffusion barrier (Figure 1A). In practice, the knife edges are virtual ones; X_s and X_p are governed by the flow rates only.

For practical use, the microchannel is embedded within a laminated card that includes liquid channels and air-pressureactuated valves. The card is interfaced via a manifold to a programmable set of pumps directed by software scripts to control the three flow rates Q_s , Q_r , and Q_p and actuate the pneumatic valves. The LFDI card that we use for serum separations is of custom design (by Micronics, Redmond, WA), distinguished by the use of large reservoirs to accommodate the large sample volumes that are often beneficial for serum work. The card design and operation have been illustrated and described previously.⁵¹

Table 1 summarizes various structural/operating parameters that are specified for any particular LFDI device/trial. In operation, the relative heights of the sample and receiver fluids X_s and X_r (Figure 1) are determined by their relative flow rates $Q_{\rm s}$ and $Q_{\rm r}$. The extent of diffusion is governed by the time the fluids spend in contact with one another, $t_{\rm res}$, which is dictated by the overall flow rate $Q_{\rm s} + Q_{\rm r}$. Finally, the diffusion barrier height is determined by the aspiration flow rate $Q_{\rm p}$ of fluid into a channel that draws the product from the LFDI microchannel exit; the lower is the aspiration flow rate, the larger is the diffusion barrier.

In practice, the LFDI channel is connected to the input (sample/receiver) and output (product/waste) streams via the interface depicted as Figure 1B; the sample and receiver channels are separated by a laminate layer $\sim 127 \ \mu m$ thick, as are the product and waste channels. The present modeling assumes the idealized arrangement (as depicted in Figure 1A); while preliminary simulations suggest that the flow converging–diverging around the dividers may play a role in determining the product composition, the differences are generally subtle, at least in the context of IR spectroscopic measurements.

Model. Given the microchannel geometry, the objective was to develop a computational model that accurately predicts the composition of the LFDI product for any reasonable combination of the three adjustable flow rates Q_s , Q_r , and Q_p . The model considers two incompressible Newtonian fluids of equal viscosities with a velocity profile that is symmetric along the diffusion



Figure 2. Simulated velocity profile for a fluid flowing through the LFDI channel.

channel cross-sectional directions x and y (Figure 1). The following considers the two dynamic processes that occur simultaneously, namely, laminar fluid flow (advection) and molecular diffusion.

Under a pressure gradient $-(\Delta p/L)\mathbf{e}_z$, the Navier–Stokes equation reduces to Poisson's equation, describing Poiseuille flow along the channel:

$$\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} = \frac{\Delta p}{\eta L} \tag{1}$$

where *v* is the flow velocity, $\eta =$ dynamic viscosity of the liquid, and *x*, *y*, and *L* are defined in Figure 1. Equation 1 (with no-slip boundary conditions) may be solved analytically⁵² or numerically using finite differences or finite elements, with comparable computational expense.

The no-slip condition at the channel walls generates a distribution of flow velocities that is essentially parabolic, as illustrated by a scale representation in Figure 2; the flow rate is maximum at the channel center, with a distribution of flow rates diminishing to zero at the channel walls. This flow profile has important ramifications in determining X_s and X_b ; if the profile is expressed as a function of one variable, "x", the flow rate per unit width can now be expressed as

$$Q_{\text{tot.}} = w \int_{x=0}^{h} v(x) \, \mathrm{d}x \tag{2}$$

where

$$v(x) = \frac{6Q_{\text{tot.}}}{h^3 w} x(h-x)$$
(3)

h is the LFDI channel height, *w* is the channel width, and $Q_{\text{tot.}} = Q_{\text{r}} + Q_{\text{s}}$. To determine X_{s} , as a function of Q_{s} , the following integration is carried out

$$Q_{\rm s} = w \int_{x=0}^{X_{\rm s}} v(x) \,\mathrm{d}x \tag{4}$$

and the resulting third order polynomial is solved for the physically admissible value of $X_{\rm s}$. An analogous relation is used to determine $X_{\rm p}$ (given the aspiration flow rate $Q_{\rm p}$) and hence $X_{\rm b}$ (= $h - X_{\rm s} - X_{\rm p}$; see Figure 3).

