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Numerical simulation of thermodynamic behavior of four components PNC including bare clay

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NRCC/IMI, PNC-Tech Meeting, Boucherville, QC, 2004.06.10

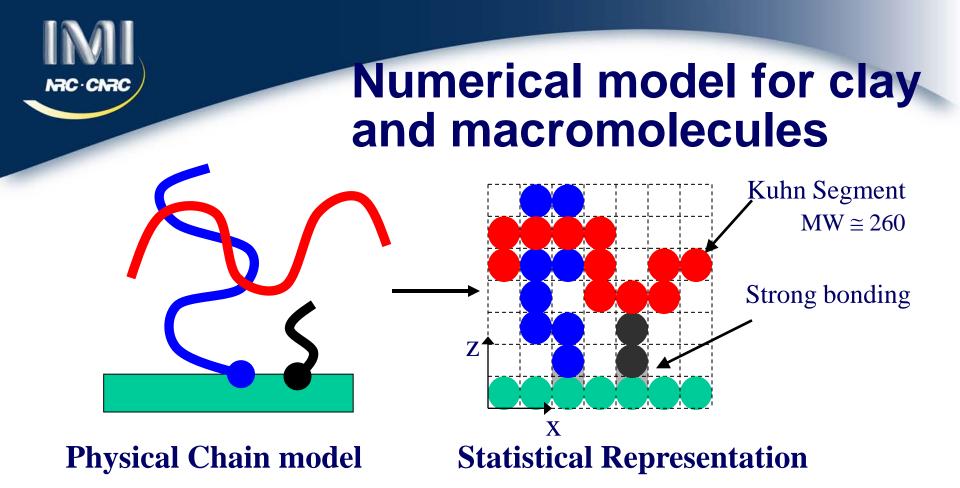


#### **Overview**

 Mathematical modeling and numerical simulation of PNC ⇒Equilibrium thermodynamics

More realistic 2D and 3D models, compromising four components and their interactions
The classical models: Fleer *et al.*, and Balazs *et al.*

Research target
Analysis and optimization of PNC composition to assure system exfoliation (thermodynamic miscibility).



- Clay platelet: No conformational energy
- Host polymer: Conformational and mixing energy
- Compatibilizer: Strong bonding to the surface
- Organic modifier: Strong bonding to clay surface

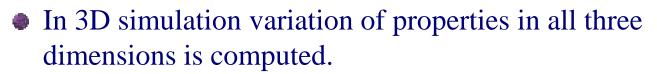
#### 1D vs. 2D or 3D model

In principle, the lattice model of PNC is 3D

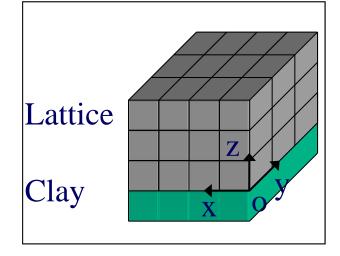
 In 1D simulations it is assumed that properties of any lattice cell on a X-Y plane are identical, varying only with platelet separation in Z.

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In 2D simulation it is assumed that properties depends on X and Z.



The computed differences between 1D, 2D and 3D originate from the different probability for segment placement hence the configurational entropy.





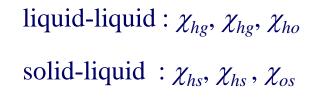
## Theory<sup>1</sup>

Excess free energy Conformational Entropy:

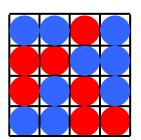
Number of ways to occupy free lattice site

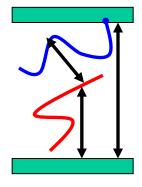
Mixing Enthalpy:

**Huggins-Flory** Theory



solid-solid

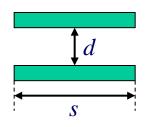




Long-range interaction:

Van der Waals force between a pair of clay plates

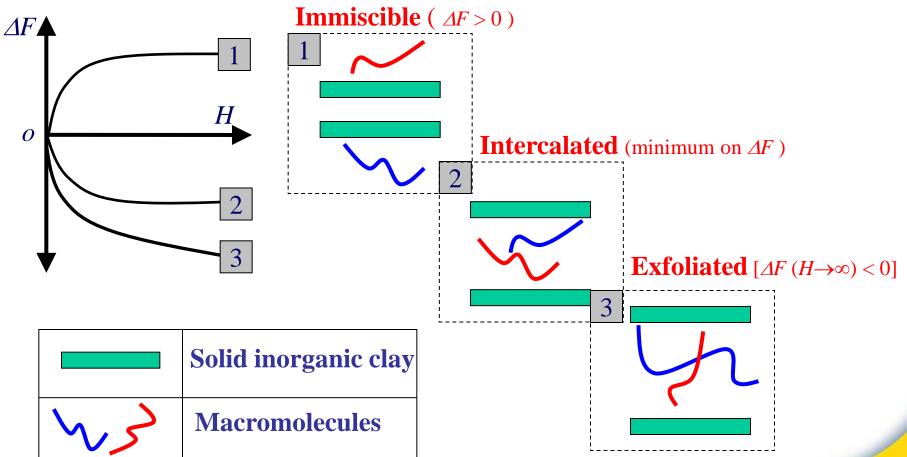
$$F = \frac{-As}{12\pi d^2}$$

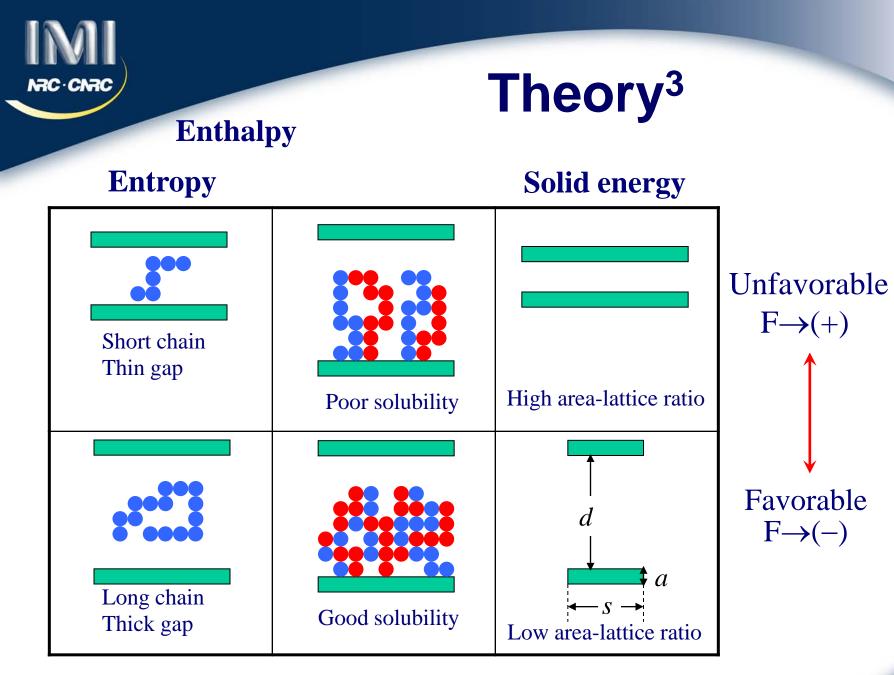






#### • Equilibrium Thermodynamics.



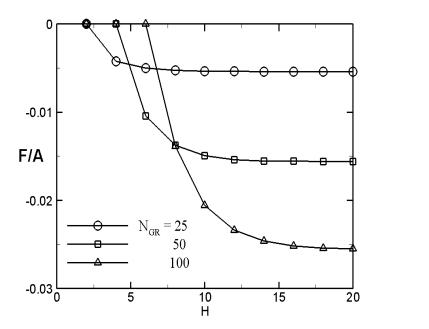


\* Area-lattice ratio :  $\varepsilon = s / a$ 

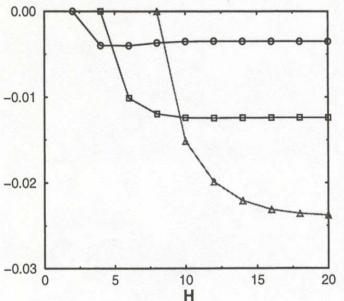


#### Result<sup>1-1</sup>

• Influence of statistical chain length on the excess free energy ( $N_h = 100, N_g \in [25, 100], \rho_g = 0.04, \chi_{gh} = 0$ ) for 1D:



(a) Kim *et al*. (1D)

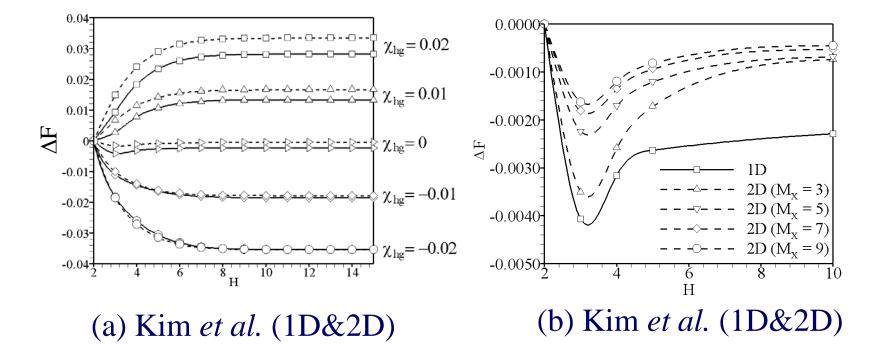


(b) Balazs et al. (1D)