The general form of the advection-diffusion problem can be expressed in Cartesian coordinates as

$$\frac{\partial C_n}{\partial t} + \left(v_x \frac{\partial C_n}{\partial x} + v_y \frac{\partial C_n}{\partial y} + v_z \frac{\partial C_n}{\partial z} \right) = D_n \left(\frac{\partial^2 C_n}{\partial x^2} + \frac{\partial^2 C_n}{\partial y^2} + \frac{\partial^2 C_n}{\partial z^2} \right)$$
(5)

where C_n is the concentration and D_n the diffusion coefficient for species *n*, and $v = (v_x, v_y, v_z)$ is the flow velocity. The diffusion coefficient describes isotropic diffusion.

The sample and receiver fluids are driven as two parallel laminar flows along the *z*-direction, under a pressure gradient across the ends. The Reynolds number of the flow is low (typically ~1 or less) so that laminar flow is maintained. Furthermore, mass transport by advection dominates diffusion along the length of the cell (in our case the *z*-direction), i.e., $v_z(\partial C/\partial z) \gg D(\partial^2 C/\partial z^2)$. Therefore, we may neglect diffusion along the axis of flow (*z*-axis) and consider only diffusion in the *x*- and *y*-directions perpendicular to the flow. Equation 5 thus simplifies to⁴⁴

$$v \frac{\partial C_n}{\partial z} = D_n \left(\frac{\partial^2 C_n}{\partial x^2} + \frac{\partial^2 C_n}{\partial y^2} \right)$$
(6)

The first step in the computational procedure for finding the concentration $C_n(x,y,z)$ is to solve for the velocity field v(x,y) (eq 1). Equation 6 may then be solved numerically by integrating along the z-direction from z = 0 to z = L (with Neumann boundary conditions; all concentration gradients are zero at the channel walls). With one such eq 6 for each species "*n*", the concentration profile for each species is determined independently. In practice, the concentration profiles were determined by using the parabolic solver (two spatial + temporal dimensions) in the Matlab partial differential equation (PDE) toolbox.

As the fluid exits the channel, at z = L, the product flux rate for species n, q_n , may be determined by integrating the flux density (velocity field multiplied by the concentration profile) over the cross-sectional area of the LFDI channel exit that lies above the diffusion barrier. The limits of integration are determined by flow rates (indirectly; the flow rates dictate the interface and diffusion barrier heights) and the diffusion cell geometry; i.e.,

$$q_n = \int_0^w \int_{h-X_p}^h v_z(x, y) \ C_n(x, y) \ dx \ dy$$
(7)

where X_p is determined as per eq 4 and the discussion following. The LFDI product concentration predicted for species *n* is then evaluated as $C_n = q_n/Q_p$.

Instrumentation and Protocols for Preliminary Experiments. LFDI trials were carried out by using a MicroFlow system from Micronics, with a custom card whose structure and operation have been described previously.⁵¹ Two procedural details have been adopted since that study was reported. First, we now discard as waste the first 90 μ L (three LFDI channel volumes) that emerge from the LFDI channel, with the rationale that the dynamic flow/ diffusion equilibrium takes some time to establish itself within the channel. The second refinement was to discard the first 60

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Figure 3. Concentration profiles calculated for creatinine and albumin within the LFDI channel clearly suggest the possibility of harvesting a metabolite-rich, albumin-depleted sample via aspiration of product from the upper third of the channel exit. Simulation flow rates were $Q_s = 0.83$ μ L/s and $Q_r = 2.03 \mu$ L/s.

 μ L of product that was aspirated into the product hold channel. The rationale for this action is that the first bolus of fluid drawn as "product" upon activation of the aspiration pump would not be representative of the genuine LFDI product; the impulse would unsettle the dynamic equilibrium within the LFDI channel.

All experimental trials discussed here made use of pooled urine samples with elevated albumin levels of typically ~ 1 g/L. Urine samples are concentrated in creatinine, which permitted us to track the fate of both compounds of interest. The main reason for choosing urine samples rather than serum samples was that the viscosity match is much closer for urine/water than for serum/ water.

The efficiencies of all separation trials were gauged by comparing the LFDI product creatinine and albumin levels to those for the original sample. All creatinine and albumin analyses were carried out using standard clinical chemistry assays as implemented on Roche/Hitachi Cobas Modular analyzers in the Clinical Biochemistry Laboratory, St. Boniface General Hospital (Winnipeg, MB, Canada). Creatinine assays made use of an enzymatic method developed by Roche.⁵³ The urine microalbumin method is an immunoturbidimetric assay.⁵⁴

Simulation Outputs: Diffusion Profiles. Albumin and creatinine concentration profiles predicted for one pair of flow rates Q_s and Q_r are illustrated in Figures 3 and 4. Figure 3 provides an intuitively clear impression of how effective the device can be in separating slow (albumin) from rapid (creatinine) diffusers. Quantitative concentration profiles are provided by Figure 4, which shows the creatinine and albumin distributions at each of six distances along the LFDI channel. At z = 0, where the sample and receiver streams first make contact, the profile is a step function for both compounds. As the two streams meet and flow in contact with one another, creatinine diffuses across the interface

Figure 4. Concentration profiles calculated for creatinine and albumin as a function of distance "*z*" along the LFDI channel. Both profiles are step functions at the channel entrance (*z* = 0) and evolve as the sample and receiver fluids flow in parallel. For each compound, the six profiles correspond to normalized values *z* = 0, 0.2, 0.4, 0.6, 0.8, and 1.0. Simulation flow rates were $Q_s = 0.83 \,\mu$ L/s, $Q_r = 2.03 \,\mu$ L/s, and $Q_p = 0.83 \,\mu$ L/s; at these flow rates, $X_p = X_s = 118 \,\mu$ m, and $X_b = 94 \,\mu$ m.

more rapidly than does albumin. By aspirating only the LFDI output stream within the cross-section above the diffusion barrier, it is possible in principle to obtain a product with substantial metabolite (creatinine) concentration that is virtually depleted of protein (albumin).

Simulation Outputs: Application to Biofluid Preconditioning for IR Spectroscopy. The first application of the simulation software was to determine flow rates that yield a product that is suitable for diagnostic/analytical IR spectroscopic metabolic fingerprinting measurements. To that end, we have carried out a series of simulations (and experiments) to explore the effect of

⁽⁵³⁾ Erhardt, V.; Voght, B. W. Manuscript in preparation.

⁽⁵⁴⁾ Multicenter study of Tina-quant albumin in urine and β-N-acetylglucosaminidase (β-NAG) in urine. Workshop Munich, Nov. 29–30, 1990. Wien. Klin. Wochenschr. 1991, 103 (Suppl. 189), 1–64.

Table 2. Summary of Four LFDI Trials Varying the Aspiration Rate $\textbf{Q}_{\rm p}$

21.6	20.8	20.7	20.2
20.8	20.8	19.2	19.2
0.25	0.14	0.09	0.05
1.4	1.3	0.3	0.8
87	145	220	374
15	17	63	25
1.02	1.02	1.02	1.02
1.84	1.84	1.84	1.84
1	0.915	0.824	0.715
10.5	10.5	10.5	10.5
65	73	80	89
	$21.6 \\ 20.8 \\ 0.25 \\ 1.4 \\ 87 \\ 15 \\ 1.02 \\ 1.84 \\ 1 \\ 10.5 \\ 65$	$\begin{array}{cccc} 21.6 & 20.8 \\ 20.8 & 20.8 \\ 0.25 & 0.14 \\ 1.4 & 1.3 \\ 87 & 145 \\ 15 & 17 \\ 1.02 & 1.02 \\ 1.84 & 1.84 \\ 1 & 0.915 \\ 10.5 & 10.5 \\ 65 & 73 \end{array}$	$\begin{array}{ccccccc} 21.6 & 20.8 & 20.7 \\ 20.8 & 20.8 & 19.2 \\ 0.25 & 0.14 & 0.09 \\ 1.4 & 1.3 & 0.3 \\ 87 & 145 & 220 \\ 15 & 17 & 63 \\ 1.02 & 1.02 & 1.02 \\ 1.84 & 1.84 & 1.84 \\ 1 & 0.915 & 0.824 \\ 10.5 & 10.5 & 10.5 \\ 65 & 73 & 80 \end{array}$

^{*a*} As a percentage of the concentration for the original sample. ^{*b*} The enhancement factor K_{Cr} gauges the relative enrichment in creatinine relative to albumin in the LFDI product, as compared to the original sample. ^{*c*} $X_s = 133 \ \mu m$, $X_r = 197 \ \mu m$, and residency time (10.5 s) are the same for all trials. The diffusion barrier height (X_b) varies solely as a consequence of variations in the product aspiration rate Q_s .

manipulating (i) $X_{\rm b}$ (with constant $X_{\rm s}$) and (ii) $X_{\rm s}$ (with constant $Q_{\rm p}$).