#### Result<sup>1-2</sup>

#### • The influence of dimensionality on excess free energy

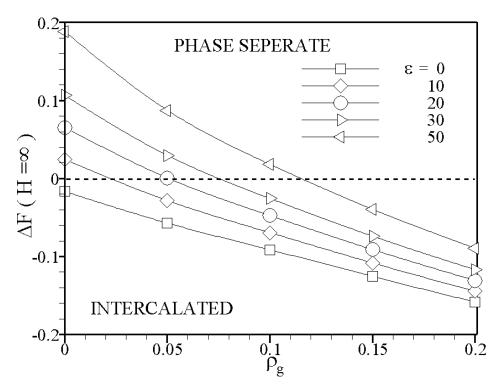


**Statistical chain length:**  $N_g = 25$ ,  $N_h = 100$ , **Surface property:**  $\rho_g = 0.04$ **Binary Interaction parameter:**  $\chi_{hg} \in [-0.02, 0.02]$ 



#### Result<sup>2-1</sup>

• The influence of the area-lattice ratio ( $\varepsilon$ ) and binary interaction  $(\chi_{hg})$  on the excess free energy

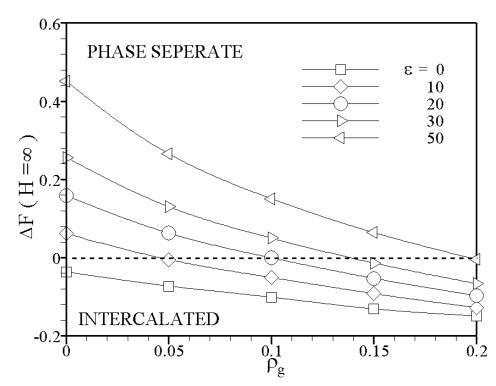


**Statistical chain length**  $N_g = 200, N_h = 400, N_o = 10$ **Surface property**  $\rho_g = 0 \sim 20\%, \rho_o = 70\%, \rho_v = 2 \sim 5\%$ **Solid influence**  $A = 20(k_B T), \varepsilon = 0 \sim 50$ **Binary Interaction parameter**  $\chi_{hg} = 0, \, \chi_{ho} = 0, \, \chi_{go} = 0,$  $\chi_{hs} = 0.01, \chi_{gs} = -0.01, \chi_{os} = -0.02$ 

Neutral ( $\chi = 0$ ; as in PP type PNC) liquid-liquid interactions, solidliquid and solid-solid interactions included (lower vacancy fraction)



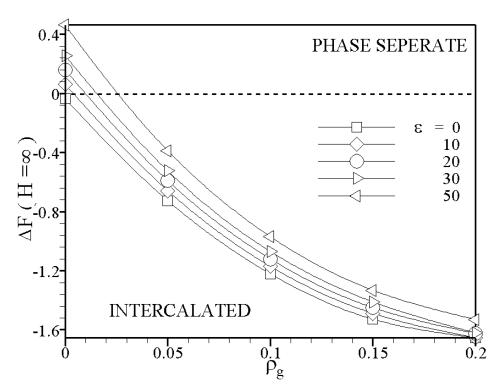
#### Result<sup>2-2</sup>



**Statistical chain length**  $N_g = 200, N_h = 400, N_o = 10$ **Surface property**  $\rho_g = 0 \sim 20\%, \rho_o = 70\%, \rho_v = 5 \sim 10\%$ **Solid influence**  $A = 20(k_B T), \varepsilon = 0 \sim 50$ **Binary Interaction parameter**  $\chi_{hg} = 0, \, \chi_{ho} = 0, \, \chi_{go} = 0,$  $\chi_{hs} = 0.01, \chi_{gs} = -0.01, \chi_{os} = -0.02$ 

Neutral liquid-liquid interaction, solid-liquid and solid-solid interactions included (higher vacancy fraction)