RESULTS

Predicted Product Stream Composition. The first set of trials encompassed four sets of flow rates. The first set of flow rates had been adopted for our earlier exploratory studies and was derived using a naïve model assuming plug flow.⁵¹ The other three trials were characterized by successive increases in $X_{\rm b}$, accomplished by decreasing $Q_{\rm p}$ while leaving $Q_{\rm s}$ and $Q_{\rm r}$ unchanged. These simulations, summarized within Table 2, predicted that the product creatinine level should remain quite stable while the albumin level is reduced, i.e., a substantial improvement in the creatinine/albumin ratio with increasing diffusion barrier height.

The second set of trials comprised seven sets of flow rates, varying the height of the sample stream X_s while keeping both the overall flow rate ($Q_s + Q_r$) and the product aspiration rate (and hence X_p) constant. Successive reductions in Q_s (and concurrent increases in Q_r) had the effect of decreasing X_s and thus increasing the diffusion barrier height. These simulations, summarized within Table 3, predict that the creatinine/albumin ratio should increase substantially with decreasing X_s .

Experimental vs Predicted Composition. Experimental data for both sets of LFDI trials are included within Tables 2 and 3. The experimental product compositions (creatinine and albumin

levels) are compared to the simulation predictions in Figure 5. Immediately apparent is the very good qualitative agreement between experimental and simulated results. Simulations clearly capture the significant experimental trends: (i) a gradual decrease in creatinine levels with increasing diffusion barrier height (or, equivalently, a decrease in X_s), (ii) a more rapid decrease in albumin concentration, and (iii) the resultant exponential increase in creatinine/albumin ratio with diffusion barrier height (Figure 6).

The observed creatinine concentrations were generally in very good quantitative agreement with predicted values. In the case of albumin, while the experimental data closely follow the trends predicted by the simulated data, closer examination reveals quantitative discrepancies (see Tables 2 and 3); the LFDI products contain somewhat more albumin than the simulations predict they should.

DISCUSSION

This work provides the basis to simulate liquid flow and diffusion in LFDI channels and hence to determine combinations of flow rates suitable for effective LFDI (bio)fluid preprocessing. Our specific aim was fulfilled, in that we have discovered flow rates that provide 40- to 60-fold enhancements in the metabolite/ protein (creatinine/albumin) ratio of the LFDI product as compared to the original sample. These enhancement levels are completely adequate for the useful integration of LFDI preprocessing with infrared spectroscopy.

The simulations suggest that enhancements in creatinine/ albumin ratio (K_{Cr}) of greater than 100-fold may be achievable, with the ratio increasing exponentially with $X_{\rm b}$. While we have not achieved these targets experimentally, there is good qualitative agreement between the experimental and predicted trends in K_{Cr} (see Figure 6), and the optimal experimental results $(K_{\rm Cr} = 40-60)$ are completely adequate for the IR spectroscopy application of primary interest here (this is the case because serum metabolites collectively amount to a concentration of typically ~ 2 g/L, as compared to a protein concentration of typically \sim 70 g/L; a LFDI preconditioning step with 35-fold enhancement in metabolite/protein ratio is therefore adequate to bring the metabolite absorptions collectively into the same intensity range as the protein absorptions). While there is some metabolite dilution in an absolute sense, this is more than compensated for by drying the LFDI product to a film (or even

Table 3. Summary of Seven LFDI Trials Varying the Height of the Sample Stream X $_{ m s}$ through Successive Decreases
in the Ratio of Sample to Receiver Flow Rates Q _s /Q _r , While Maintaining a Constant Overall Flow Rate (Q _s + Q _r)

$C_{\text{creatinine}}$ (predicted) ^{<i>a</i>}	28.3	26.5	24.9	23.2	21.5	19.8	18.2
$C_{\text{creatinine}}(\text{exptl})^a$	26.7	28.6	24.8	22.9	22.9	21.0	19.0
C_{albumin} (predicted) ^{<i>a</i>}	0.71	0.50	0.41	0.29	0.20	0.14	0.10
$C_{\text{albumin}}(\text{exptl})^a$	2.7	2.1	1.7	2.0	1.2	0.6	0.6
$K_{\rm Cr} = C_{\rm creatinine} / C_{\rm albumin} ({\rm predicted})^b$	40	53	61	80	108	141	182
$K_{\rm Cr} = C_{\rm creatinine} / C_{\rm albumin} ({\rm exptl})^b$	10	14	14	11	19	37	34
$Q_{\rm s}$ ($\mu {\rm L/s}$)	0.80	0.76	0.72	0.67	0.63	0.59	0.55
$Q_{\rm r}$ ($\mu {\rm L/s}$)	1.30	1.34	1.38	1.43	1.47	1.51	1.55
$Q_{\rm p}$ (µL/s)	0.70	0.70	0.70	0.70	0.70	0.70	0.70
residency time (s)	14.3	14.3	14.3	14.3	14.3	14.3	14.3
$X_{\rm s}$ (μ m)	139	134	129	125	120	115	110
$X_{\rm r}$ (μ m)	191	196	201	205	210	215	220
$X_{\rm b}$ ($\mu {\rm m}$)	64	68	73	78	82	87	92

^{*a*} As a percentage of the concentration for the original sample. ^{*b*} The enhancement factor K_{Cr} gauges the relative enrichment in creatinine relative to albumin in the LFDI product, as compared to the original sample.

Figure 5. LFDI product albumin (\blacktriangle = simulation, \triangle = experimental) and creatinine (\blacklozenge = simulation, \bigcirc = experimental) concentrations for two sets of flow rates "A" (left panel; the flow rates and derived parameters for these four trials are summarized in Table 2) and "B" (right panel; the flow rates and derived parameters for these seven trials are summarized in Table 3).

Figure 6. Comparison of simulated to experimental creatinine/albumin enhancement factors for seven LFDI trials. The flow rates and derived parameters for these trials are summarized in Table 3.

stacking successive aliquots), with the added advantage that the otherwise overwhelming water absorptions are entirely eliminated.

While the present experiments do not achieve the very large enhancements in metabolite/protein ratio that the simulations suggest to be achievable in principle, the residual discrepancies may originate with experimental challenges rather than deficiencies of the model. In particular, we are beginning to assess the practical limitations imposed by the (in)stability of the sample/ receiver fluid interface. Extremely smooth pump dispense rates are desirable, since fluctuations of a few micrometers in the interface and/or diffusion barrier height can be very significantparticularly in contributing to possible "leakage" of the waste stream (high protein) over the diffusion barrier. It is extraordinarily difficult experimentally to eliminate all sources of pulsatile flow components, and we suspect residual fluctuations (in very good pumps) to be the dominant factor contributing to variability in the (low) product albumin levels. Although further performance enhancements are simply not required for IR spectroscopic applications, they may prove very beneficial to other metabolomic techniques, in particular for integration with mass spectrometry characterization of the "metabolic fingerprint". To that end, we continue to explore avenues to improve the experimental performance of the LFDI system.

In tandem with possible fine-tuning of the experimental approach, refinements of the modeling protocol are planned. One such refinement will involve developing the capacity to more accurately model the flow of sample, receiver, and product streams at the actual LFDI channel entrance and exit (as opposed to their "idealized" counterparts; see Figure 3). In particular, we will explicitly account for the 127 μ m divider around which the sample and receiver streams merge. Particular emphases will be on the question of whether the sample/receiver interface and/or diffusion barrier height is/are offset relative to their heights predicted on the basis of the idealized LFDI/exit channel interface (Figure 1), and on the possibility of turbulent flow around the blunt divider. Exploratory simulations have highlighted the need to carefully consider the question of where the sample/receiver boundary lies at the LFDI exit; if the boundary were misplaced, the simulated product protein (albumin) concentration distribution would be correspondingly displaced.

In addition, we will incorporate the influence of sample viscosity. The influence is not likely to be important for the particular simulation/experimental comparisons presented here, since the viscosity of urine is very similar to that of water. Preliminary work has shown that the velocity profile is affected and that the sample/receiver interface X_s is shifted relative to the interface for fluids with matched viscosities at the same flow rates.

CONCLUDING REMARKS

The LFDI technique has the potential for very broad application in preconditioning liquid samples for subsequent analytical manipulations (e.g., chromatography) and/or spectroscopic characterization. The progress reported here forms the basis for optimal integration with IR spectroscopic characterization of serum metabolites—"metabolic fingerprinting"—and further points the way to further optimizations that would be beneficial for integration with mass spectrometry. The next steps in our ongoing research will be focused on resolving the residual quantitative discrepancies between simulated and experimental data and thus to open the door to optimal use of the LFDI technique in a broader range of metabolomic and proteomic sample preprocessing applications.

Finally, a very significant attraction of LFDI sample preprocessing is that the technique may in principle be physically integrated with the IR spectroscopic sensor within a single platform. This possibility constitutes a decisive advantage for LFDI preconditioning over ultrafiltration (which requires a centrifuge and attendant sample handling) and opens the door to adoption of the integrated platform in environments requiring rapid sample turnaround and minimal sample handling, e.g., in clinical settings ranging from specialty clinics to the emergency room.

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