#### Result<sup>2-3</sup>

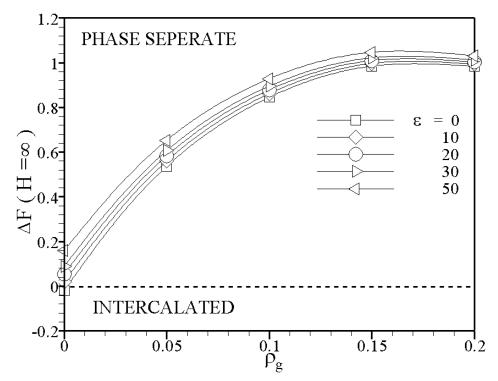


Statistical chain length  $N_g = 200, N_h = 400, N_o = 10$ Surface property  $\rho_g = 0 \sim 20\%, \rho_o = 70\%, \rho_v = 5 \sim 10\%$ Solid influence  $A = 20(k_B T), \varepsilon \in [0,50]$ Binary Interaction parameter  $\chi_{hg} = -0.02, \chi_{ho} = 0, \chi_{go} = 0,$  $\chi_{hs} = 0.01, \chi_{gs} = -0.01, \chi_{os} = -0.02$ 

Favorable liquid-liquid interaction, solid-liquid and solid-solid interactions included (higher vacancy fraction).



#### Result<sup>2-4</sup>



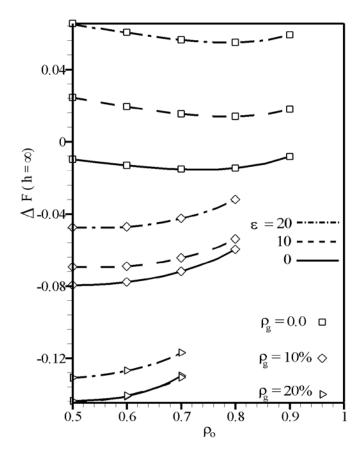
**Statistical chain length**  $N_{g} = 200, N_{h} = 400, N_{o} = 10$ **Surface property**  $\rho_g = 0 \sim 20\%, \rho_o = 70\%, \rho_v = 2 \sim 5\%$ **Solid influence**  $A = 20(k_{B}T), \varepsilon \in [0, 50]$ **Binary Interaction parameter**  $\chi_{hg}=0.02, \chi_{ho}=0, \chi_{go}=0,$  $\chi_{hs} = 0.01, \chi_{gs} = -0.01, \chi_{os} = -0.02$ 

Unfavorable liquid-liquid interaction, solid-liquid and solid-solid interactions included (lower vacancy fraction).



#### **Result<sup>3</sup>**

• The influence of the area-lattice ratio ( $\varepsilon$ ) and grafting density ( $\rho_g$ ,  $\rho_o$ ) on the excess free energy

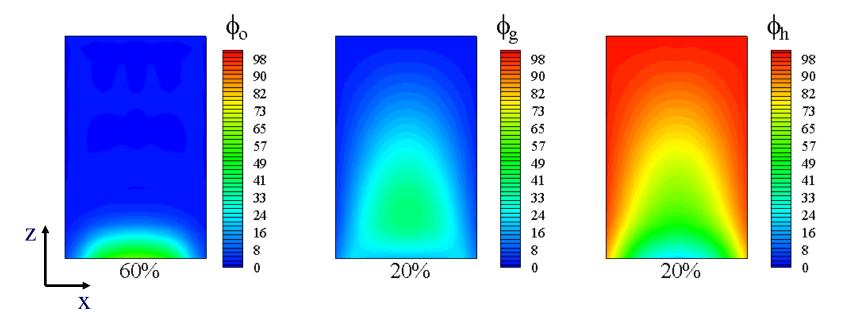


**Statistical chain length**  $N_g = 200, N_h = 400, N_o = 10$ **Surface property**  $\rho_g = 0 \sim 20\%$ ,  $\rho_o = 50 \sim 90\%$ ,  $\rho_v = 2 \sim 5\%$ **Solid influence**  $A = 20(k_B T), \varepsilon \in [0, 20]$ **Binary Interaction parameter**  $\chi_{hg} = 0, \, \chi_{ho} = 0, \, \chi_{go} = 0,$  $\chi_{hs} = 0.01, \, \chi_{gs} = -0.01, \, \chi_{os} = -0.02$ 



#### **Result**<sup>4-1</sup>

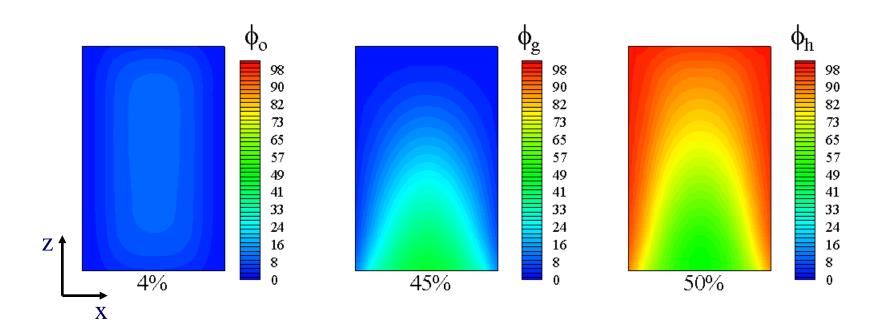
The influence of degradation of organic modifier on the volume fraction of species in 2D lattice.



 $N_g = 200, N_h = 400, N_o = 100, \rho_g = 15\%, \rho_o = 80\%, \rho_v = 2 \sim 5\%, A = 20(k_B T), \chi_{hg} = 0, \chi_{ho} = 0, \chi_{go} = 0, \chi_{hs} = 0.01, \chi_{gs} = -0.01, \chi_{os} = -0.02, \gamma_g = 0.0$ 



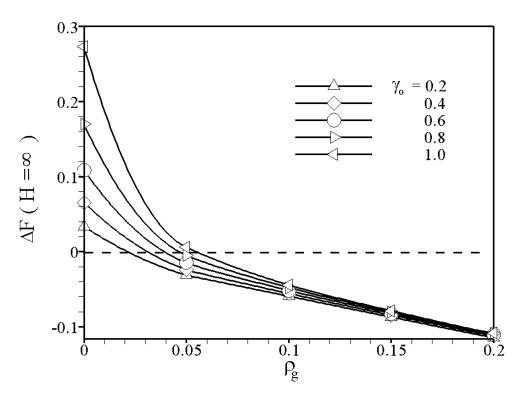
#### **Result**<sup>4-4</sup>



 $N_g = 200, N_h = 400, N_o = 100, \rho_g = 15\%, \rho_o = 80\%, \rho_v = 2 \sim 5\%, A = 20(k_B T), \chi_{hg} = 0, \chi_{ho} = 0, \chi_{go} = 0, \chi_{hs} = 0.01, \chi_{gs} = -0.01, \chi_{os} = -0.02, \gamma_o = 100\%$ 



#### **Result**<sup>4-5</sup>



Statistical chain length  $N_g = 200, N_h = 400, N_o = 10$ Surface property  $\rho_g = 0 \sim 20\%, \rho_o = 70\%, \rho_v = 2 \sim 5\%$ Solid influence  $A = 20(k_B T), \varepsilon = 10, \gamma_o \in [0.2, 1.0]$ Binary Interaction parameter  $\chi_{hg} = 0, \chi_{ho} = 0, \chi_{go} = 0,$  $\chi_{hs} = 0.01, \chi_{gs} = -0.01, \chi_{os} = -0.02$ 

Neutral liquid-liquid interaction, solid-liquid and solid-solid interactions with organic modifier degradation.

#### Summary of findings for SCF model

- To achieve exfoliation in 4-component system:
  - Clay: Intercalated, but with surface partially bare for interacting with a compatibilizer (functionalized polymer)
  - Stable intercalant; no thermal degradation or extraction
  - Compatibilizer

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- Strongly interacting with clay surface
- High molecular weight
- With non-positive  $\Delta F$  of mixing with host polymer
- Host polymer MW comparable to that of compatibilizer.



# Solutions of practical problems

Problem	Suggestion
The absence of specific interaction between host and grafted polymer $(\chi_{hg} = 0)$	Higher grafting density, and/or higher MW of compatibilizer and organic modifier $(\rho_o, \rho_g, N_o \text{ and } N_g)$
Increased bare surface area (unfavorable solid-solid interaction)	Higher favorable interactions between clay and compatibilizer or intercalant (stronger negative values for $\chi_{gs}$ and $\chi_{os}$ )
Thermal degradation of organic modifier (increasing $\gamma_0$ )	- Better attraction between compatibilizer and solid surface and bigger $\rho_g$ - Less unfavorable interaction between host polymer and solid
Unfavorable host polymer-solid interaction ( $\chi_{hs} > 0$ )	Decrease $\rho_v$ High saturation of inorganic surface region with the compatibilizer and organic modifier



### Conclusions

- Successful recovery of the 1D solutions based on the classical theory by Fleer *et al.* and that of Balazs *et al.*
- Validation of the 2D solution by comparison with the 1D approach.
- More realistic physical simulation by incorporating liquidliquid, liquid-solid and solid-solid interactions, as well as binary interaction parameters.
- SCF approach requires less computational resources than molecular dynamics simulation.
- Successful identification of optimum operational parameters.



#### Acknowledgement

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